# Finite-rate oxidation model for carbon surfaces from molecular beam experiments

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FA9550-10-1-0563: AFOSR MURI FY2010 Doctoral Dissertation Fellowship, UofMinnesota





## Background:

**Need:** Understand surface ablation for thermal protection system (TPS) design. Challenging long-duration, high-altitude (nonequilibrium) flight conditions. Accurate ablation models are required within CFD simulations for vehicle design.

**Problem:** Wind-tunnel ablation experiments involve coupled gas-phase, gas-surface physics, which obscures fundamental processes. Current CFD models have large uncertainty.

**Approach:** Molecular Beam experiments combined with molecular simulation/theory to construct new gas-surface reaction models for CFD. Individual reaction mechanisms revealed and quantified.

## **Existing Models: Park Model**

Images and rates taken from: **Park C.**, "Effects of atomic oxygen on graphite ablation", *AIAA Journal*, Vol. 14, No. 11, 1976, pp. 1640-1642.



## Existing Models: Zhluktov and Abe (ZA) Model

• Surface coverage model (required for wide temperature/pressure range).

Zhluktov S.V., Abe T., "Viscous Shock-Layer Simulation of Airflow Past Ablating Blunt Body with Carbon Surface", Journal of Thermophysics and Heat Transfer, Vol. 13, No. 1, 1999, pp. 50-59.

1. 
$$O + (C) \Leftrightarrow (C - O)$$
  
2.  $O_2 + 2(C) \Leftrightarrow 2(C - O)$   
3.  $O_2 + (C) \Leftrightarrow (C - O) + O$   
4.  $O_2 + (C) \Leftrightarrow (C - O) + CO$   
5.  $(C - O) \Leftrightarrow CO + (C)$   
6.  $O + (C - O) \Leftrightarrow CO_2 + (C)$   
7.  $2(C - O) \Leftrightarrow CO_2 + 2(C)$   
8.  $(C) \Leftrightarrow C + (C)$   
9.  $2(C) p \Leftrightarrow C_2 + 2(C)$   
10.  $3(C) \Leftrightarrow C_3 + 3(C)$   
11.  $N + (C) \Leftrightarrow (C - N)$   
12.  $(C - N) + N \Leftrightarrow N_2 + (C)$   
 $k_{f1} = \varepsilon_1 f_0$   
 $k_{f2} = \varepsilon_1 f_{N_2} e^{-T_{a12}/T}$   
 $k_{f1} = \varepsilon_{11} f_N$   
 $k_{f1} = \varepsilon_{12} f_{N_2} e^{-T_{a12}/T}$ 

# Existing Models: Zhluktov and Abe (ZA) Model

- **Surface coverage** model (required for wide temperature/pressure range).
- But how to parameterize all of the rate coefficients? Typical ablation experiments involved coupled gas-phase and gas-surface processes.

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1.	$0 + (C) \Leftrightarrow (C - 0)$	$k_{f1} = \varepsilon_1 f_0$
2.	$O_2 + 2(C) \Leftrightarrow 2(C - O)$	$k_{r^2} = \varepsilon_2 B(kT/h) e^{-T_{a^2}/T}$
3.	$O_2 + (C) \Leftrightarrow (C - O) + O$	$k_{f3} = \varepsilon_3 f_{O_2} e^{-T_{a3}/T}$
4.	$O_2 + (C) \Leftrightarrow (C - O) + CO$	$k_{f4} = \varepsilon_4 f_{\rm CO_2}$
5.	$(C - O) \Leftrightarrow CO + (C)$	$k_{f5} = \varepsilon_5 B(kT/h) e^{-T_{a5}/T}$
6.	$O + (C - O) \Leftrightarrow CO_2 + (C)$	$k_{f6} = \varepsilon_6 f_0 e^{-T_{a6}/T}$
7.	$2(C - O) \Leftrightarrow CO_2 + 2(C)$	$k_{f7} = \varepsilon_7 B(kT/h) e^{-T_{a7}/T}$
8.	$(C) \Leftrightarrow C + (C)$	$k_{r8} = \varepsilon_8 f_{\rm C}$
9.	$2(C) p \Leftrightarrow C_2 + 2(C)$	$k_{r_{2}} = \varepsilon_{2} f_{C_{2}}$
10.	$3(C) \Leftrightarrow C_3 + 3(C)$	$k_{12} = s_{12} f_{-}$
11.	$N + (C) \Leftrightarrow (C - N)$	$k_{r10} = c_{10}/c_3$
12.	$(C - N) + N \Leftrightarrow N_2 + (C)$	$k_{f11} = \varepsilon_{11} f_{\rm N}$
		$k_{r12} = \varepsilon_{12} f_{\rm N_2} e^{-r_{a12}/T}$

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- We propose to use Molecular Beam experiments.

