

# (Micro) Rectenna Arrays for Infrared Power Conversion



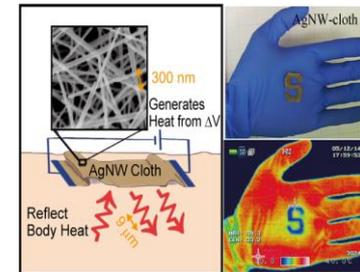
**Dr. Richard Osgood, Mr. Stephen Giardini, Dr. Yassine Ait El Aoud, Ms. Diane Steeves, Mr. Dennis Magnifico**  
**US Army Natick Soldier Research, Development, and Engineering Center**



**Drs. Lalitha Parameswaran, Mordechai Rothschild, Vladimir Liberman**  
**MIT Lincoln Laboratory**

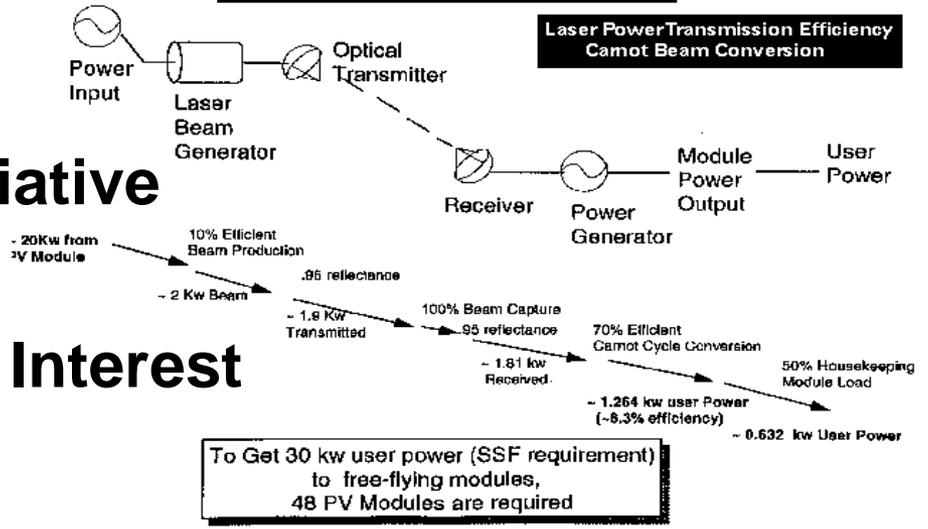
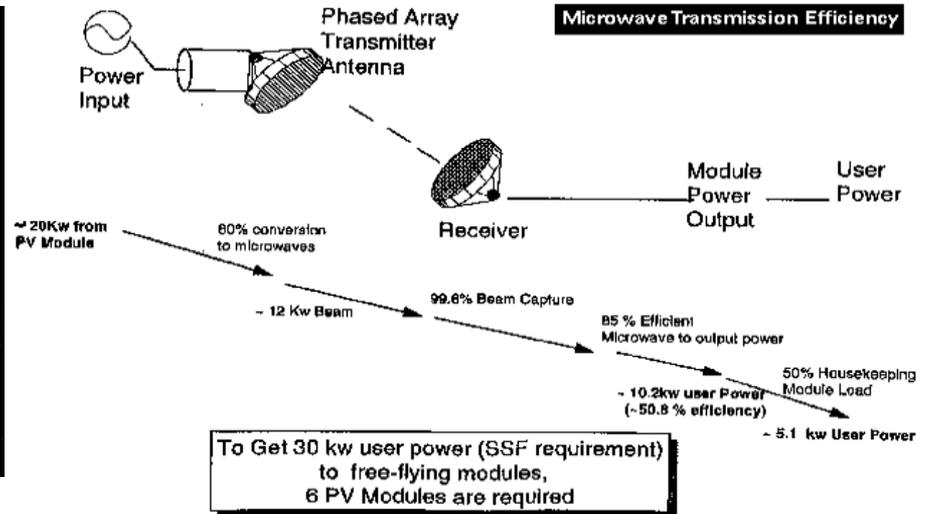
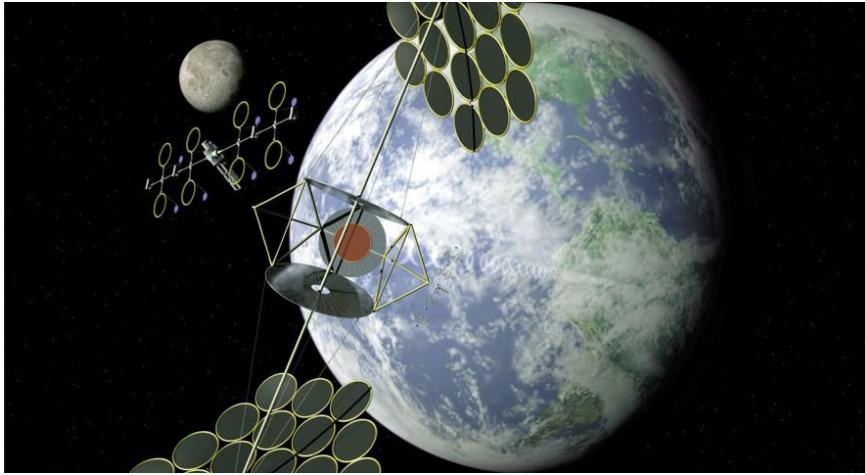
**Prof. Jimmy Xu, Dr. Gustavo Fernandes, Mr. Declan Oller, Dr. Jin Ho Kim**  
**Brown University**

**Prof. Ki-Bum Kim, Ms. Min-Yi Kang\***  
**Seoul National University, Republic of Korea**



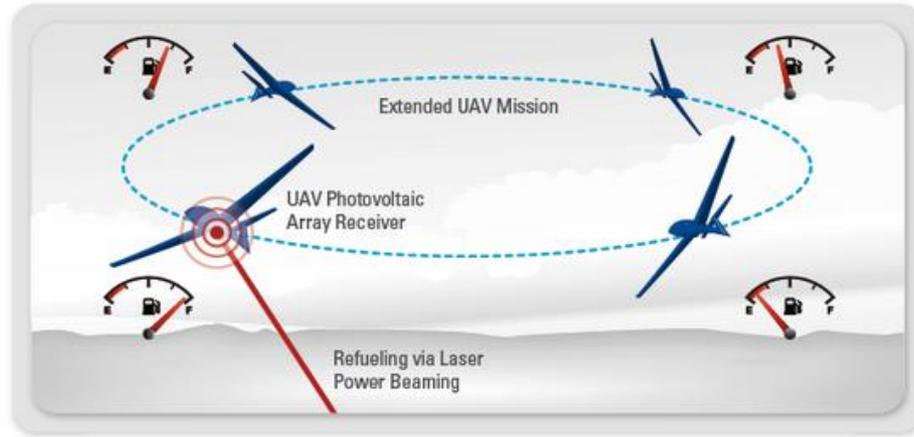
**Mr. Mathew Chin, Dr. Madan Dubey, Dr. Barbara Nichols**  
**Army Research Laboratory (ARL) – Sensors and Electron Devices Directorate**





- Space Solar Power Initiative
- Solar Power Satellite
- Japanese Government Interest
- Also Infrared Sensing

- **UAS sustainment**



**Resonant Infrared Wavelengths – Converted to Signal**

**Non-Resonant Wavelengths Rejected**

Tuned infrared detectors detect preferred wavelength band from friendly sources

- Communication
- Combat ID
- Use wavelengths undetectable to standard commercial detectors

• Challenges: Requires line-of-sight, laser sources, and research on devices and efficient power/signal transfer

Output Current

Frequency

Microrectenna Response



**Other applications: Battlefield Data Transfer and Identification**

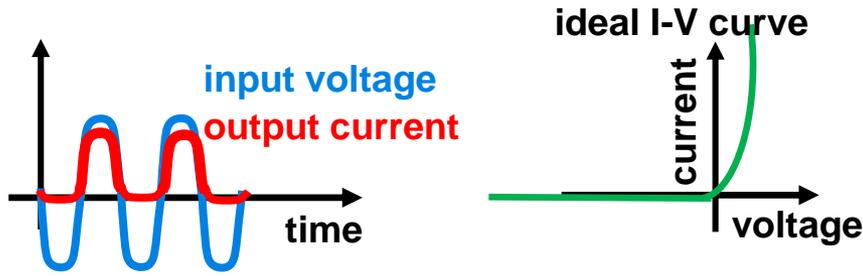


# (Micro) Rectenna Arrays for Infrared Power Conversion

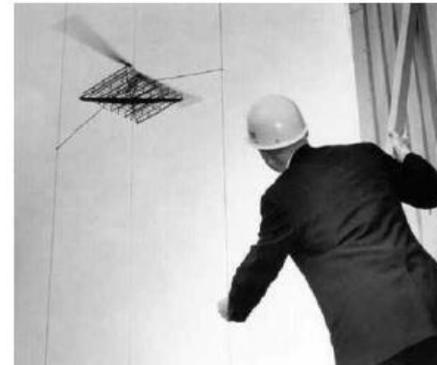


- **What are microrectennas and microrectenna arrays?**
- **Materials for microrectenna arrays**
- **Vertical MIM diode rectifiers**
  - J-V curve experiments and modeling
  - Estimation of responsivity and direct current
- **Horizontal stripe-teeth metamaterial arrays**
  - Design and fabrication
  - Analysis
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# Antenna-coupled rectifiers for GHz



Diode rectification  
(assumes ideal, highly non-linear I-V curve)



Dr. W. C. Brown, Raytheon Corporation (1964)

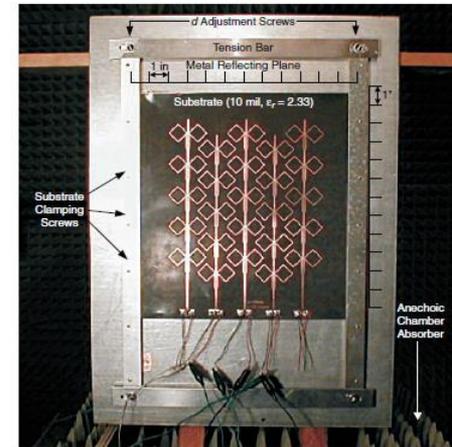
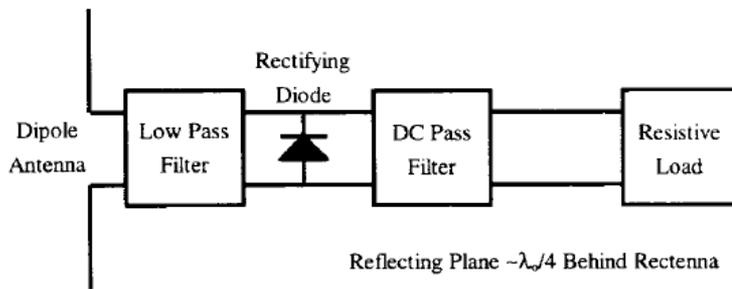


Figure 9. 5.61-GHz circular polarized printed rectenna with over 78% efficiency [38].

>75% efficient 5.61 GHz rectenna array (TAMU) – IEEE Microwave Journal (2002)

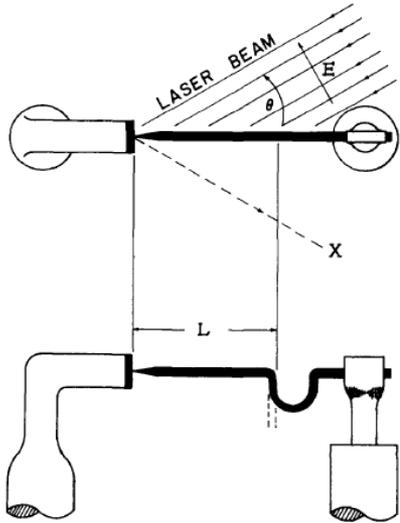
McSpadden *et. al.*, IEEE Trans. Microw. Theory Tech. v. 46 p.2053 (1998)

$\eta > 80\%$  for 5.8 GHz!



