

(Micro) Rectenna Arrays for Infrared Power Conversion



Dr. Richard Osgood, Mr. Stephen Giardini, Dr. Yassine Ait El Aoud, Ms. Diane Steeves, Mr. Dennis Magnifico

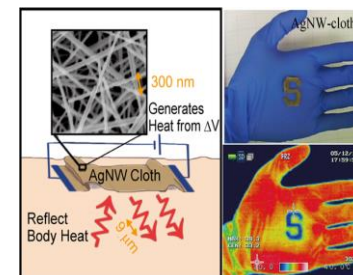
US Army Natick Soldier Research, Development, and Engineering Center



Drs. Lalitha Parameswaran, Mordechai Rothschild, Vladimir Liberman
MIT Lincoln Laboratory

Prof. Jimmy Xu, Dr. Gustavo Fernandes, Mr. Declan Oller, Dr. Jin Ho Kim
Brown University

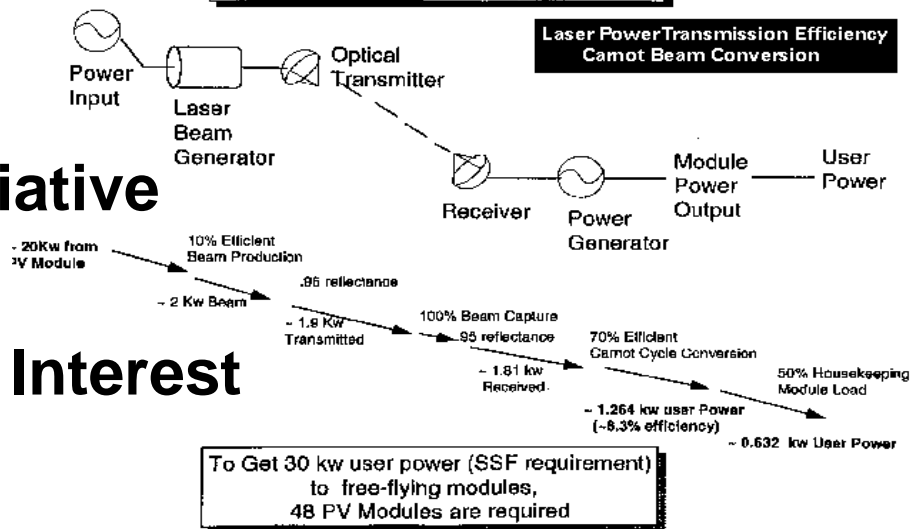
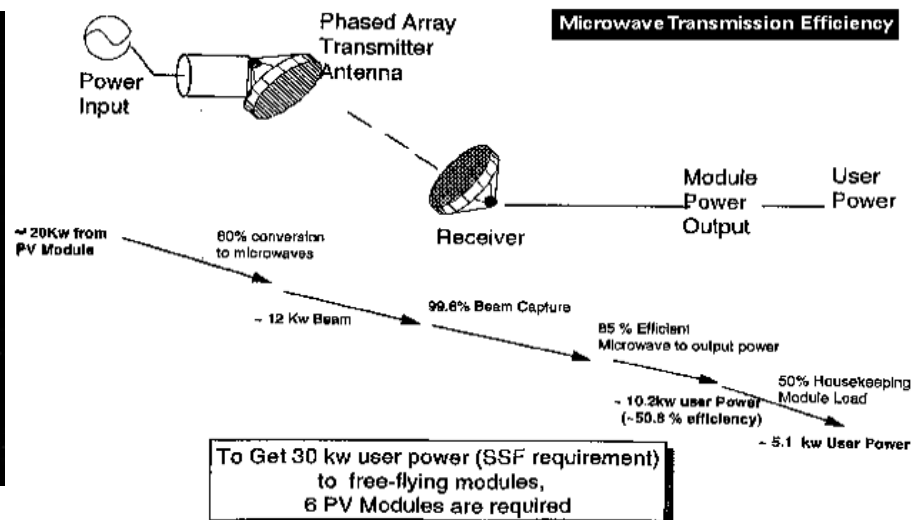
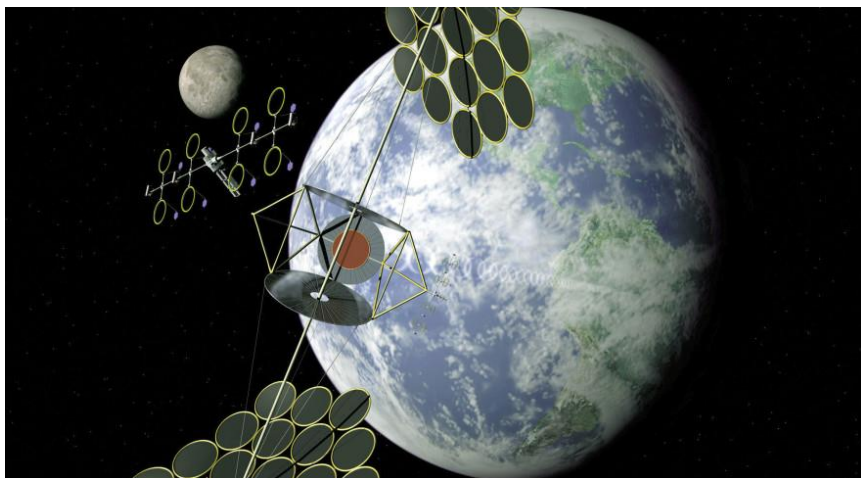
Prof. Ki-Bum Kim, Ms. Min-Yi Kang*
Seoul National University, Republic of Korea



Mr. Mathew Chin, Dr. Madan Dubey, Dr. Barbara Nichols
Army Research Laboratory (ARL) – Sensors and Electron Devices Directorate

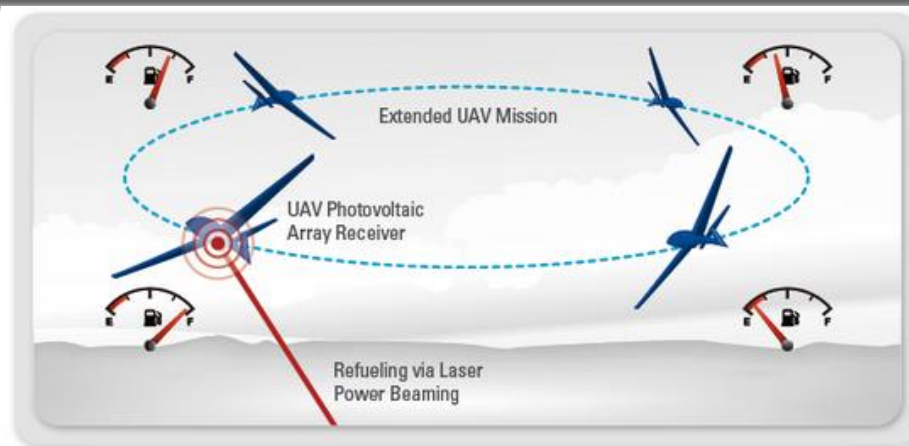


Rectenna Arrays for Infrared Power Conversion – Power Beaming in Space



- Space Solar Power Initiative
- Solar Power Satellite
- Japanese Government Interest
- Also Infrared Sensing