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## Molecular Beam Experiments (Minton group – Montana State)



## Can we use Molecular Beam data for boundary layer flows?

Two significant results from Molecular Beam (MB) experiments (Minton group, Montana State) changed our approach:

- 1) Majority of reaction products were observed to scatter *thermally* (despite the high-energy 5eV beam O atom source).
  - the beam acts as a supply of oxygen to the surface and scattering is primarily dependent on the surface temperature, not the beam energy

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- 2) Despite near-vacuum conditions, the carbon surfaces in MB experiments have a high surface coverage of O atoms (T<1200K). At higher surface temperature the surface begins losing O coverage.
  - if experimental surfaces had low coverage at all conditions, this would have made its use for boundary layer flows (high p) questionable
  - surface coverage modeling is important for CFD and the fact that a transition from high-to-low coverage is observable in the experiments is very interesting

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These two results enable individual reaction rates, for use in CFD-type ablation models, to be determined using Molecular Beam data.

## Molecular Beam Results: Time-of-Flight (TOF) Distributions

- Beam contains 93% 0 and 7%  $O_2$
- Beam pulse lasts only  ${\sim}1~\mu s$  and occurs every 0.5 seconds (2 Hz)
- TOF distributions for various T<sub>surface</sub> (single scattering angle of 15 degrees) averaged under steady-state operation (~15min of beam operation)



Using *only* the Molecular Beam data, we have constructed a preliminary oxygen-carbon gas-surface model:

Mechanisms	Rate	Rate constant (k)	Units
${ m O}+({ m s}) ightarrow{ m O}({ m s})$	$k_1[O][(s)]$	$\frac{1}{4B}\sqrt{\frac{8k_bT}{\pi m_O}}$	$\frac{m^3}{mol \ s}$
m O(s)  ightarrow  m O+(s)	$k_2[O(s)]$	$\frac{2\pi m_O k_b^2 T^2}{Bh^3} e^{-\frac{44277}{T}}$	$\frac{1}{s}$
$\mathrm{O} + \mathrm{O}(\mathrm{s}) + \mathrm{C}(\mathrm{b}) \rightarrow \mathrm{CO} + \mathrm{O}(\mathrm{s})$	$k_3[O][O(s)]$	$\frac{1}{4B}\sqrt{\frac{8k_bT}{\pi m_O}}57.37e^{-\frac{4667}{T}}$	$\frac{m^3}{mol \ s}$
$O + O(s) + C(b) \rightarrow CO_2 + (s)$	$k_4[O][O(s)]$	$\frac{1}{4B}\sqrt{\frac{8k_bT}{\pi m_O}} 8.529 \times 10^{-6} e^{-\frac{-6958.0}{T}}$	$\frac{m^3}{mol \ s}$
$\mathrm{O} + \mathrm{C(b)} + \mathrm{(s)}  ightarrow \mathrm{CO} + \mathrm{(s)}$	k <sub>6</sub> [O][(s)]	$\frac{1}{4B}\sqrt{\frac{8k_bT}{\pi m_O}}0.1203e^{-\frac{-2287}{T}}$	$\frac{m^3}{mol \ s}$

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A finite-rate model accounting for surface coverage (similar to Z-A model) does in fact fit the MB data accurately (bottom-left figure). Very interesting.

Surface coverage model is based only on MB data, yet it should be applicable to much higher fluxes (bottom-right figure). Remarkably, these predictions are in reasonable agreement with existing models/literature for boundary layer (high flux) conditions.



AFOSR Aerothermodynamics - BRICC (06/29/16)

#### In fact, a maximum in CO production was observed experimentally!!



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Our new model predicts maximum CO probability at similar T<sub>surface</sub> seen in both experiments at significantly different pressures (due to surface-coverage modeling).