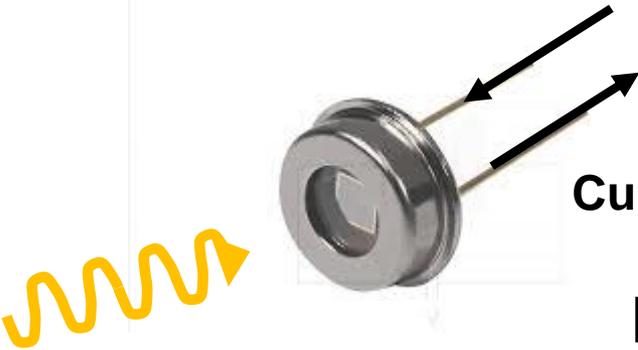
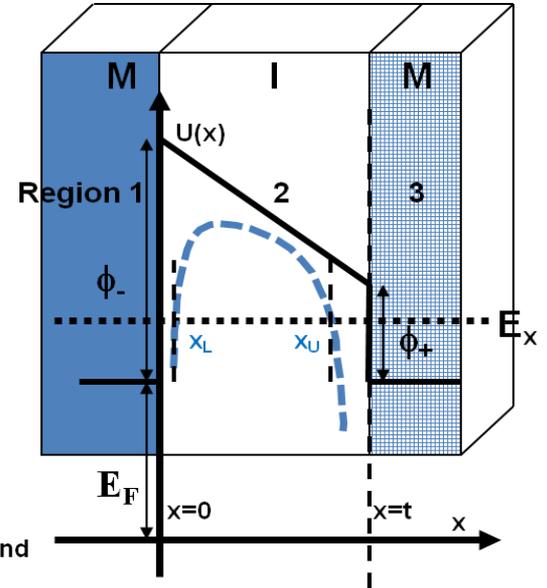
# High frequency Metal-Insulator-Metal (MIM)-based diodes for detection

- Accurate measurements of infrared/visible frequencies



**Point-contact devices  
(1960s and 1970s)**

“Improved coupling to infrared whisker diodes by use of antenna theory” Matarrese and Evenson, *Appl. Phys. Letts.* 17, 8 (1970)



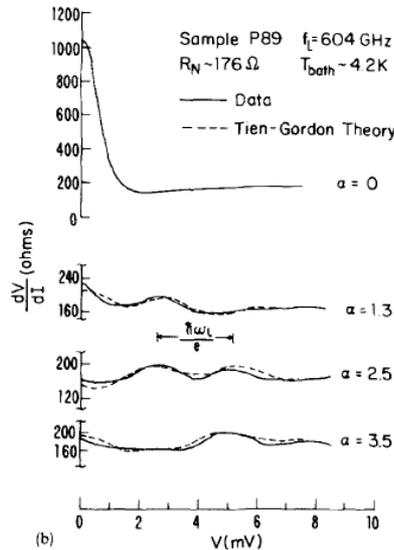
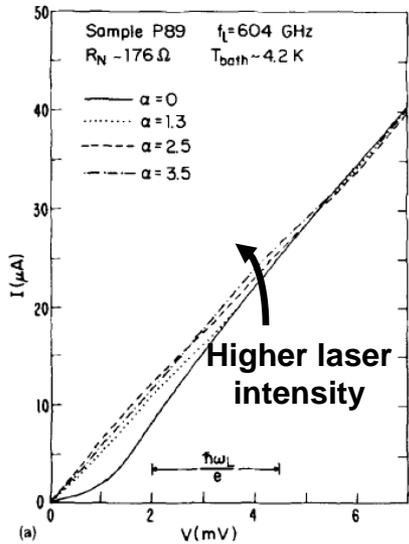
**Current in Amperes**

**Responsivity R in A/W [1/V]**

**Radiative power in Watts**

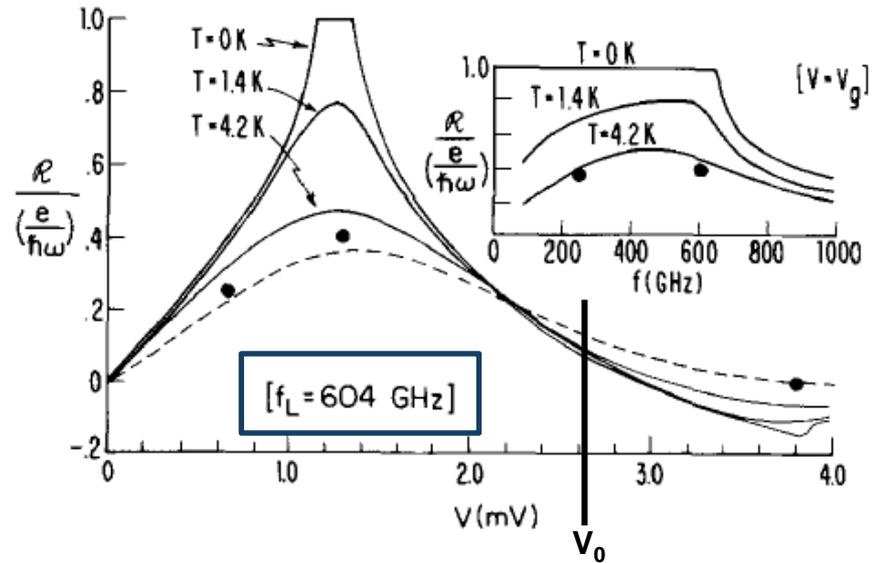
# Responsivity of Metal-Insulator-Metal (MIM) Diodes

- Tinkham: Responsivity of Superconductor – Insulator – Superconductor/Normal junctions (1982)



Steps in  $dV/dI$  separated by photon voltage = (photon energy)/ $e$

$$\alpha = V_{AC}/\text{photon voltage}$$



$$R_Q = \frac{e}{\hbar\omega} \left[ \frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e) - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

Rectification responsivity  $R_Q$  in A/W

# Quantum responsivity of MIM diodes

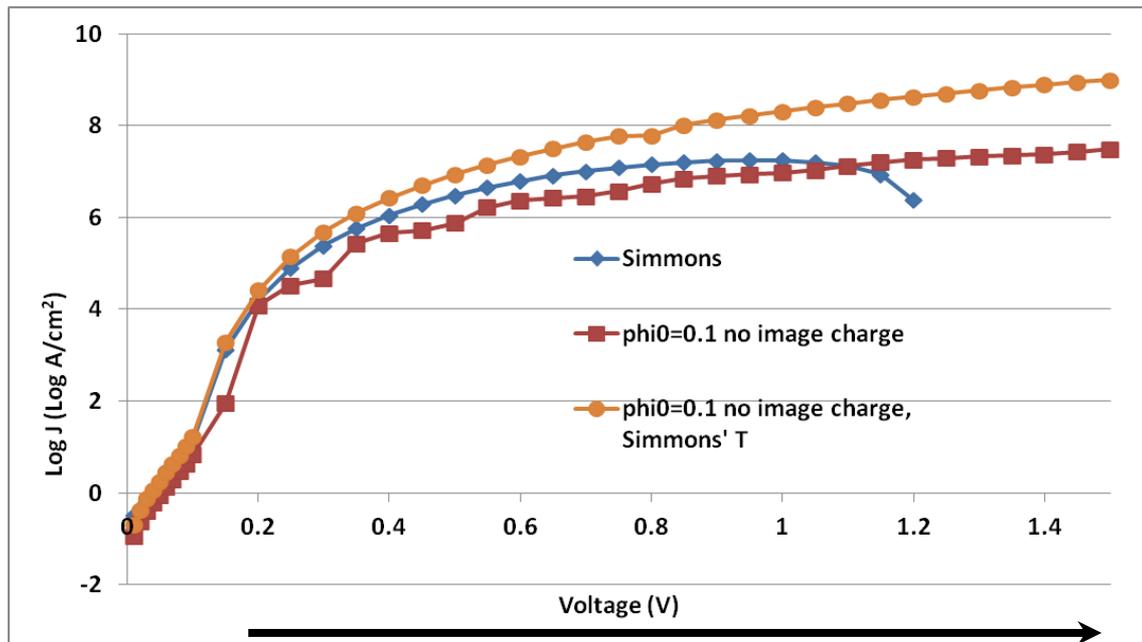
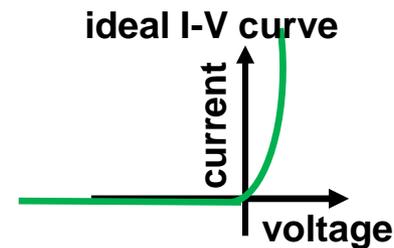
$$R_Q = \frac{e}{\hbar\omega} \left[ \frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e) - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

0.45 A/W maximum  
for green light  
(higher in infrared)

➔ 
$$= \frac{1}{2} \frac{\partial^2 I_{dc} / \partial^2 V}{\partial I_{dc} / \partial V} \Big|_{V=V_0}$$

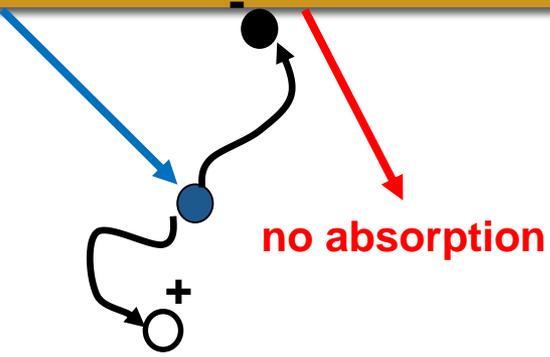
Approximation!  
Valid only in  
classical case

Must model I-V curve  
to predict rectification  
responsivity (A/W),  
especially at high  
voltages for  $R_Q$ !



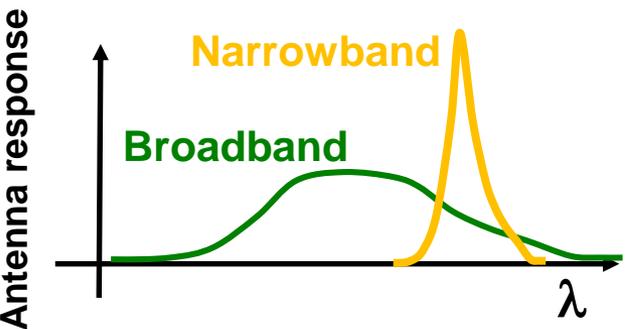
photon voltage  $\hbar\omega/e$  (visible light)

# What are microrectennas and microrectenna arrays?

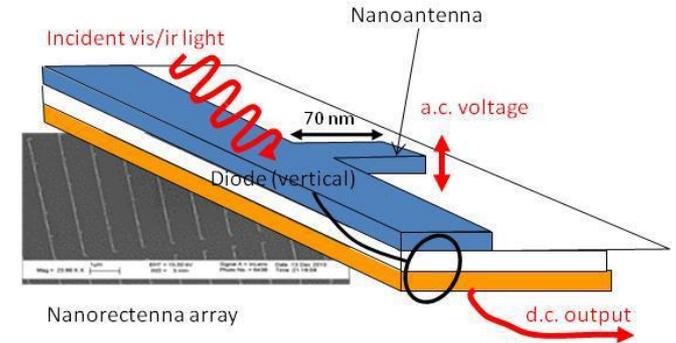


Photovoltaic (electron-hole generation with semiconducting bandgap)

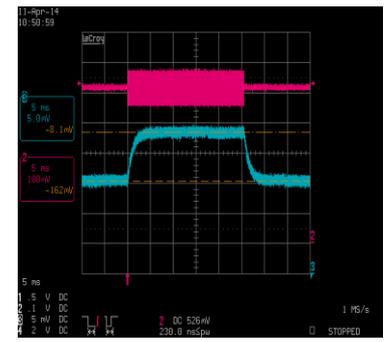
PV doesn't absorb photon energies less than bandgap



Dependent on dimensions and conductivity (no bandgap)



Perspective view of microrectenna



$$\Delta I_{dc} * 1 M\Omega$$

Simple rectification verification at 1 MHz (NbOx – based diode)



# (Micro) Rectenna Arrays for Infrared Power Conversion

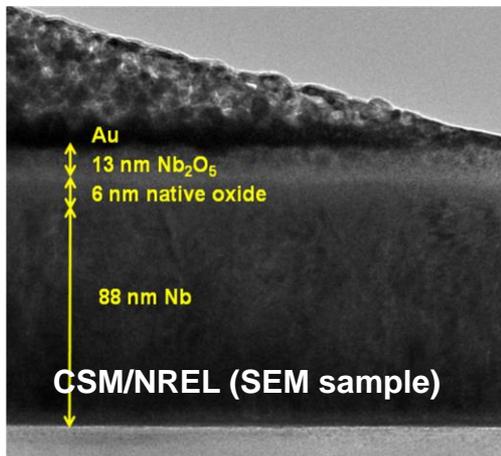


- **What are microrectennas and microrectenna arrays?**
- **Materials for microrectenna arrays**
- **Vertical MIM diode rectifiers**
  - J-V curve experiments and modeling
  - Estimation of responsivity and direct current
- **Horizontal stripe-teeth metamaterial arrays**
  - Design and fabrication
  - Analysis
  - Response to cw lasers

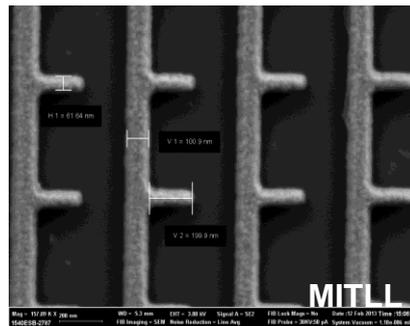
# Materials for microrectenna arrays

- **Materials systems investigated:**
  - M/Nb<sub>2</sub>O<sub>5</sub>/NbO<sub>x</sub>/Nb, M = Ag/Ti, Au/Ti, Pt/Ti, others
  - M/Al<sub>2</sub>O<sub>3</sub> (ALD)/Al, M = Al, Au
- **Al or Nb ground planes**
- **Au wire antennas underneath Al electrode**
  - Small cluster of nanorectennas
  - Antennas run between electrodes in top plane, vertical MIM diode (same as other cases)

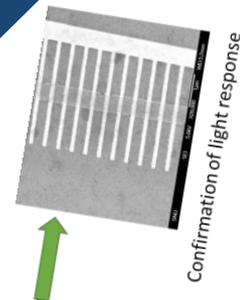
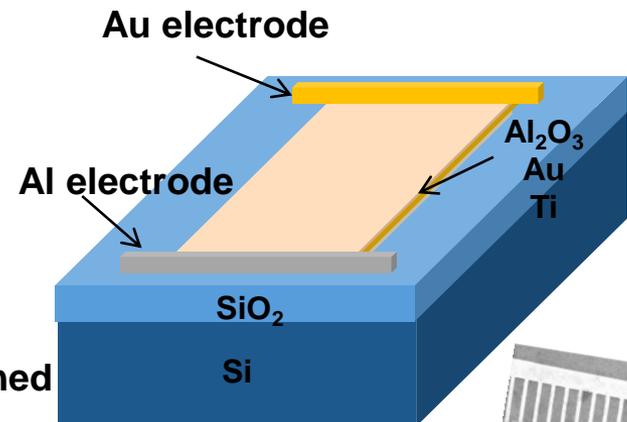
- **CNT-based diodes**