• UAS sustainment



Resonant Infrared Wavelengths – Converted to Signal

Non-Resonant Wavelengths Rejected

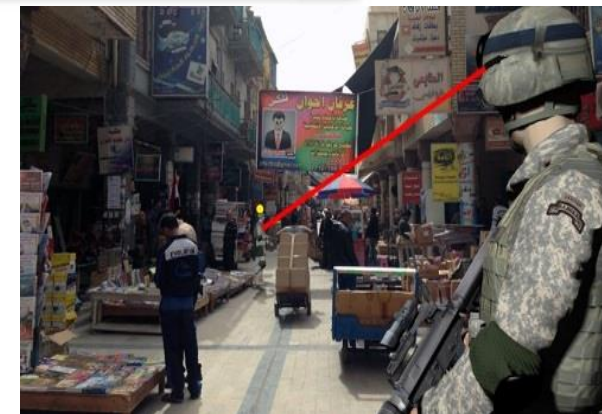
Tuned infrared detectors detect preferred wavelength band from friendly sources

- Communication
- Combat ID
- Use wavelengths undetectable to standard commercial detectors

• Challenges: Requires line-of-sight, laser sources, and research on devices and efficient power/signal transfer

Microrectenna Response

Output Current vs Frequency



Other applications: Battlefield Data Transfer and Identification

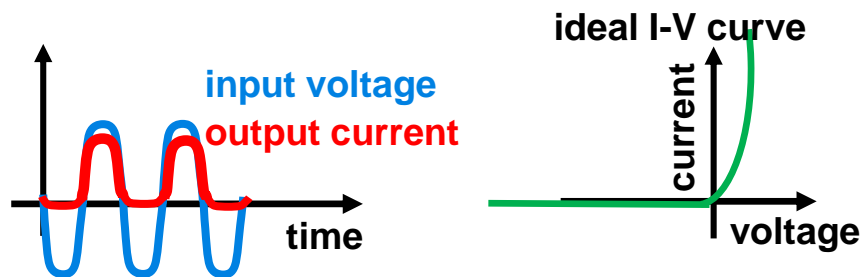


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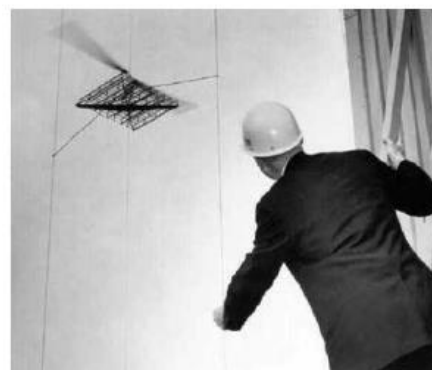
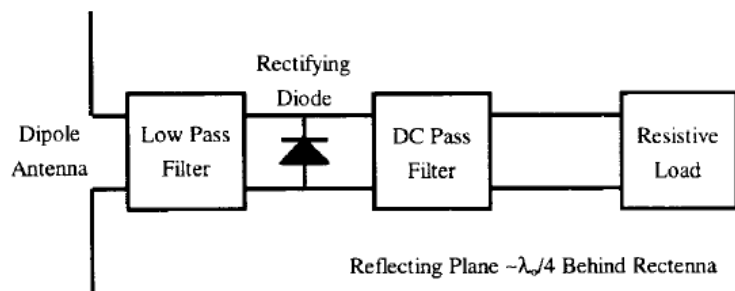
(Micro) Rectenna Arrays for Infrared Power Conversion



- **What are microrectennas and microrectenna arrays?**
- **Materials for microrectenna arrays**
- **Vertical MIM diode rectifiers**
 - J-V curve experiments and modeling
 - Estimation of responsivity and direct current
- **Horizontal stripe-teeth metamaterial arrays**
 - Design and fabrication
 - Analysis
 - Response to cw lasers



Diode rectification
(assumes ideal, highly non-linear I-V curve)



Dr. W. C. Brown, Raytheon Corporation (1964)

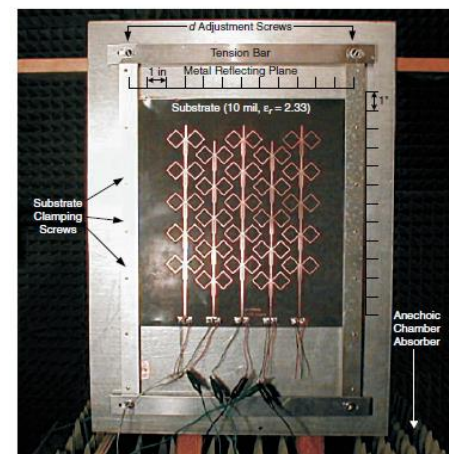


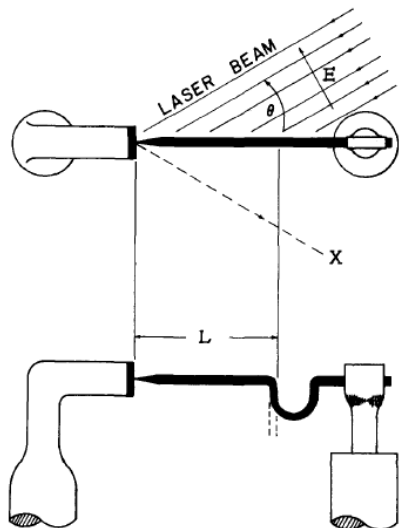
Figure 9. 5.61-GHz circular polarized printed rectenna with over 78% efficiency [38].