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[10/14]
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Simulations performed by Graham V. Candler (University of Minnesota)

- Hypersonic flow over 8<sup>0</sup> cone with 10cm radius leading edge (using the US3D code)
- 5-species reacting air, U = 7km/s, prescribed  $T_{surface}$  variation around geometry





[12/14]

- Total mass loss is similar between models, species fluxes are completely different.
- ZA-model: All CO<sub>2</sub> for T<3000K and all CO for T>3000K
- New-model: All CO at any T with negligible CO



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- ZA-model: All CO<sub>2</sub> for T<3000K and all CO for T>3000K
- New-model: All CO at any T with negligible CO
- P<sub>CO</sub> >> P<sub>CO2</sub> is consistent with recent CFD/Experimental results of Dr. Chris Alba *et al.*:

C.R. Alba, R.B. Greendyke, J. Marschall, Development of a Nonequilibrium Finite-Rate Ablation Model for Radiating Earth Reentry Flows, Journal of Spacecraft and Rockets, 2016, Vol.53, No. 1, pp. 98-120.



- At higher altitudes (stronger nonequilibrium), the total mass loss is higher with the new model [solid black line].
- Again, the species fluxes are completely different. Notice how the ZA-model predicts CO *adsorption* leading to CO<sub>2</sub> production.

## Conclusions

1) Clearly, the same macroscopic result (i.e. surface recession) can be obtained with many different model parameterizations. Too many "knobs" to turn...

2) A new experimental method of creating/validating CFD ablation models is introduced. Molecular Beam data can uniquely determine *individual* mechanisms and rates, in contrast to plasma wind-tunnel measurements where all processes are coupled.

3) The observations of thermal reaction mechanisms and surface coverage dependence make Molecular Beam data directly relevant to hypersonic flows.

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AFOSR Aerothermodynamics - BRICC (06/29/16)



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## New AFOSR Grant (starting in Fall 2016)

## "Nonequilibrium Gas-Surface Interactions at High Temperature"



Aerothermodynamics (Dr. Ivett Leyva)

Aerospace Materials for Extreme Environments (Dr. Ali Sayir)

Tom Schwartzentruber – Minnesota Graham Candler – Minnesota Tim Minton – Montana State Erica Corral – Arizona John Perepezko – Wisconsin



Brief Overview:

- Further oxygen-carbon molecular beam experiments
- Finalize/validate oxygen-carbon CFD model
- Molecular beam and torch testing of ceramic (SiC-based) TPS
- CFD modeling of ceramic (SiC-based) TPS, validated models
- Fabrication of new TPS materials and coatings for testing in various facilities

## Last Year: A general mechanism for carbon oxidation



# **Relevant Length Scales**

SEI

5.0kV

X30,000

U of MN

- Molecular Dynamics domain is the size of ~1 pixel on image below...
- Carbon surfaces used in Molecular Beam experiments are representative of surface structure well-above the atomic scale.

SEM Image by Eric Stern (Minnesota) Oxidized Carbon Fiber

100nm

WD 6.1mm

Can Molecular Beam data be used directly?

50 nm

MD Simulations: Poovathingal, Schwartzentruber, Srinivasan, van Duin, J. Phys. Chem. A, 2013.



Nicholson, Minton, Sibener, J. Phys.

Chem. B 2005, 109, 8476-8480

## Molecular Beam Results: Time-of-Flight (TOF) Distributions

• TOF distributions are accurately fit with a Maxwell-Boltzmann distribution corresponding to  $T_{surface}$  (thermal scattering is dominant, especially for CO/CO<sub>2</sub>)





## Reaction Probabilities from Molecular Beam Data

Molecular Beam scattering occurs under steady-state conditions.

We therefore assume that the amount of oxygen in the beam flux is equal to the amount of oxygen observed to scatter from the surface  $(0, 0_2, CO, CO_2)$ . Thus, we can readily calculate probabilities of forming each reaction product.

Event	$P_{\rm Exp-i} = N_i/N_{\rm O_{beam}}$		
	Case I	Case II	
$\mathrm{C(s)} + \mathrm{O}  ightarrow \mathrm{C(s)} + \mathrm{O}$	0.743	0.431	
$\mathrm{C(s)} + \mathrm{O}  ightarrow \mathrm{CO}$	0.193	0.421	
$\mathrm{C(s)} + \mathrm{O} + \mathrm{O} \rightarrow \mathrm{CO_2}$	0.032	0.074	

Case 1: Keep hyperthermal O Case 2: Ignore hyperthermal O

Regardless of small assumptions: Mainly CO production (little  $CO_2$ ). Reaction prob. is high ( > 0.1).  $O_2$  is essentially non-reactive.



Reactant flux (N<sub>i</sub>): thermal component (red), hyperthermal component (blue), total (yellow).