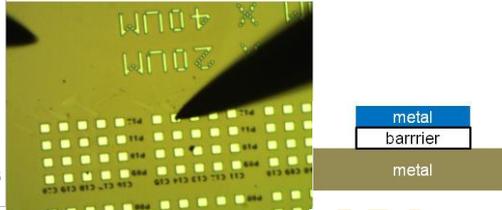
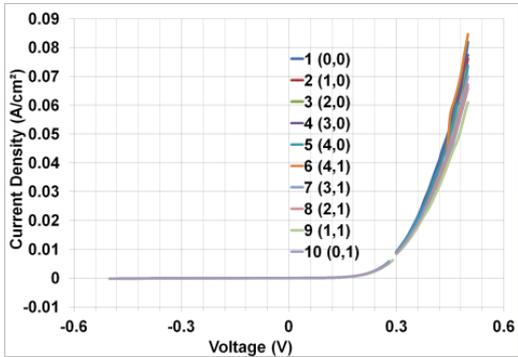
Cross-section of NSRDEC-designed microrectenna array (metal-insulator-metal (MIM) diode)



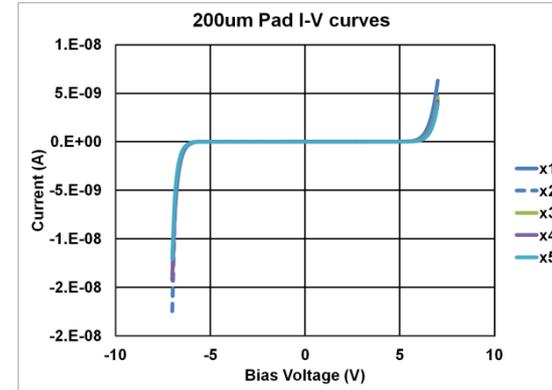
Plan view of NSRDEC-designed microrectenna array (Al stripe-teeth antennas)



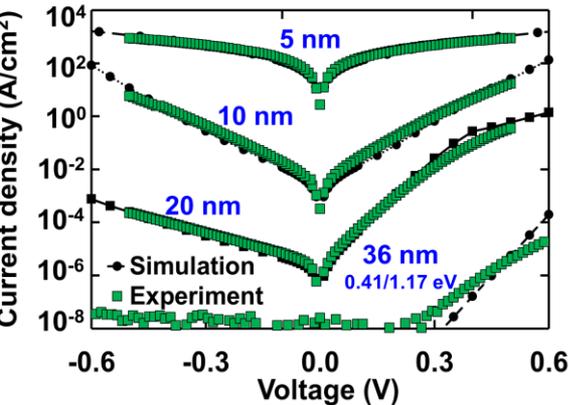
# Vertical MIM diode rectifiers (Al- and Nb-based)



Pt/NbO<sub>x</sub>/Nb test diodes (ARL)

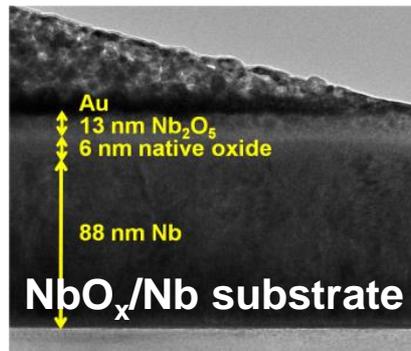


Al-Al<sub>2</sub>O<sub>3</sub>-Al test diodes



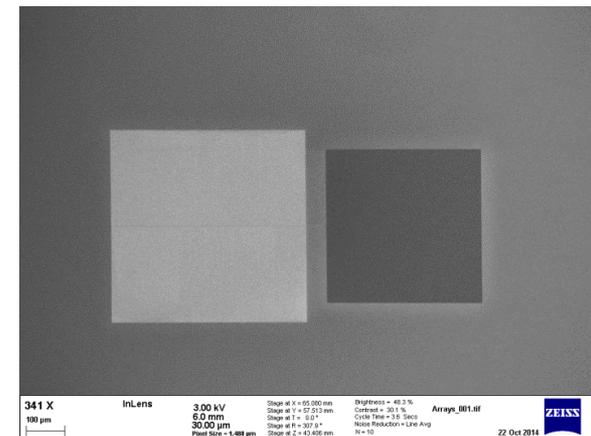
NSRDEC measurement, analysis, modeling

Pt/Nb<sub>2</sub>O<sub>5</sub>/(NbO<sub>x</sub>)Nb test diodes with various barrier (oxide) thicknesses



Derived material parameters for Pt/Nb<sub>2</sub>O<sub>5</sub>/(NbO<sub>x</sub>)Nb diodes:

- $\phi_+/\phi_- = 0.41/0.77$  eV
- $K = 6$
- $m_2 = 0.16 m_0$



Antenna-coupled Al-Al<sub>2</sub>O<sub>3</sub>-Al array



# (Micro) Rectenna Arrays for Infrared Power Conversion

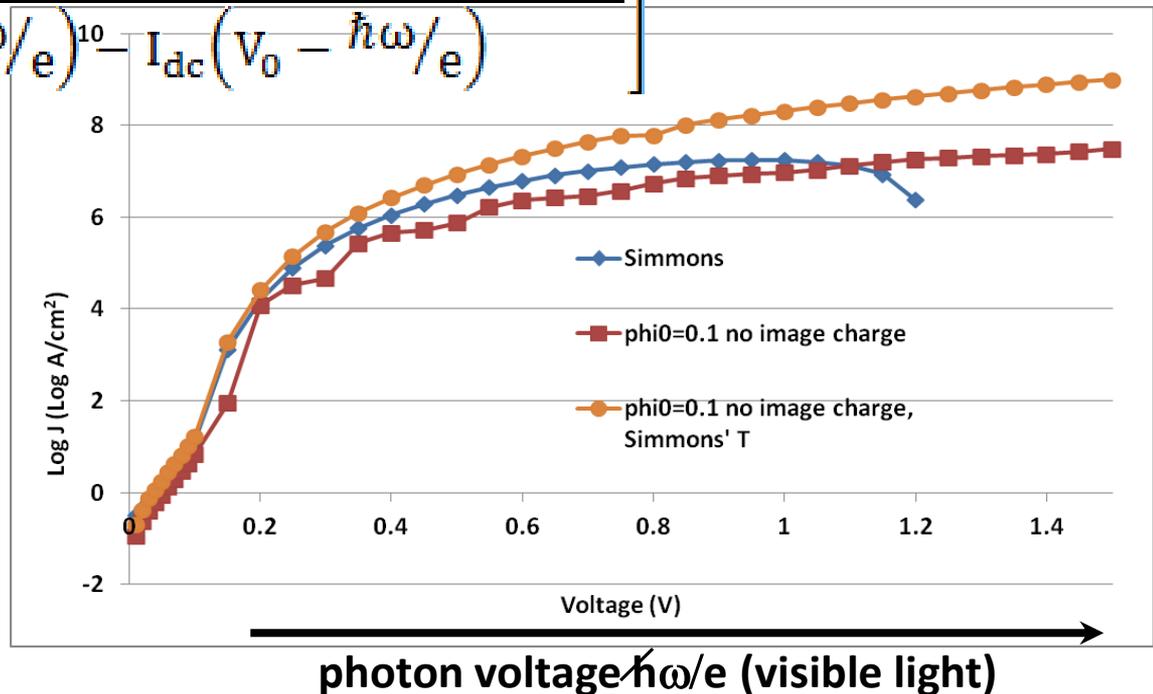


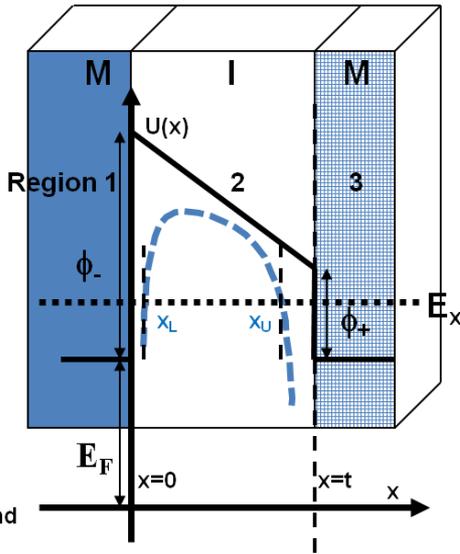
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## Vertical MIM diode rectifiers

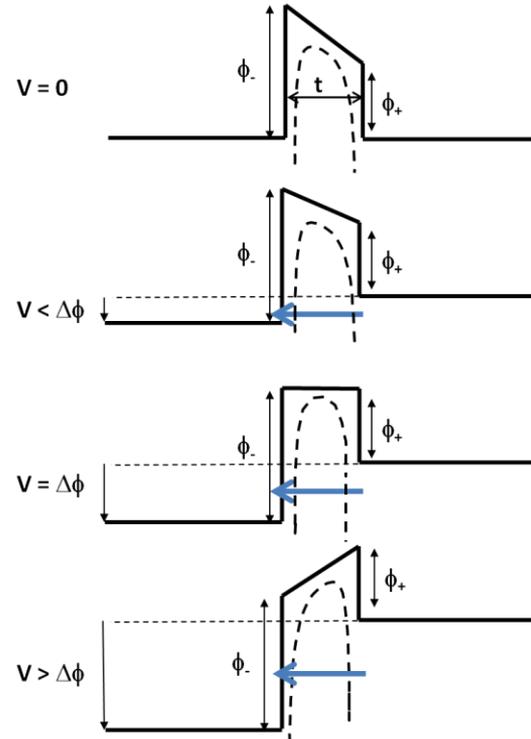
$$R_Q = \frac{e}{\hbar\omega} \left[ \frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e)^{10} - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

**Must model I-V curve to predict rectification responsivity (A/W), especially at high voltages for  $R_Q$ !**



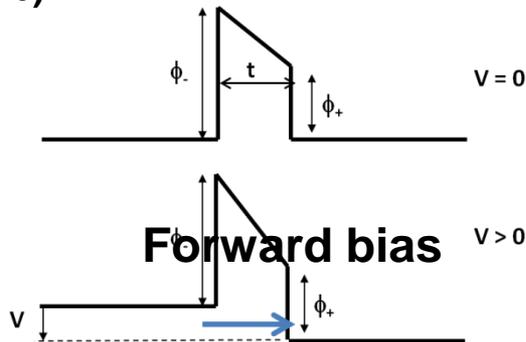


Barrier heights:  
 $\phi_+$ ,  $\phi_-$



Reverse bias

Osgood, Giardini, *et. al.*, JVSTA 34, 0151514 (2016)

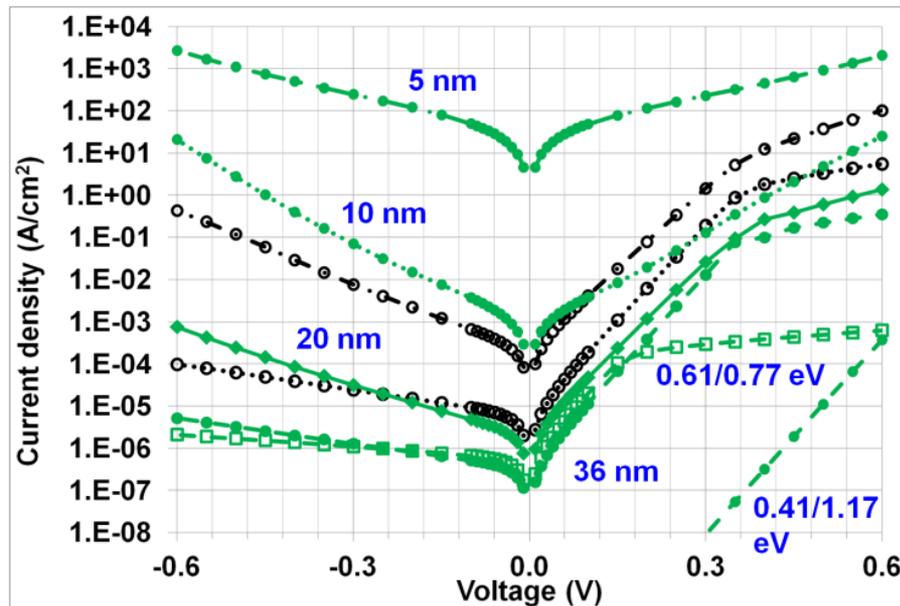
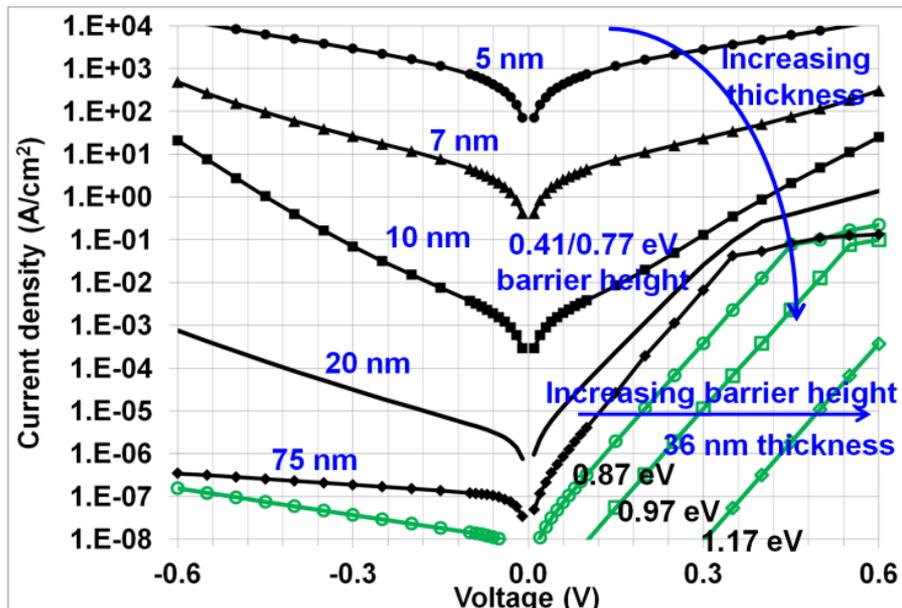