>75% efficient 5.61 GHz
rectenna array (TAMU) – IEEE
Microwave Journal (2002)

McSpadden et. al., IEEE Trans. Microw.
Theory Tech. v. 46 p.2053 (1998)

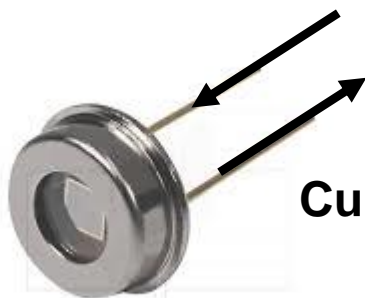
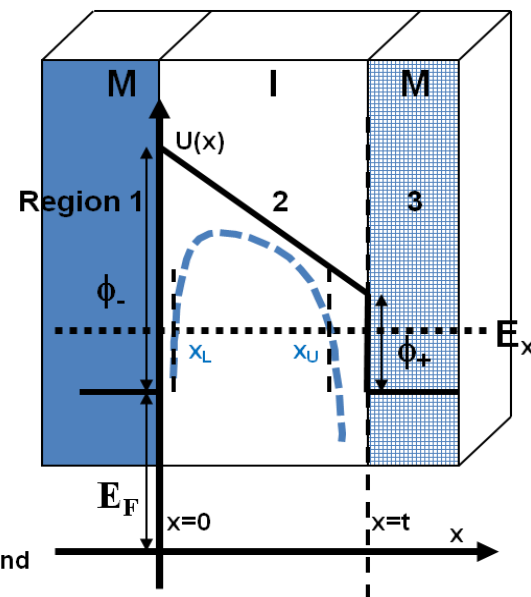
$\eta > 80\%$ for 5.8 GHz!

- Accurate measurements of infrared/visible frequencies



**Point-contact devices
(1960s and 1970s)**

“Improved coupling to infrared whisker diodes by use of antenna theory” Matarrese and Evenson, Appl. Phys. Letts. 17, 8 (1970)



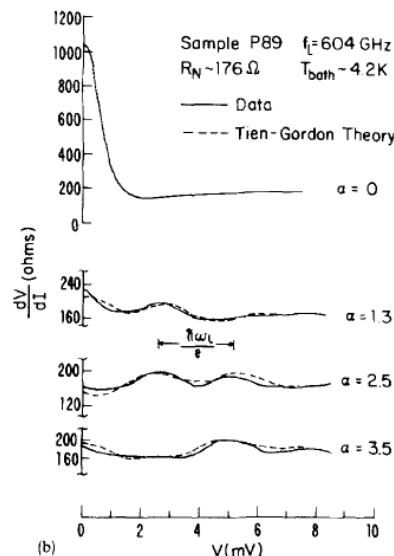
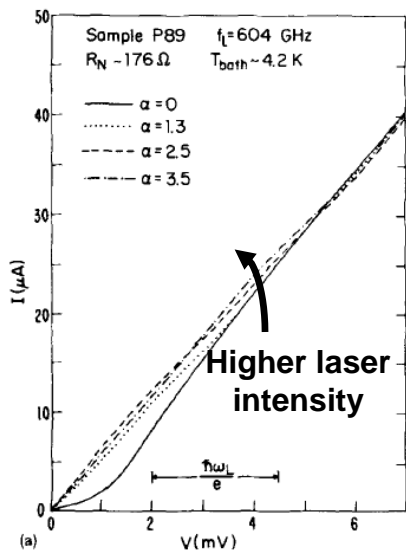
Current in Amperes

Responsivity R in A/W [1/V]

Radiative power in Watts

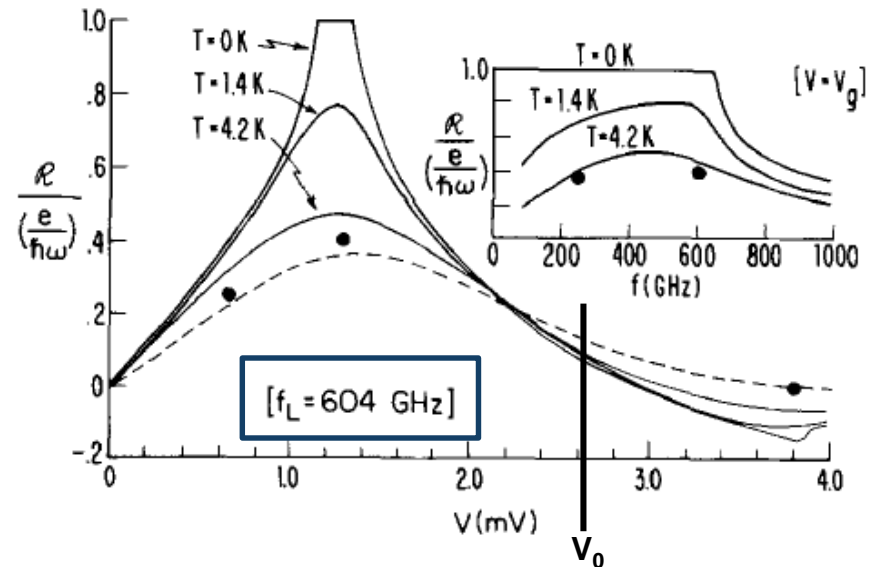
Responsivity of Metal-Insulator-Metal (MIM) Diodes

- Tinkham: Responsivity of Superconductor – Insulator – Superconductor/Normal junctions (1982)



Steps in dV/dI separated by photon voltage = (photon energy)/e

$$\alpha = V_{AC}/\text{photon voltage}$$



$$R_Q = \frac{e}{\hbar\omega} \left[\frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e) - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