Forward bias

New physics in model

- Exact solution to trapezoidal potential barrier: no WKB approximation
- Principle of “equal action” to solve image force problem
- Effective mass not equal to electron rest mass
- Note convention: larger barrier on left

## Trends with thickness and effective mass



### Conduction and rectification in NbO<sub>x</sub>- and NiO-based metal-insulator-metal diodes

### Barrier heights in format: $\phi_+ / \phi_-$

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 Natick, Massachusetts 01760

Prakash Periasamy,<sup>b)</sup> Harvey Guthrey, and Ryan O'Hayre  
 Department of Metallurgical and Materials Engineering, Colorado School of Mines, Golden, Colorado 80401

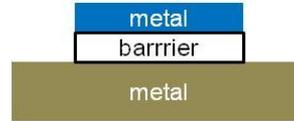
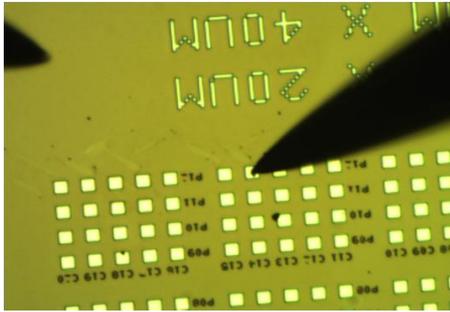
Matthew Chin, Barbara Nichols, and Madan Dubey  
 RF and Electronics Division, US Army Research Laboratory, Adelphi, Maryland 20783

Gustavo Fernandes, Jin Ho Kim, and Jimmy Xu  
 Division of Engineering, Brown University, Box D, Providence, Rhode Island 02912

Philip Parilla, Joseph Berry, and David Ginley  
 National Renewable Energy Laboratory, Golden, Colorado 80401

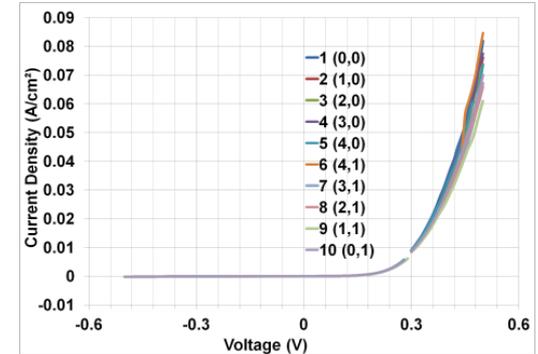
(Received 18 January 2016; accepted 1 August 2016; published 25 August 2016)

# Eleven orders of magnitude in current through NbO<sub>x</sub> – based diodes

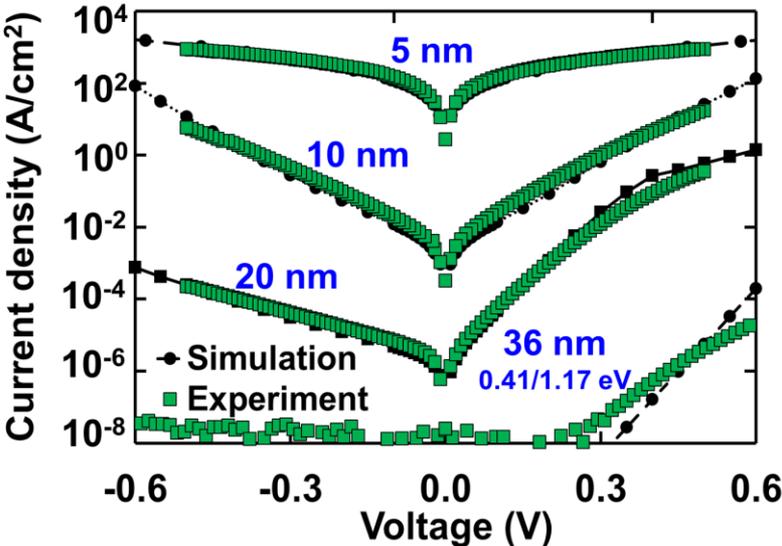


**ARL**

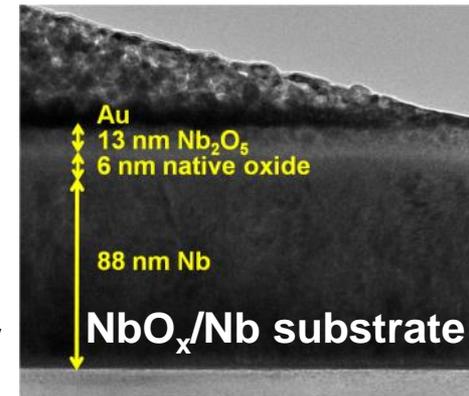
**Pt/NbO<sub>x</sub>/Nb test diodes (ARL)**



**NSRDEC measurement, analysis, modeling**



**Pt/Nb<sub>2</sub>O<sub>5</sub>/(NbO<sub>x</sub>)Nb test diodes with various barrier (oxide) thicknesses**



Barrier heights in format:  $\phi_+/\phi_-$

Derived material parameters for Pt/Nb<sub>2</sub>O<sub>5</sub>/(NbO<sub>x</sub>)Nb diodes:

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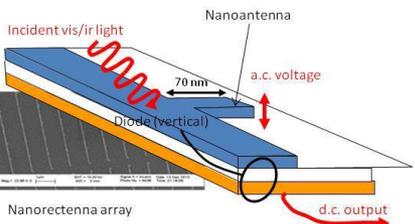


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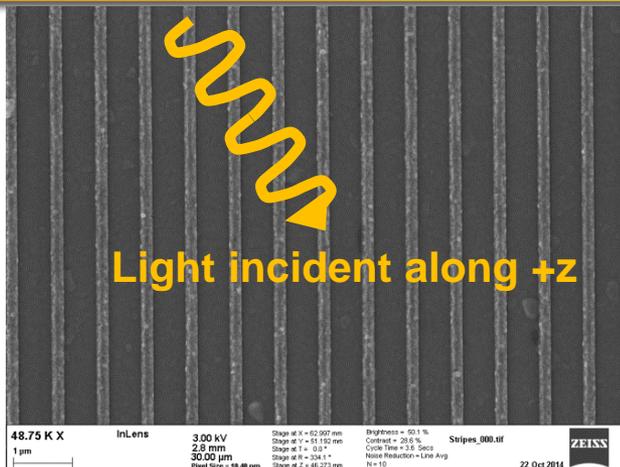
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# Stripe arrays exhibit cross-stripe resonances

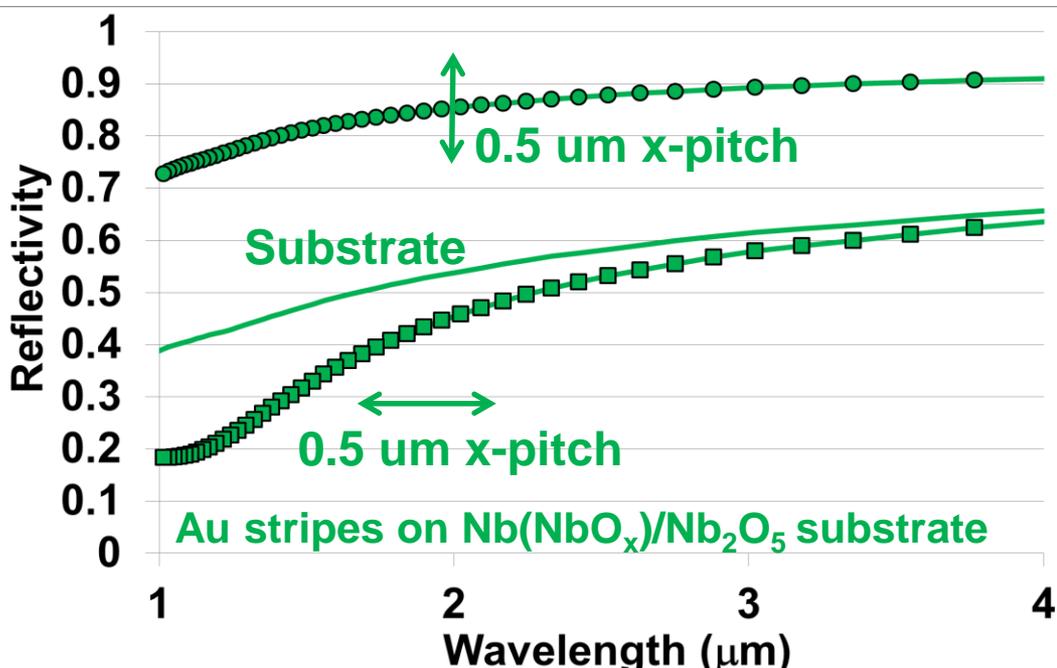
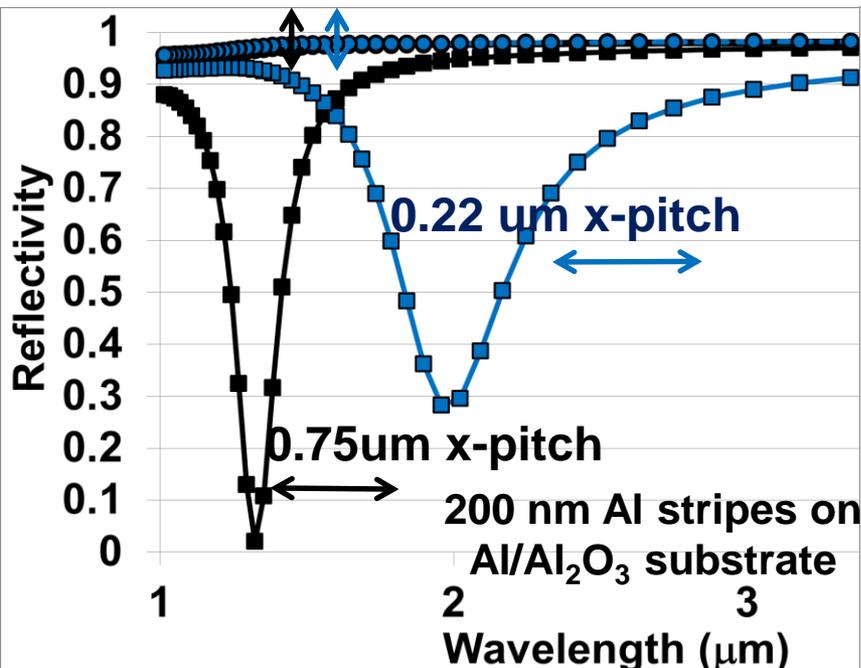
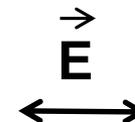


Microrectenna

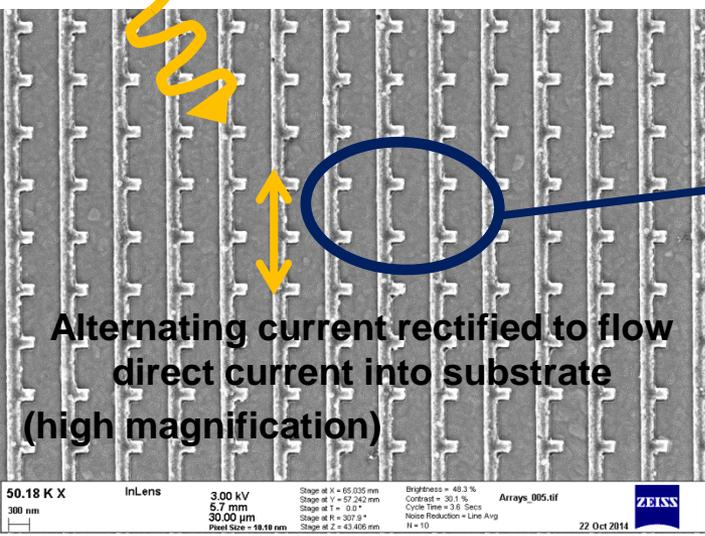
Top view of stripe array



Light incident along +z

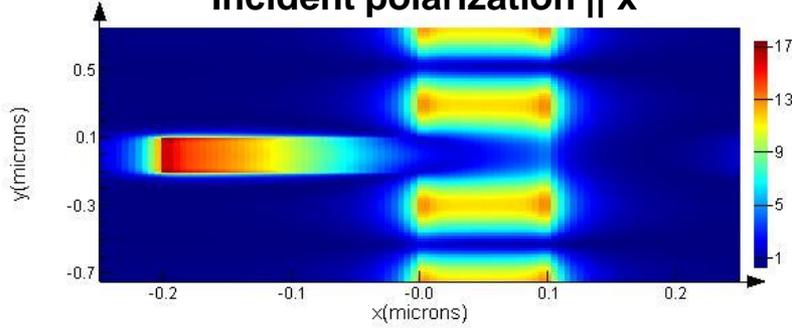


# Stripe-teeth resonances (Al-Al<sub>2</sub>O<sub>3</sub>-Al microrectenna arrays)

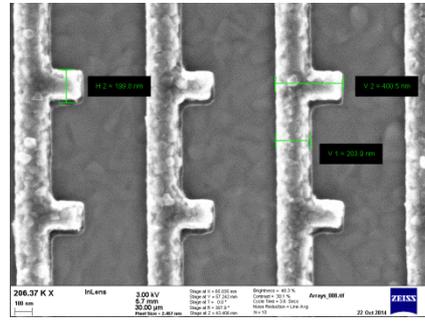


Alternating current rectified to flow direct current into substrate (high magnification)

2.25 μm resonance  
Incident polarization || x



“Teeth” add additional cross-stripe resonances!  
(dependent on teeth separation)

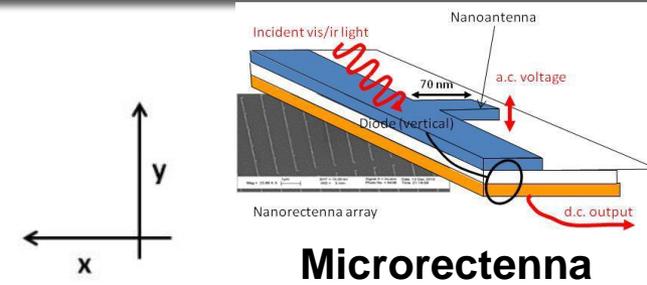


Top view

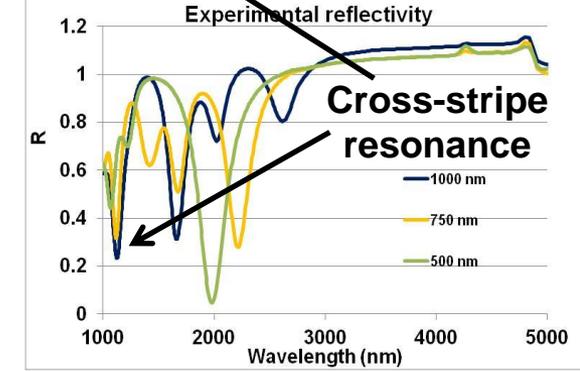
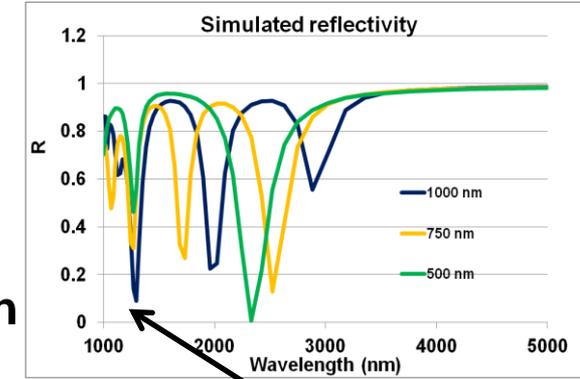
LINCOLN LABORATORY  
MASSACHUSETTS INSTITUTE OF TECHNOLOGY

US Army NSRDEC design

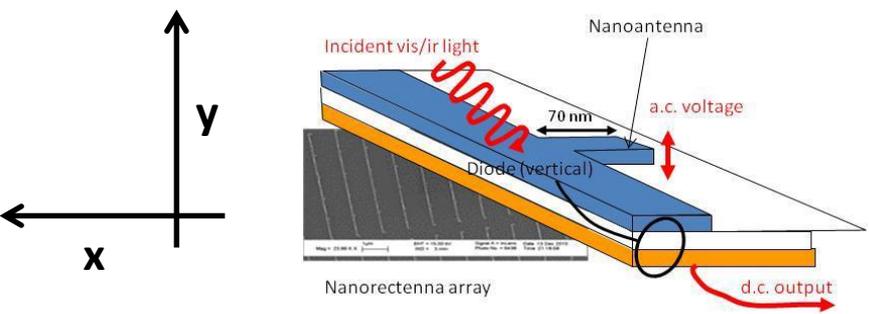
200 nm long Al teeth  
and stripes  
E || x



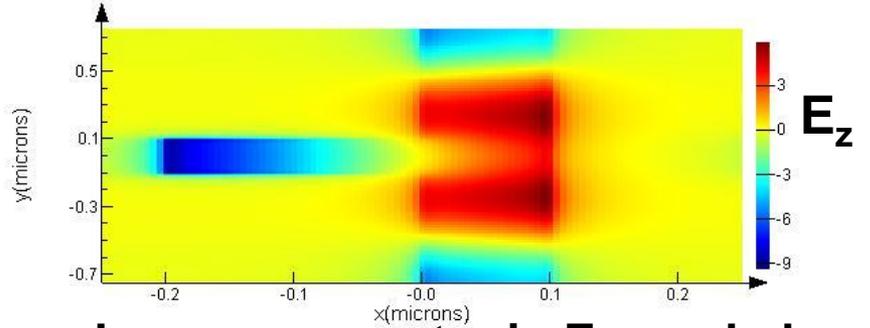
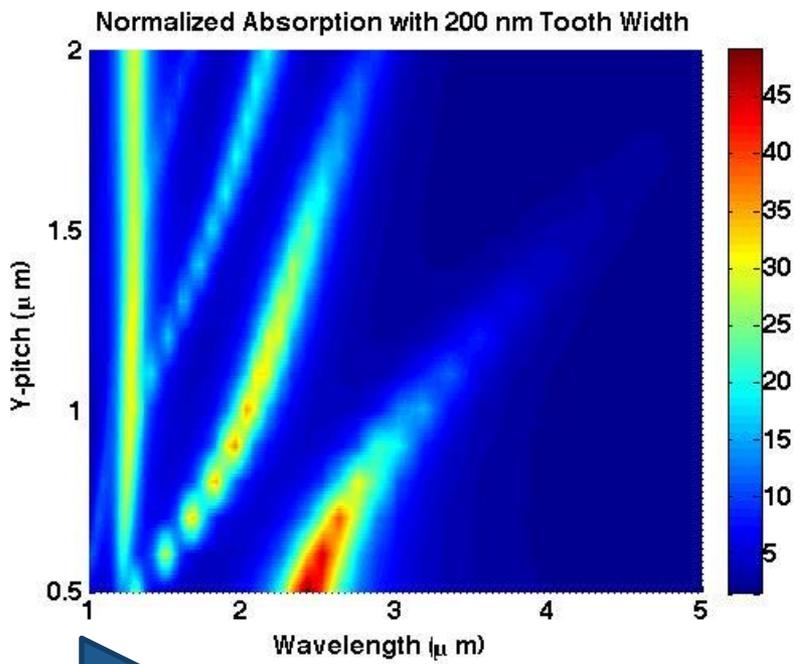
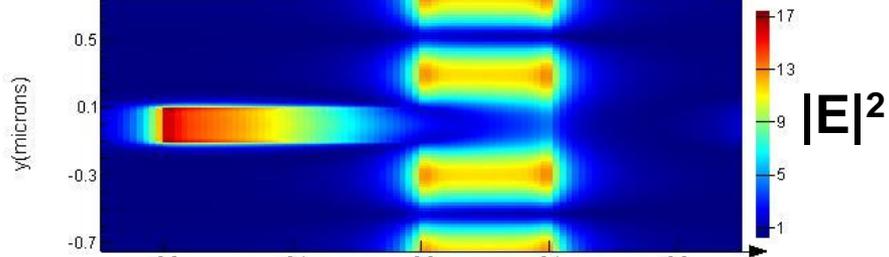
Microrectenna



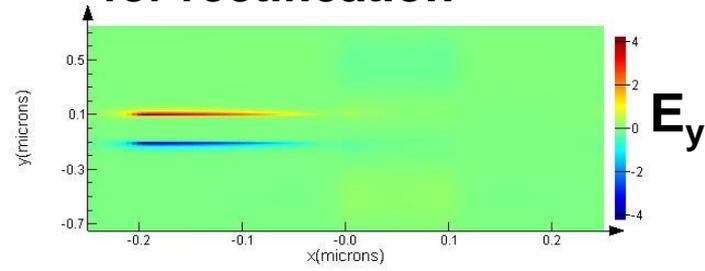
# Stripe-teeth resonances (Al-Al<sub>2</sub>O<sub>3</sub>-Al microrectenna arrays)



**2.25  $\mu\text{m}$  resonance**  
Incident polarization  $\parallel$  x

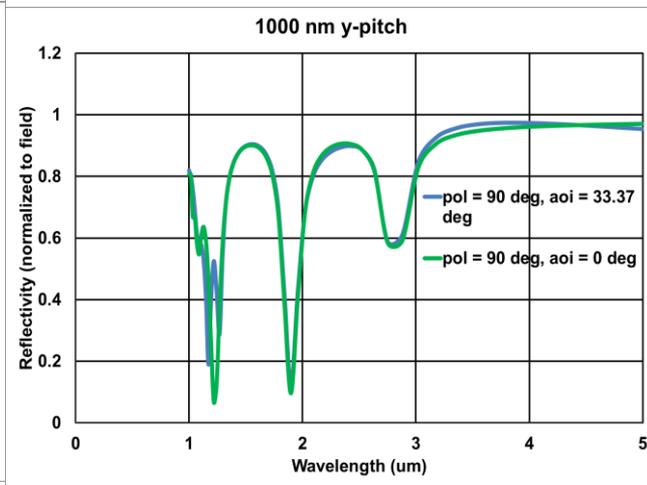
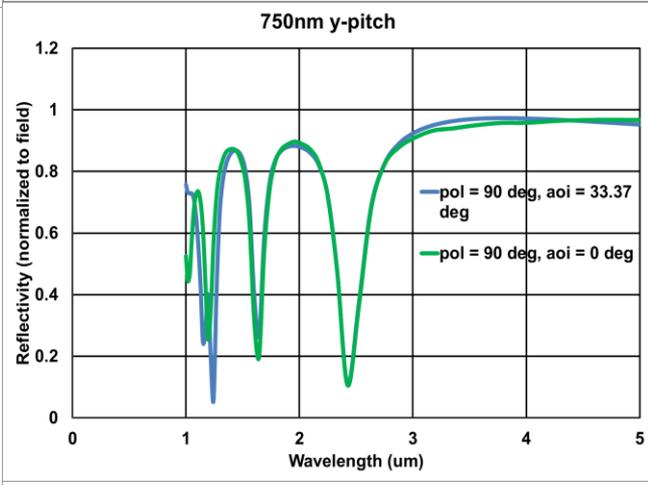
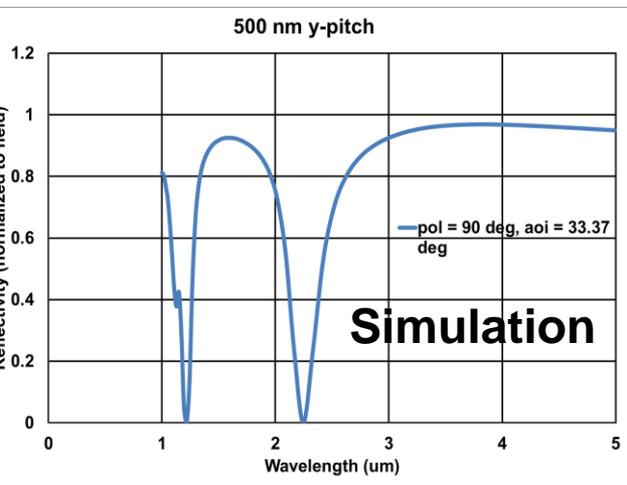
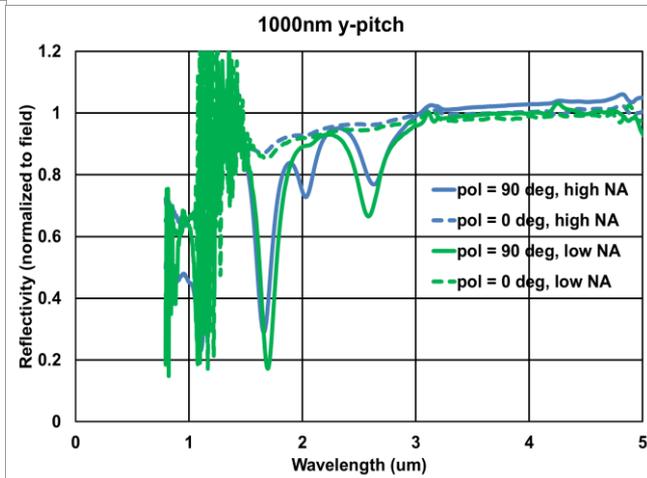
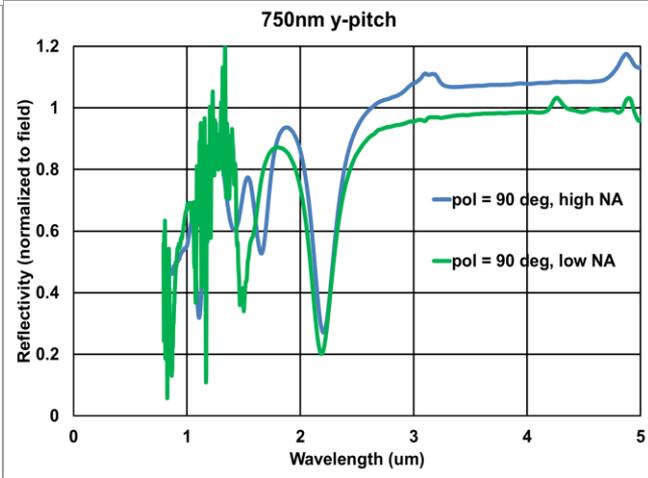
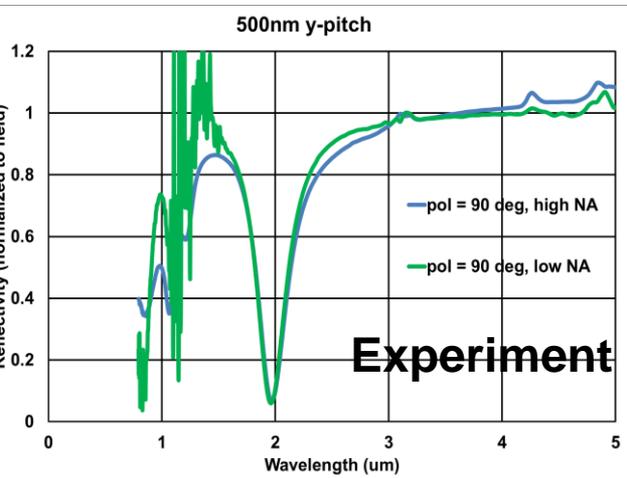