Rectification responsivity
 R_Q in A/W

Quantum responsivity of MIM diodes

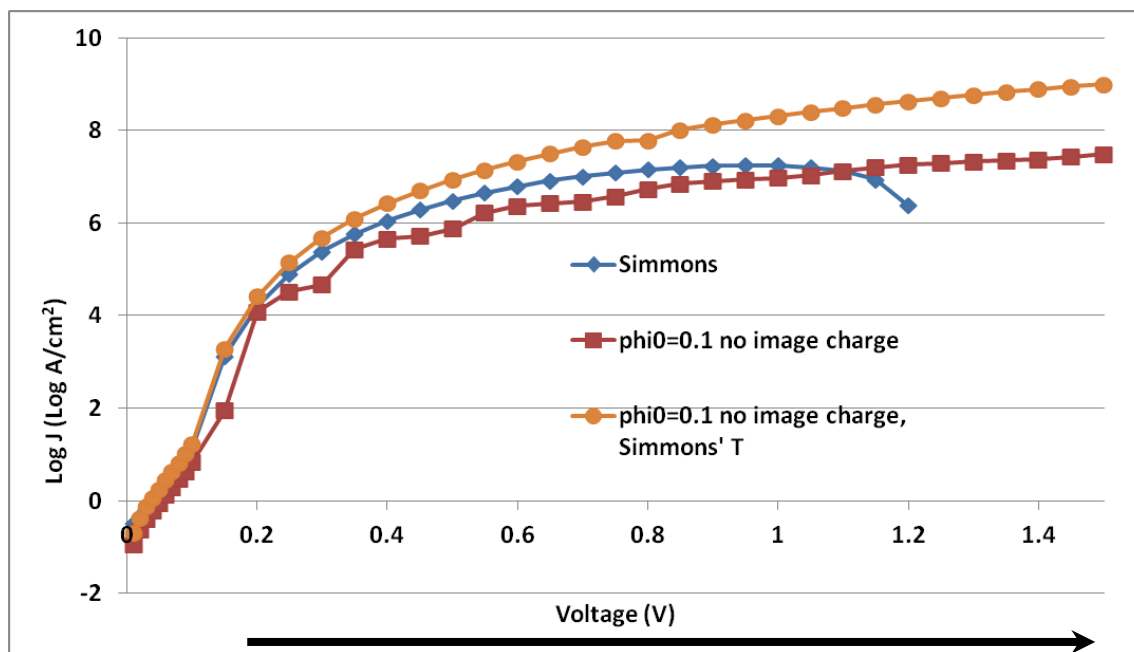
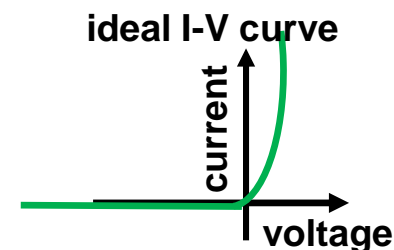
$$R_Q = \frac{e}{\hbar\omega} \left[\frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e) - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

0.45 A/W maximum
for green light
(higher in infrared)

➔
$$= \frac{1}{2} \frac{\partial^2 I_{dc} / \partial^2 V}{\partial I_{dc} / \partial V} \Big|_{V=V_0}$$

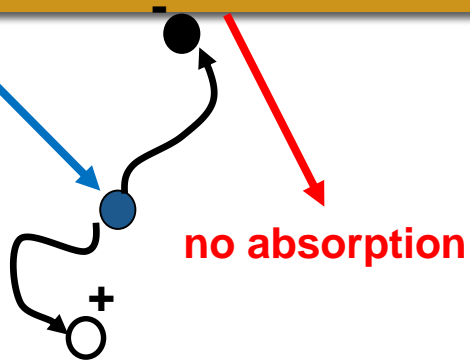
Approximation!
Valid only in
classical case

**Must model I-V curve
to predict rectification
responsivity (A/W),
especially at high
voltages for R_Q !**



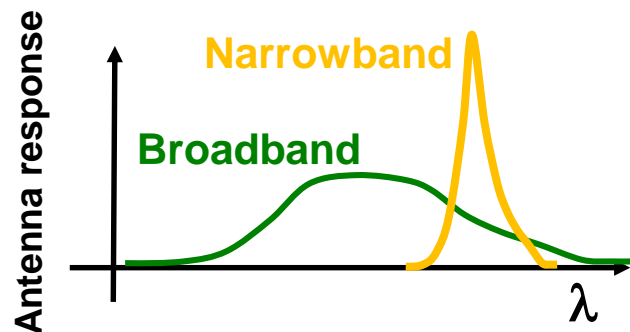
photon voltage $\hbar\omega/e$ (visible light)

What are microrectennas and microrectenna arrays?

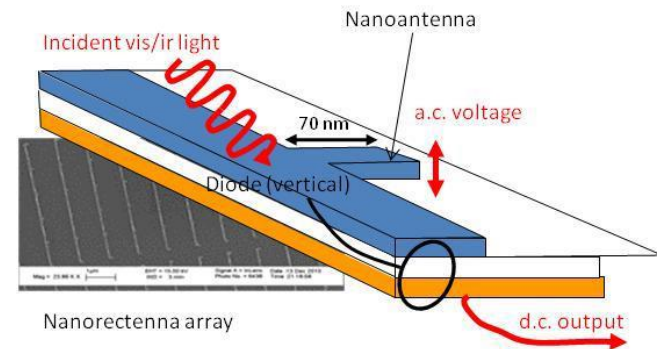


Photovoltaic (electron-hole generation with semiconducting bandgap)

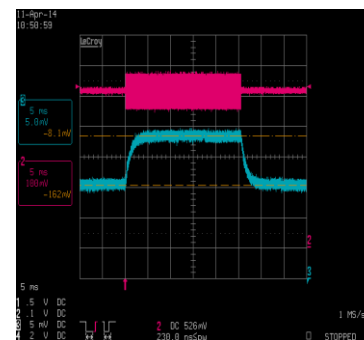
PV doesn't absorb photon energies less than bandgap



Dependent on dimensions and conductivity (no bandgap)



Perspective view of microrectenna



$$\Delta I_{dc} * 1 \text{ M}\Omega$$

Simple rectification verification
at 1 MHz
(NbOx – based diode)



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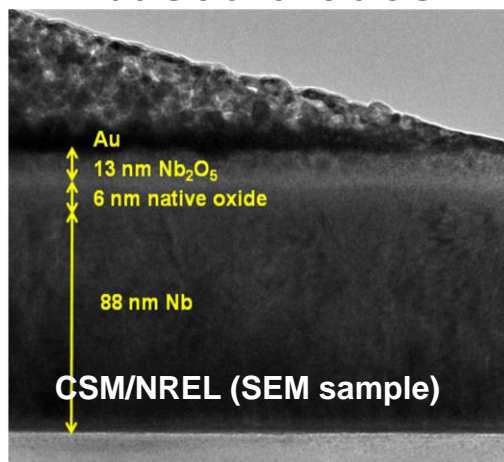
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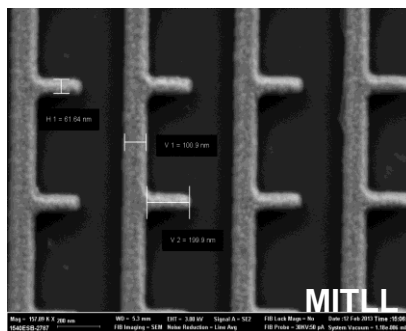
- What are microrectennas and microrectenna arrays?
- **Materials for microrectenna arrays**
- Vertical MIM diode rectifiers
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Materials for microrectenna arrays