**Large asymmetry in  $E_z$  needed for rectification**



**Has very asymmetric  $E_z$ , but need stripes to extract current at resonance**

# Stripe-teeth resonances (Al-Al<sub>2</sub>O<sub>3</sub>-Al microrectenna arrays)



- **Good (not perfect) agreement between FTIR-measured spectra and simulated reflectivity. Insensitive to angle-of-incidence (to > 33°).**

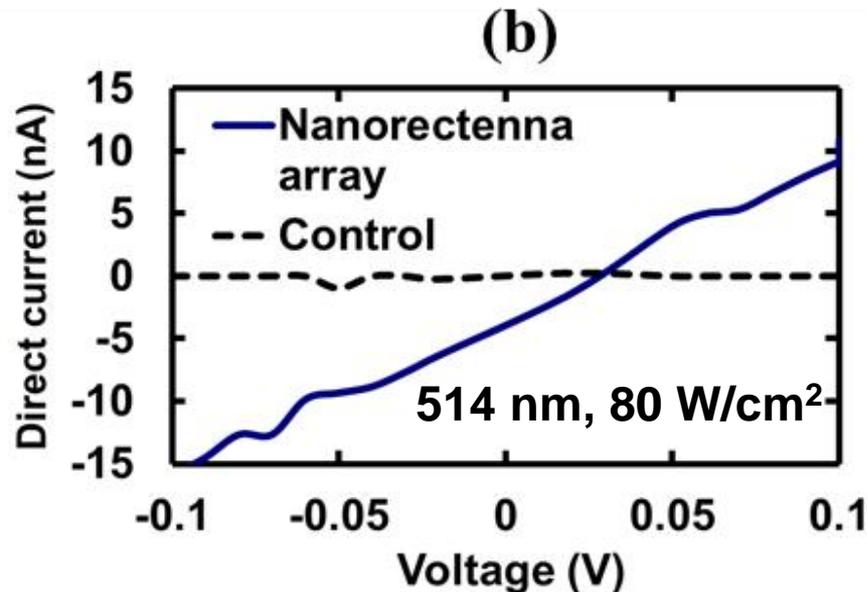
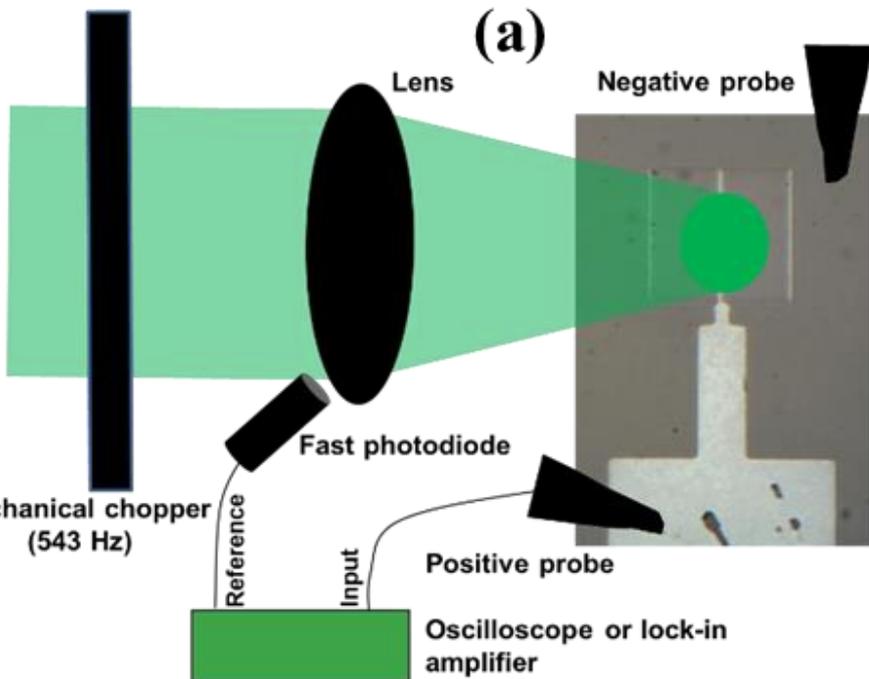


# Analysis of horizontal stripe-teeth arrays



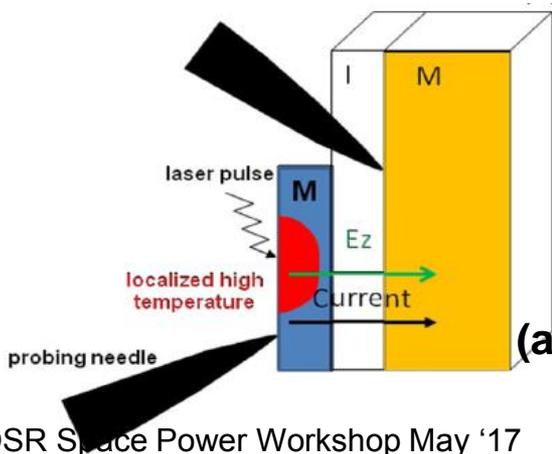
- **Designed for maximum asymmetry/non-linearity consistent with stripes to extract current**
- **Al-Al<sub>2</sub>O<sub>3</sub>-Al arrays have excellent quality and controlled resonances**
  - **Make broadband with chirped arrays**
  - **With “Au wire” responds to cw visible lasers**
- **Au/Ti-Nb<sub>2</sub>O<sub>5</sub>-NbO<sub>x</sub>-Nb has a lossier ground plane (Nb) and, while an excellent electronic-quality oxide, antenna resonances much broader and weaker**
  - **However there is an interesting response to cw lasers with small dimensions (“nanorectenna array”)**

# Nanorectenna array output power from cw laser illumination!

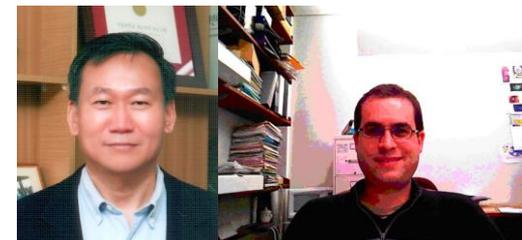


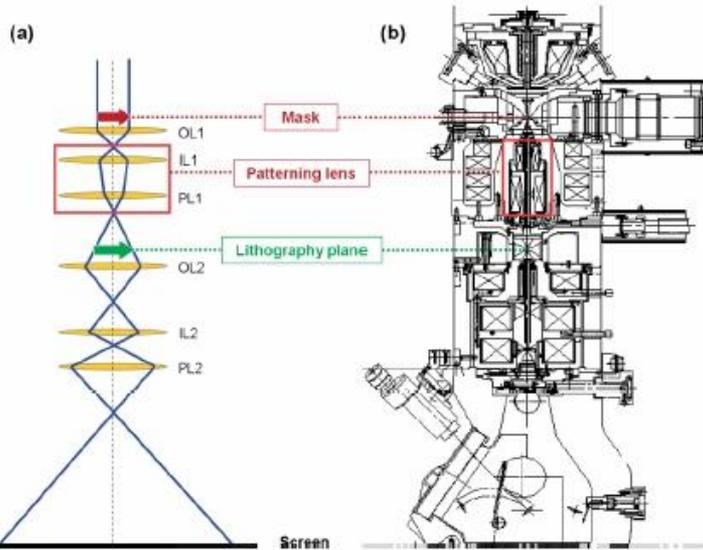
- 5 nA at zero volts - much higher than predicted from rectification responsivity (0.45 A/W maximum)!

NSRDEC measurement, analysis, modeling



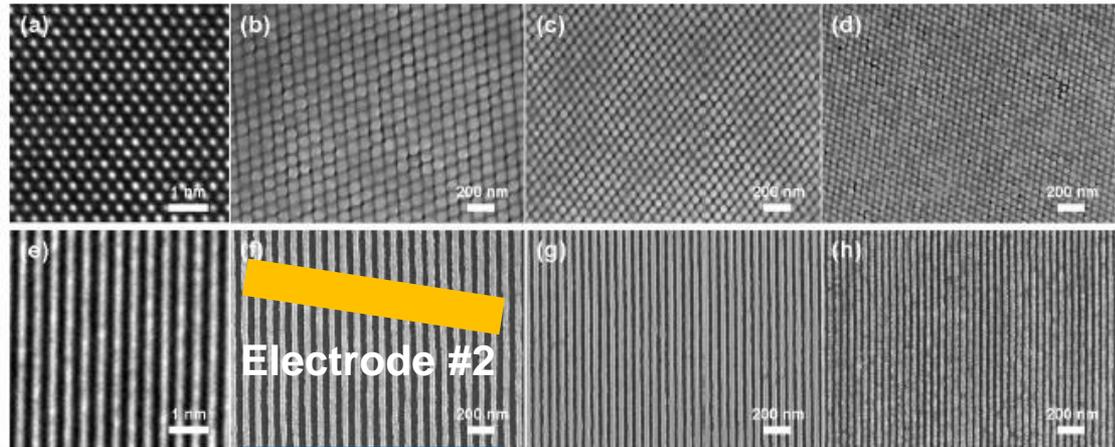
Photothermoelectric effect (antenna heated more than the ground plane)?





- Inverted Au/Al<sub>2</sub>O<sub>3</sub> (ALD)/Al stack
- Au wire antennas underneath Al electrode
- Regular, high-resolution arrays of lines and dots
- Unique nanopatterning approach

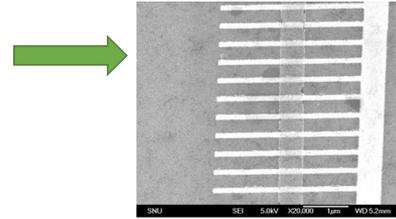
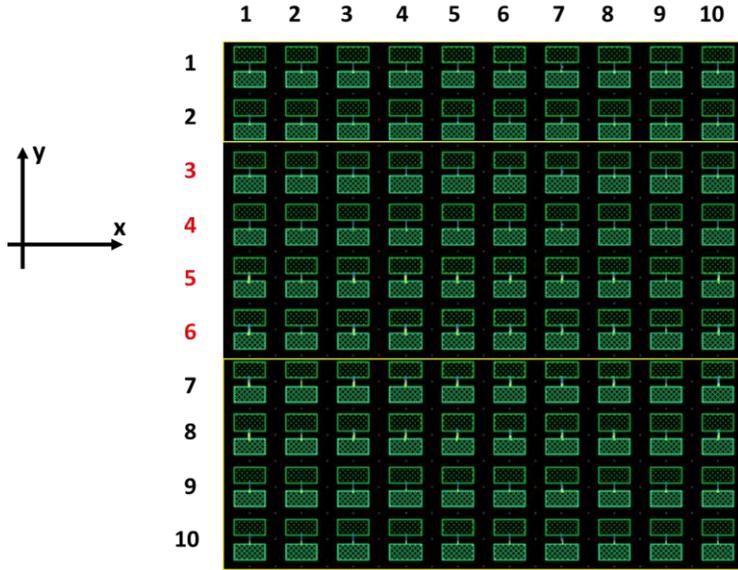
**Figure 1.** Schematic ray diagram and cross-sectional view of the present lithography system. a) Ray diagram of the basic lens system of image formation, which is composed of two different sets of OL, IL, and PL. The first set magnifies the sample image to the lithography plane with a magnification ranging from 50 to 300 times, while the second set further magnifies this image to the viewing screen. b) The specially designed hardware which was developed based on the modification of a 200 kV TEM equipped with a field emission gun (JEM-2010F, JEOL Ltd.).