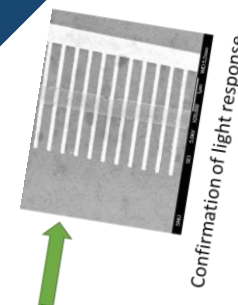
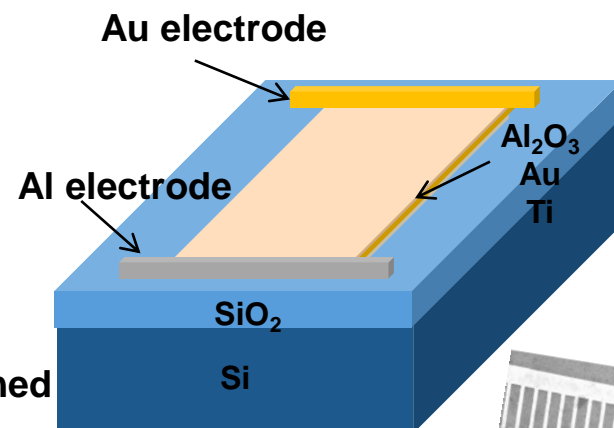
- **Materials systems investigated:**
 - $M/\text{Nb}_2\text{O}_5/\text{NbO}_x/\text{Nb}$, $M = \text{Ag}/\text{Ti}$, Au/Ti , Pt/Ti , others
 - $M/\text{Al}_2\text{O}_3$ (ALD)/ Al , $M = \text{Al}$, Au
- **Al or Nb ground planes**
- **Au wire antennas underneath Al electrode**
 - Small cluster of nanorectennas
 - Antennas run between electrodes in top plane, vertical MIM diode (same as other cases)
- **CNT-based diodes**



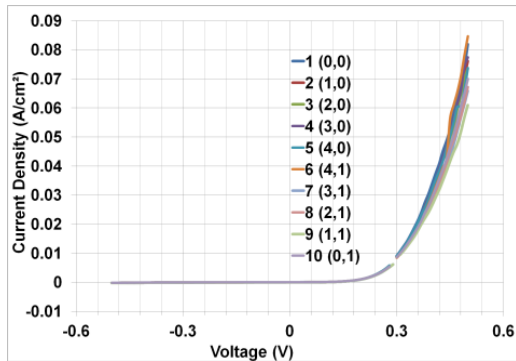
Cross-section of NSRDEC-designed microrectenna array (metal-insulator-metal (MIM) diode)



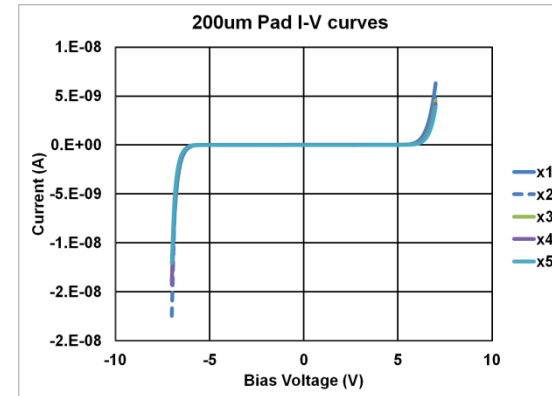
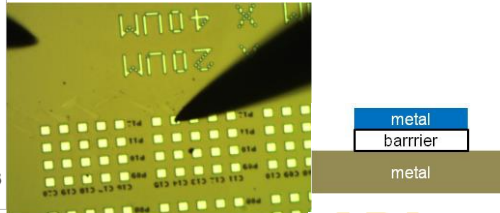
Plan view of NSRDEC-designed microrectenna array (Al stripe-teeth antennas)



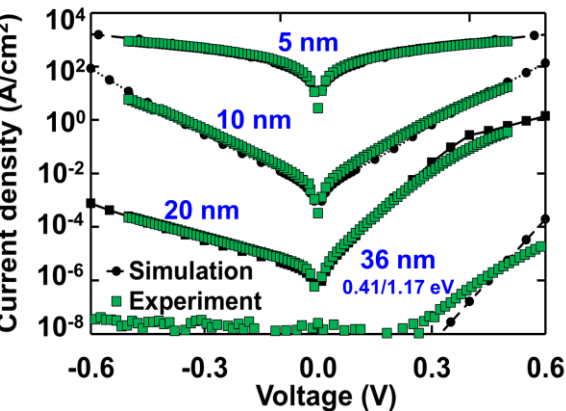
Vertical MIM diode rectifiers (Al- and Nb-based)



Pt/NbO_x/Nb test diodes (ARL) 

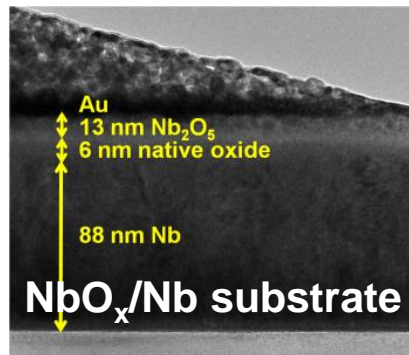


Al-Al₂O₃-Al test diodes



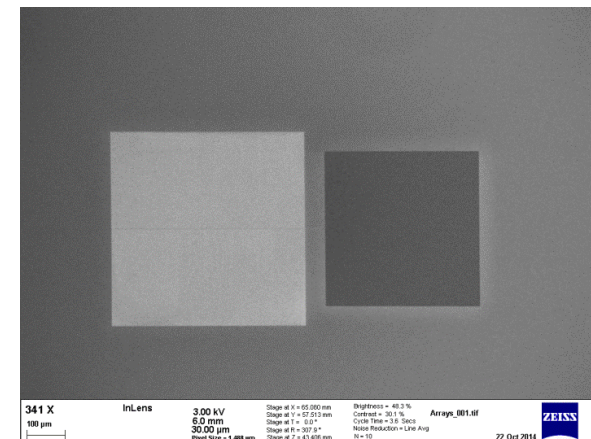
NSRDEC measurement, analysis, modeling

Pt/Nb₂O₅/(NbO_x)Nb test diodes with various barrier (oxide) thicknesses



Derived material parameters for Pt/Nb₂O₅/(NbO_x)Nb diodes:

- $\phi_+/\phi_- = 0.41/0.77$ eV
- $K = 6$
- $m_2 = 0.16 m_0$



Antenna-coupled Al-Al₂O₃-Al array



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(Micro) Rectenna Arrays for Infrared Power Conversion