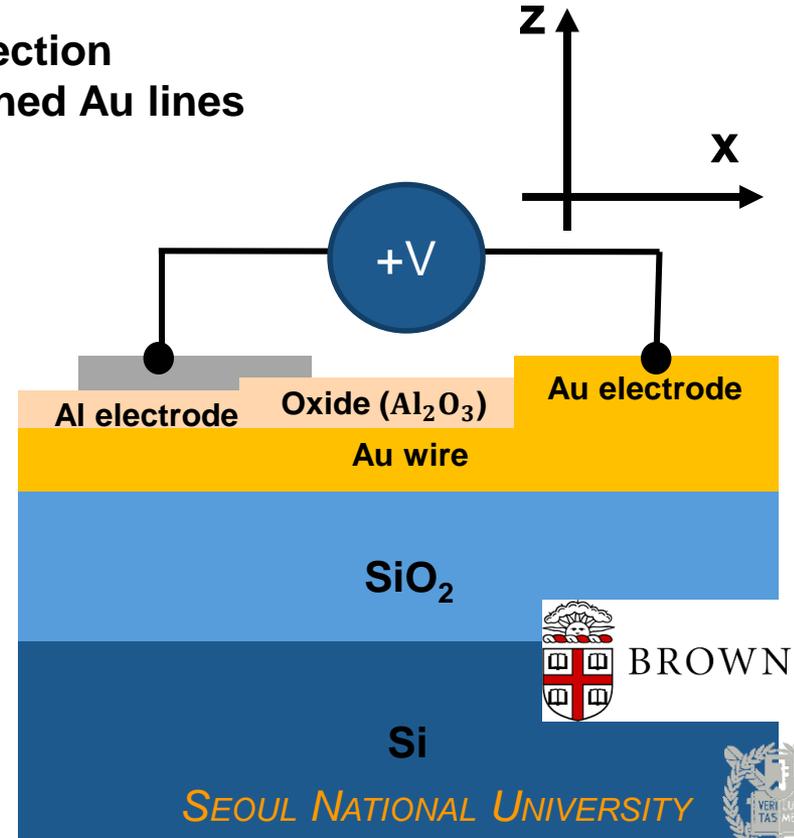
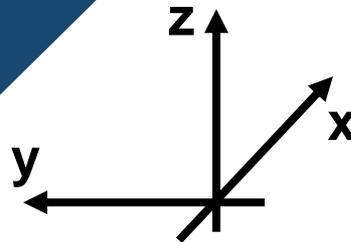
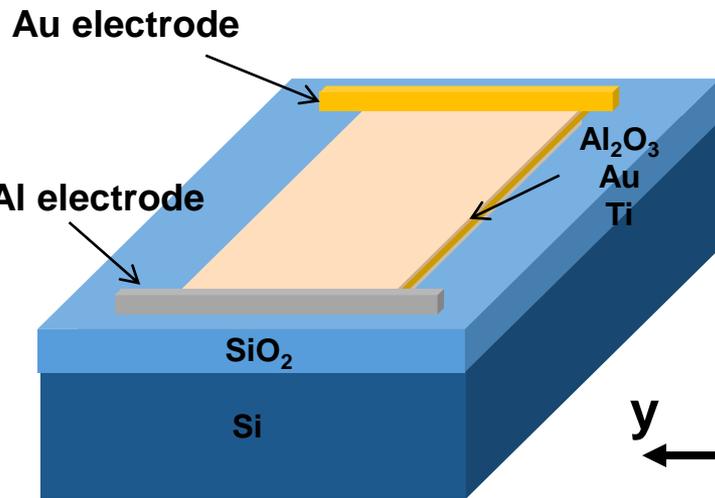
**Electrode #1**

**Vertical diode, horizontal antennas**

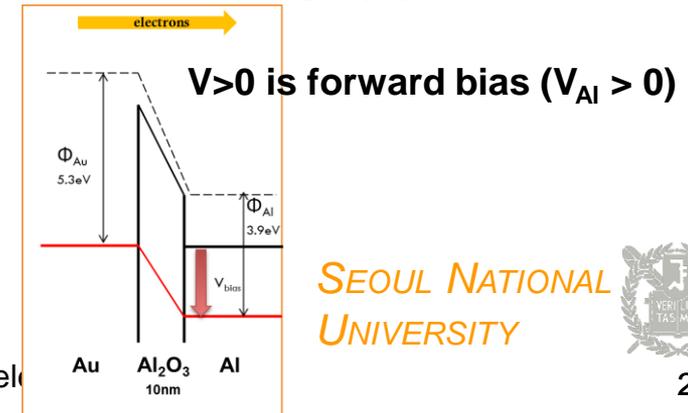
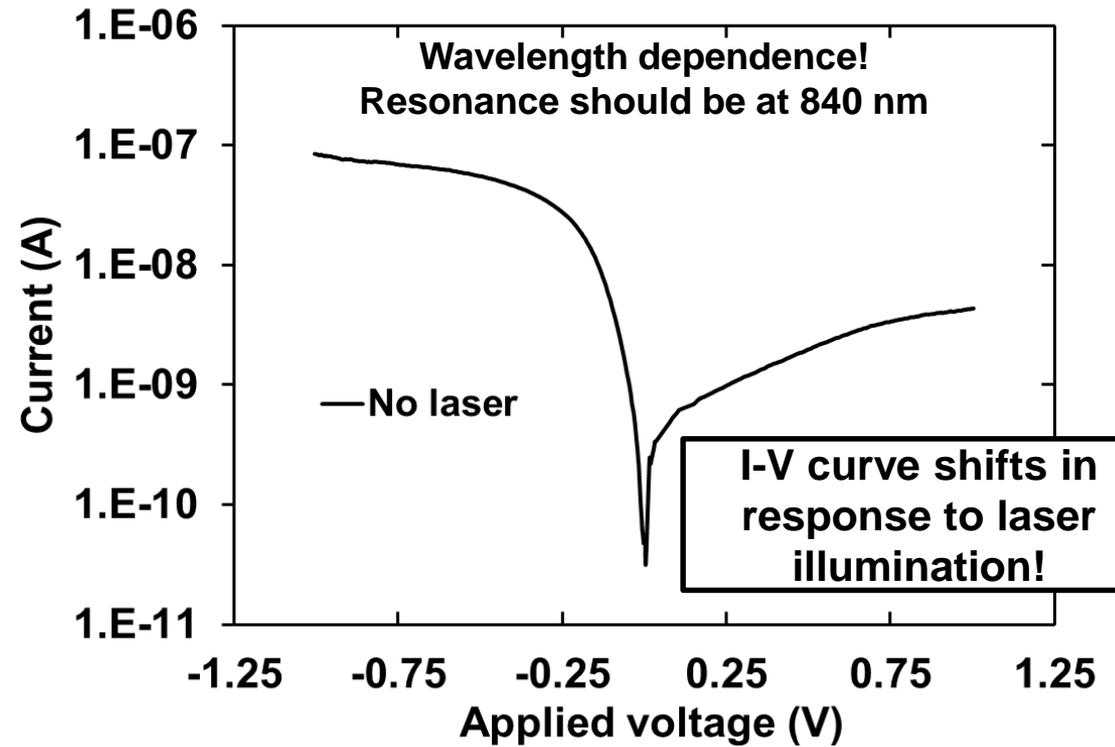
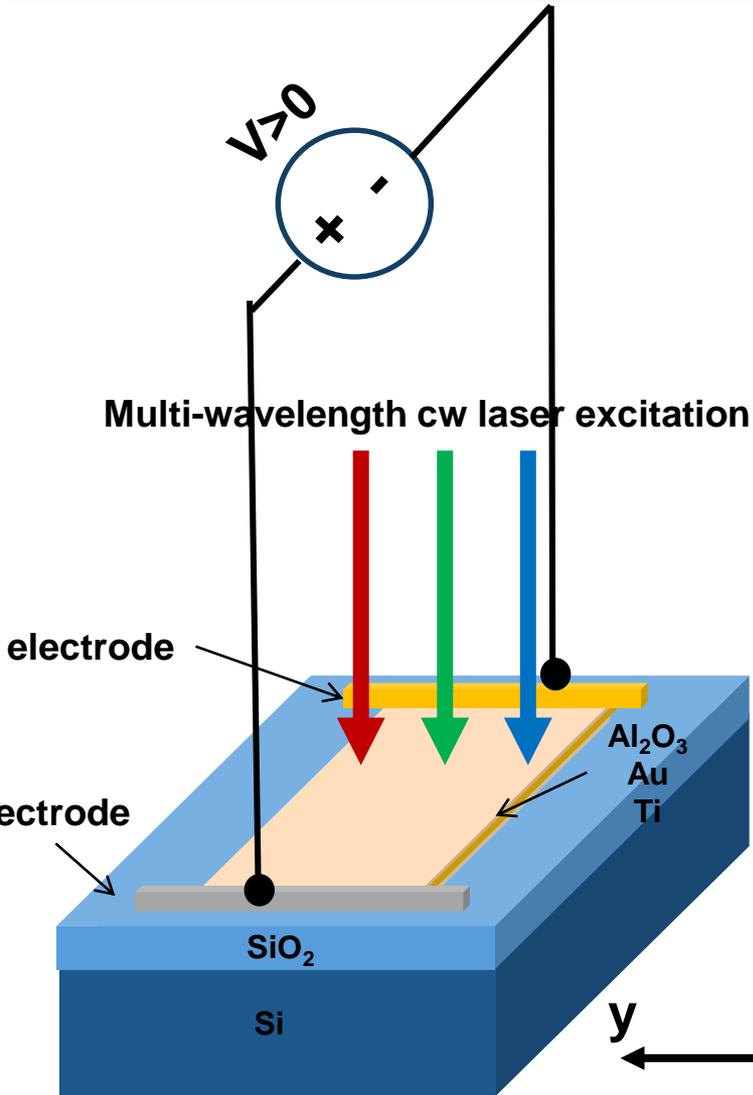
# Nanowire-based nanorectenna clusters



Projection  
nanopatterned Au lines

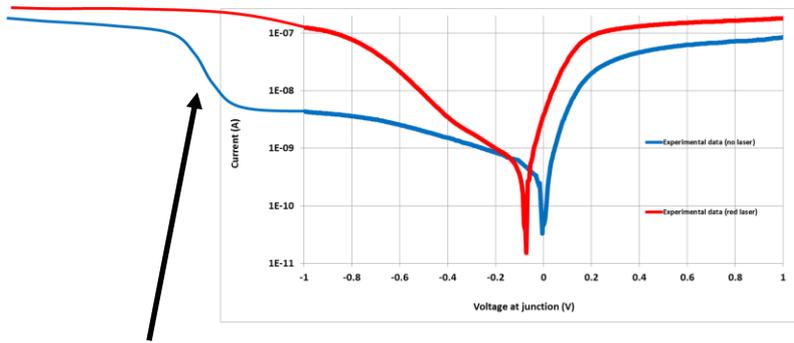


# Nanowire-based nanorectenna clusters



# Modeling Al-Al<sub>2</sub>O<sub>3</sub>-Au nanorectennas to explain data

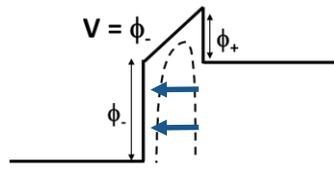
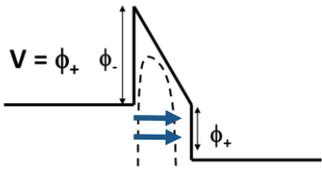
**Hypothesis I: steps in I-V curve are due to oscillations in transmission function through barrier layer in MIM diode, which are due to interferences in the transmission through the trapezoidal (image-modified) potential**



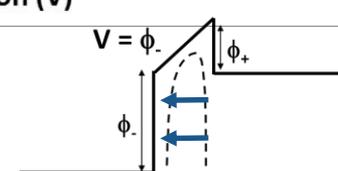
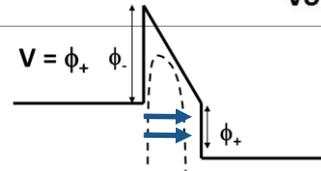
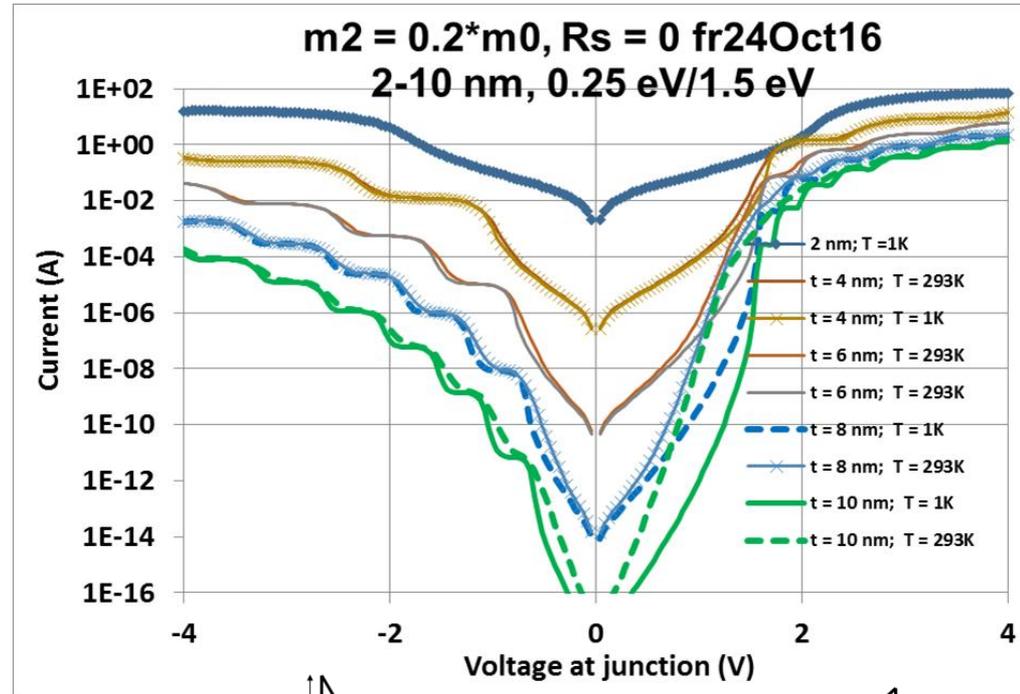
Hypothesized "step" in I-V curve