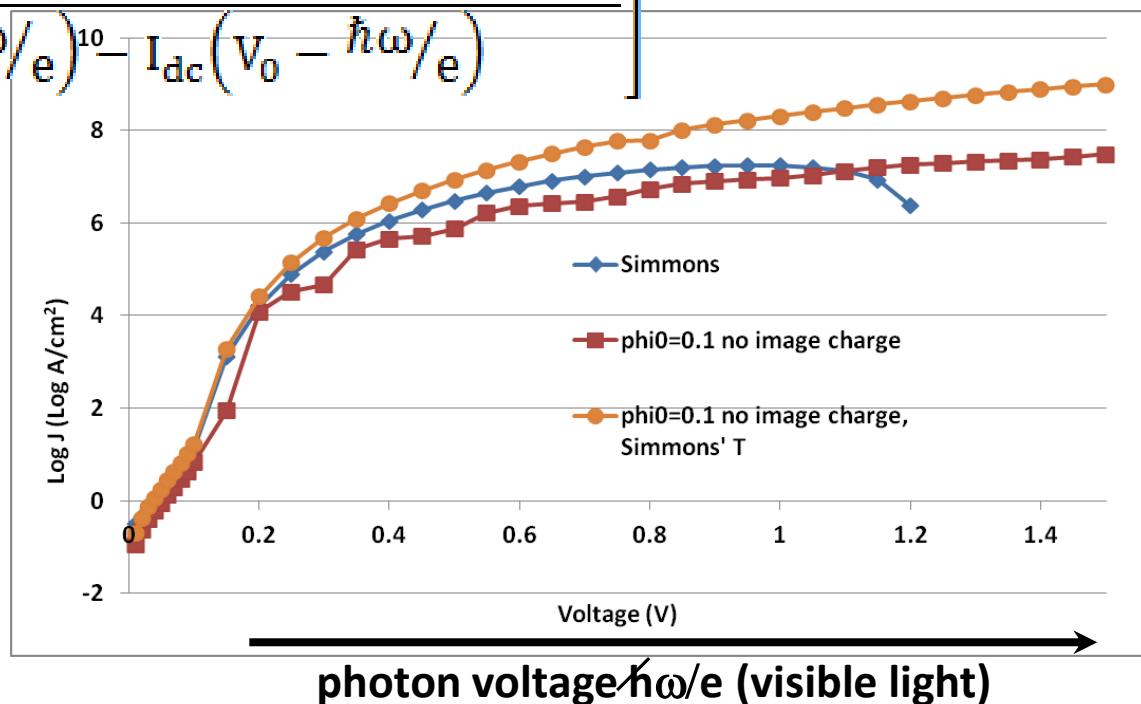
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Need accurate knowledge of MIM diode's I-V curve to predict R_Q

Vertical MIM diode rectifiers

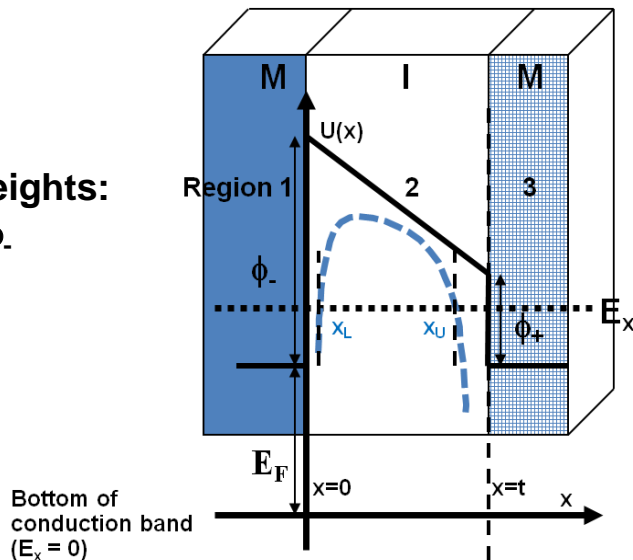
$$R_Q = \frac{e}{\hbar\omega} \left[\frac{I_{dc}(V_0 + \hbar\omega/e) - 2I_{dc}(V_0) + I_{dc}(V_0 - \hbar\omega/e)}{I_{dc}(V_0 + \hbar\omega/e)^{10} - I_{dc}(V_0 - \hbar\omega/e)} \right]$$

Must model I-V curve to predict rectification responsivity (A/W), especially at high voltages for R_Q !

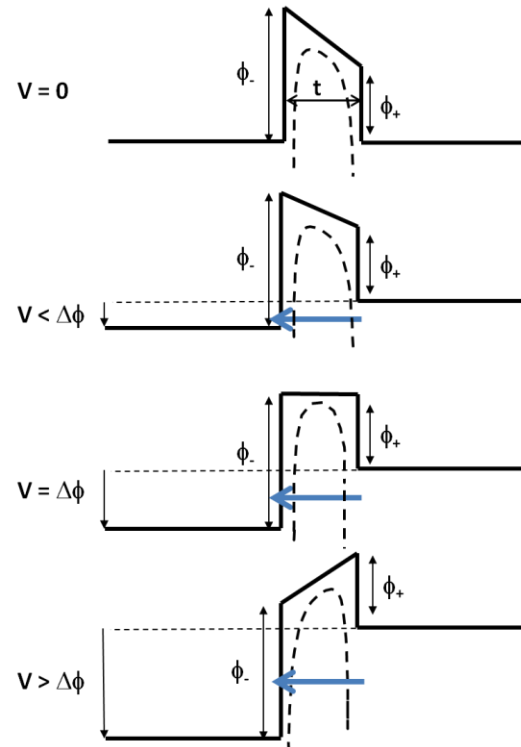
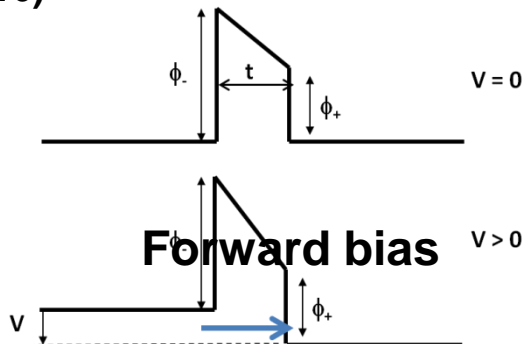


Barrier heights:

$$\phi_+, \phi_-$$



Osgood, Giardini, *et. al.*, JVSTA 34, 0151514 (2016)

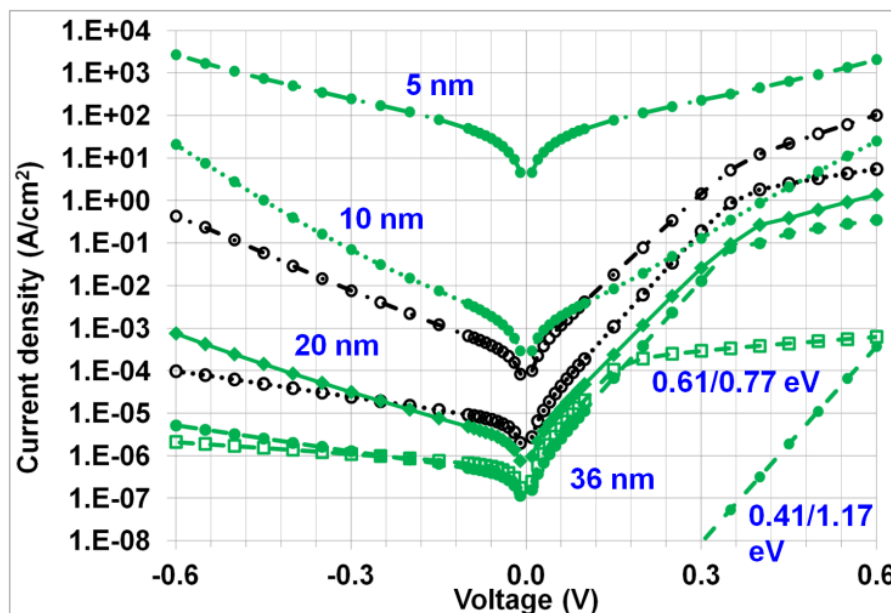
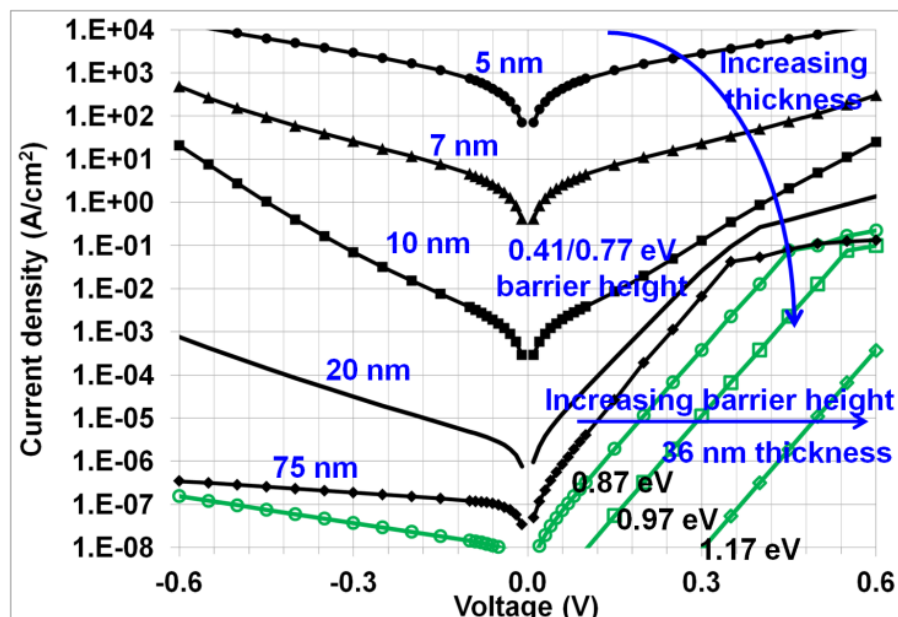


Reverse bias

New physics in model

- Exact solution to trapezoidal potential barrier: no WKB approximation
- Principle of “equal action” to solve image force problem
- Effective mass not equal to electron rest mass
- Note convention: larger barrier on left

Trends with thickness and effective mass



Conduction and rectification in NbO_x - and NiO -based metal-insulator-metal diodes

Barrier heights in format: ϕ_+/ ϕ_-

Richard M. Osgood III,^{a)} Stephen Giardini, and Joel Carlson
US Army Natick Soldier Research Development and Engineering Center (NSRDEC), 15 General Greene Ave.,
Natick, Massachusetts 01760

Prakash Periasamy,^{b)} Harvey Guthrey, and Ryan O'Hayre
Department of Metallurgical and Materials Engineering, Colorado School of Mines, Golden, Colorado 80401

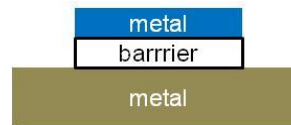
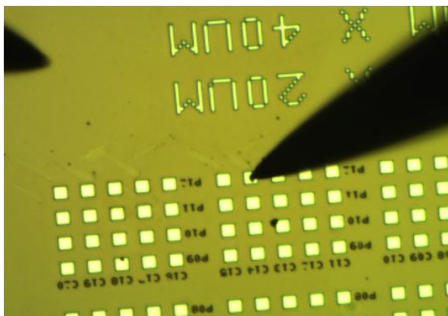
Matthew Chin, Barbara Nichols, and Madan Dubey
RF and Electronics Division, US Army Research Laboratory, Adelphi, Maryland 20783

Gustavo Fernandes, Jin Ho Kim, and Jimmy Xu
Division of Engineering, Brown University, Box D, Providence, Rhode Island 02912

Philip Parilla, Joseph Berry, and David Ginley
National Renewable Energy Laboratory, Golden, Colorado 80401

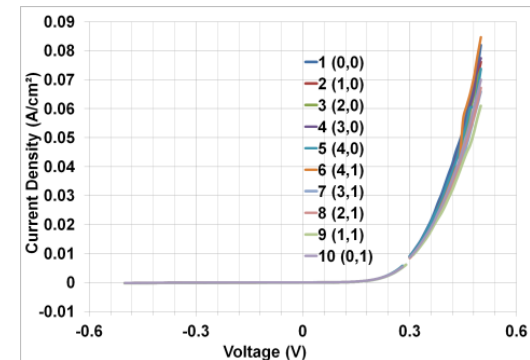
(Received 18 January 2016; accepted 1 August 2016; published 25 August 2016)