Forward bias

Reverse bias



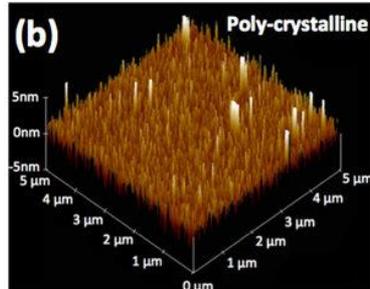
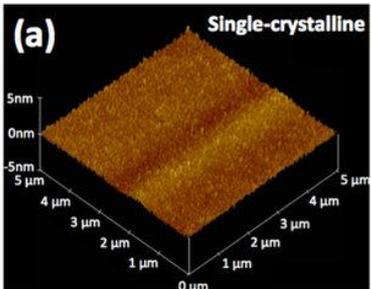
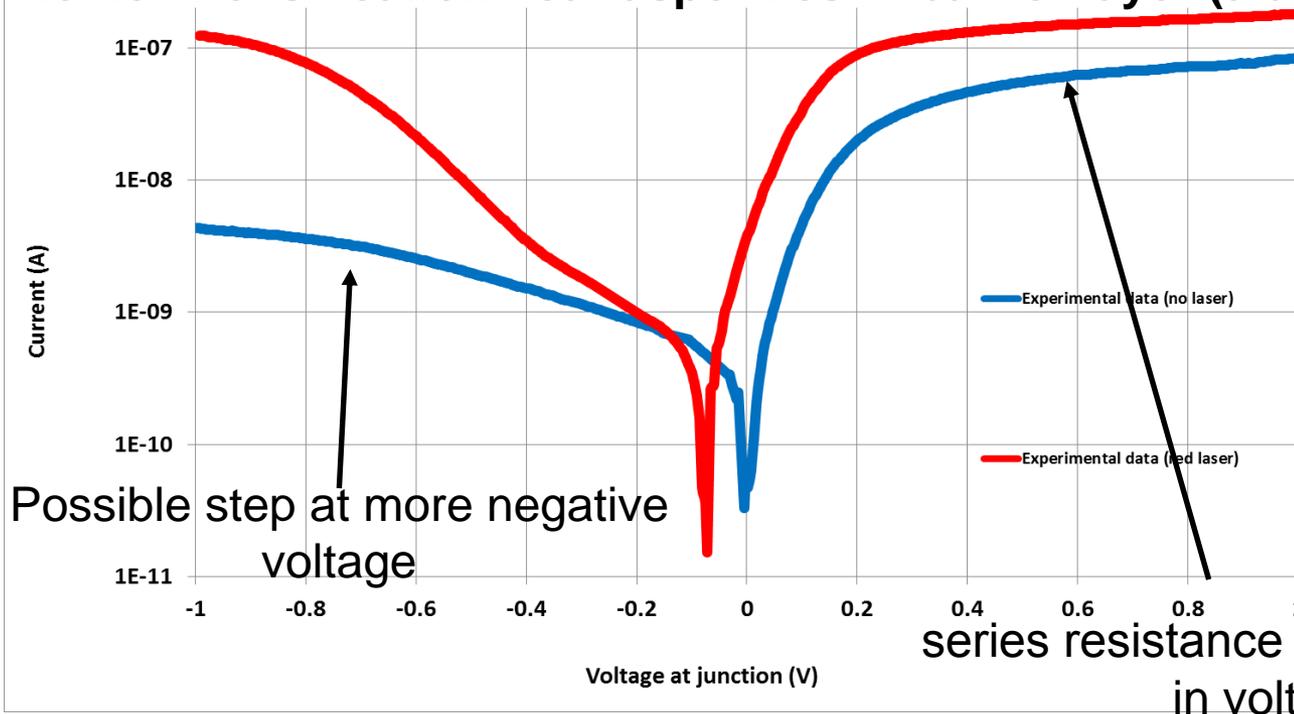
A few states below the Fermi level have tunneling transmission resonances across barrier into empty states (producing steps in the I-V curve at low temperatures), but  $V$  must be at least  $> \phi_+$  (for forward bias) and at least  $> \phi_-$  (for reverse bias)



2-10 nm thick barrier layer,  $K = 6$ , Temp = 293 K or 1 K

Note:  $V > 0$  is *reverse bias*

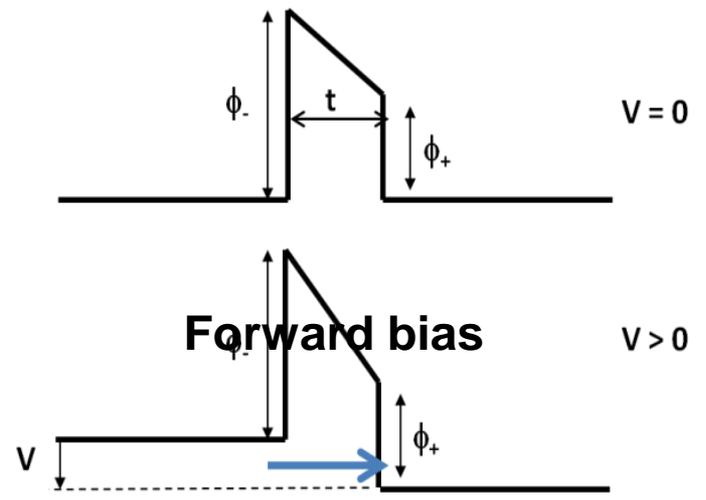
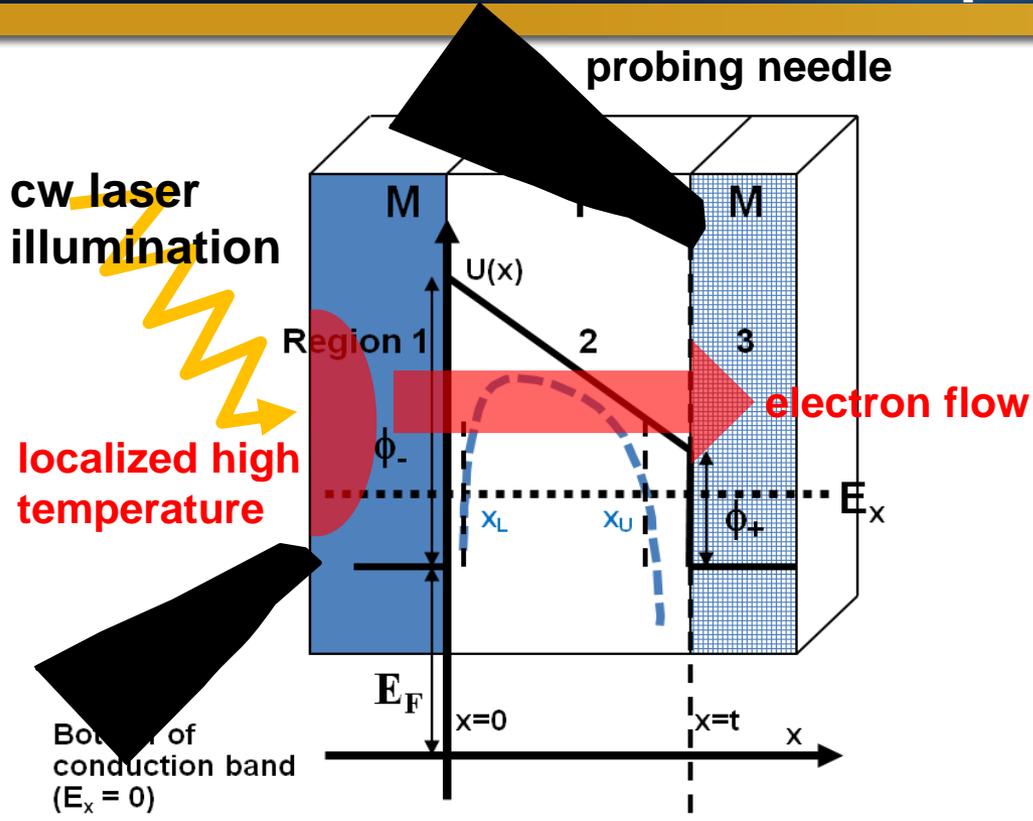
**Hypothesis II: Shift in J-V curve due to laser illumination may be due to field and plasmonic intensification near asperities in barrier layer (aluminum oxide)**



Other possibilities for large response to cw visible laser: rectification, charging

Note:  $V > 0$  is *reverse bias*; opposite from previous notation.

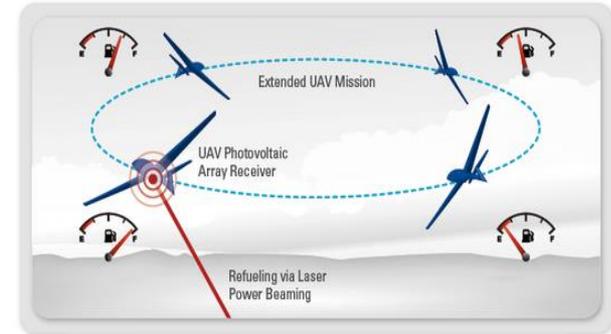
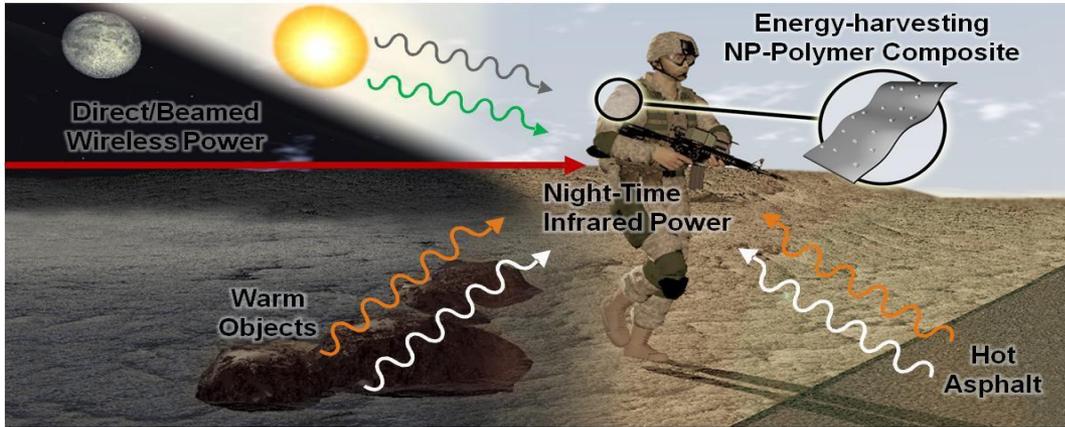
# MIM diode model improved to include temperature gradients



New temperature gradient in NSRDEC MIM diode model; regions 1 and 3 are at different temperatures. Barrier heights:  $\phi_-$  and  $\phi_+$ , where  $\phi_- > \phi_+$ .

- **Nonlinear rectifying metadevices create new opportunities (quantum and nonlinear plasmonics)**
- **Nb- and Al-based stripe-teeth metamaterial arrays designed and analyzed**
  - Both have cross-stripe resonances
  - Au/NbOx/Nb: broad, weak resonances
  - Al/Al<sub>2</sub>O<sub>3</sub>/Al: well-controlled absorption spectrum
    - Standing wave resonances dependent on y-pitch
    - Angle of incidence has little effect to at least 33 deg.
  - J-V curves for Ag(Ti)/NbOx/Nb show  $\phi/\phi_+ = 0.41/0.77$  eV
  - J-V curves for Al/Al<sub>2</sub>O<sub>3</sub>/Au show  $\phi/\phi_+$  reduced
    - Curves shift with focused laser – due to field enhancement from AlOx roughness, photoemission/charging, and heating effects
    - “Steps” in I-V?
    - Rectification responsivity predicts shift due to laser illumination?
- **Large direct current at  $V = 0$  from Ag(Ti)/NbOx/Nb and Al/Al<sub>2</sub>O<sub>3</sub>/Au microrectenna arrays much larger than predicted by classical and quantum rectification formulas**
  - Rectification or photothermoelectric effect?
  - Are steps in MIM diode I-V curves possible?

- A new early applied program on narrowband infrared rectenna arrays starting in FY17.
- Proof-of-concept experiments (lab-scale demonstrations) will be carried out for power and data beaming.



Potential application: Wireless power/data transfer/communications (Warfighter/Soldier/Squad and/or UAS sustainment)

Enhanced thin-film photovoltaics

Potential future application:  
Solar blankets and/or  
military shelters