Eleven orders of magnitude in current through NbOx – based diodes

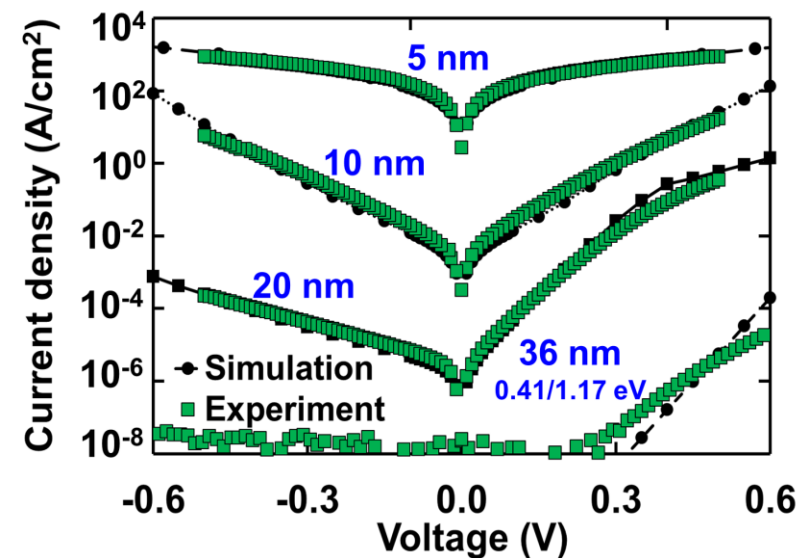


ARL

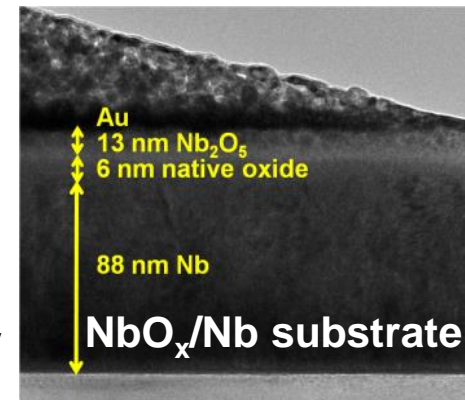
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Barrier heights in format: ϕ_+/ϕ_-



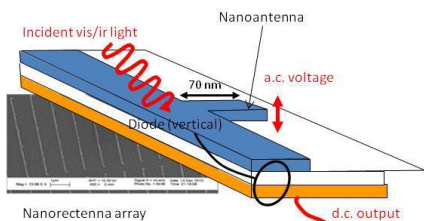
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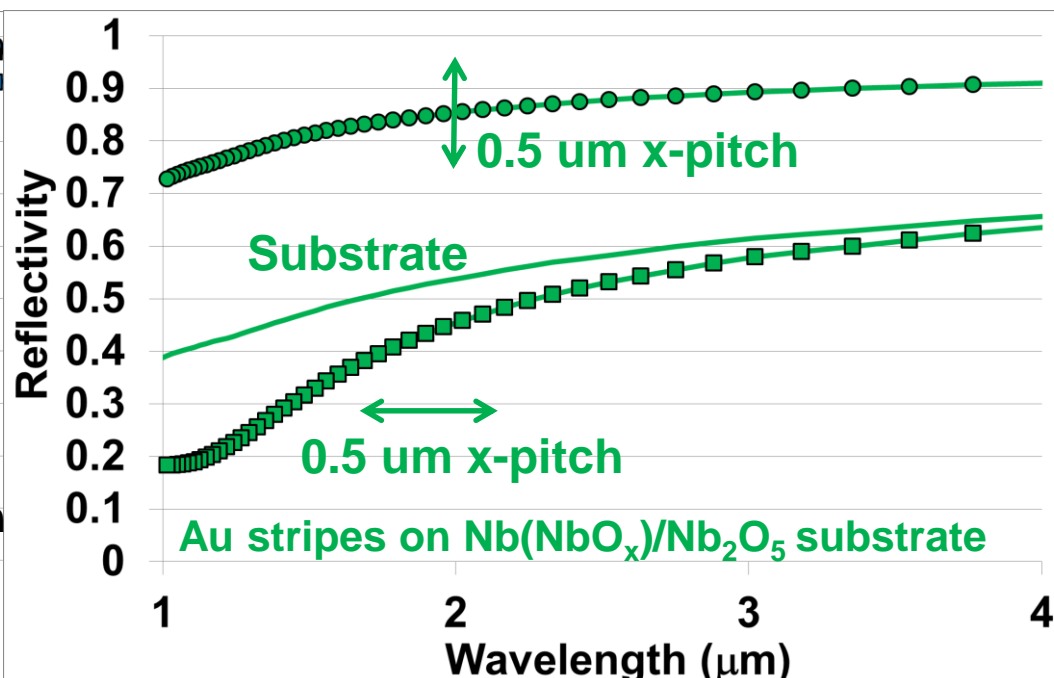
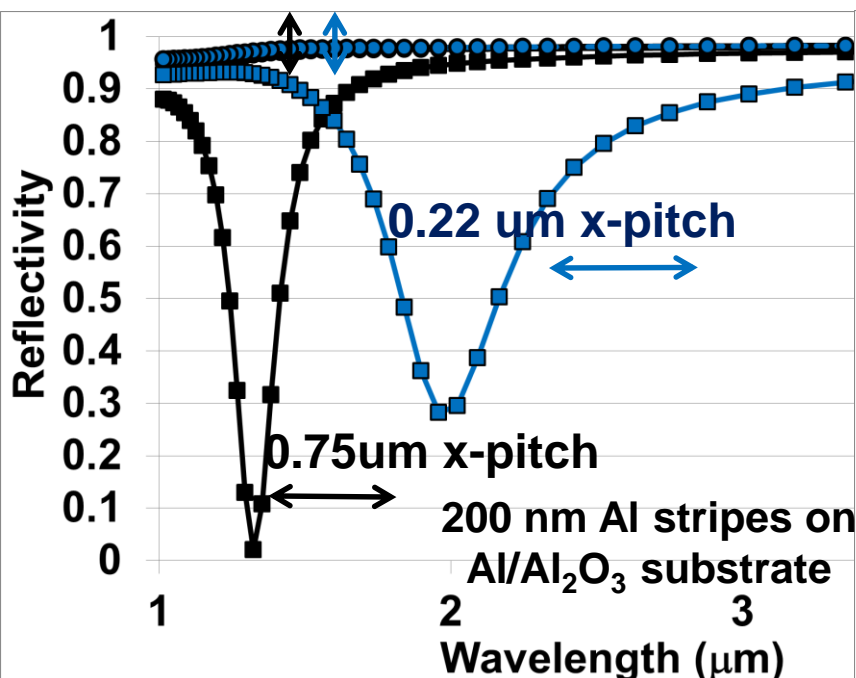
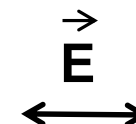
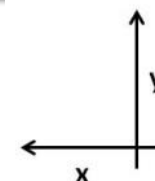
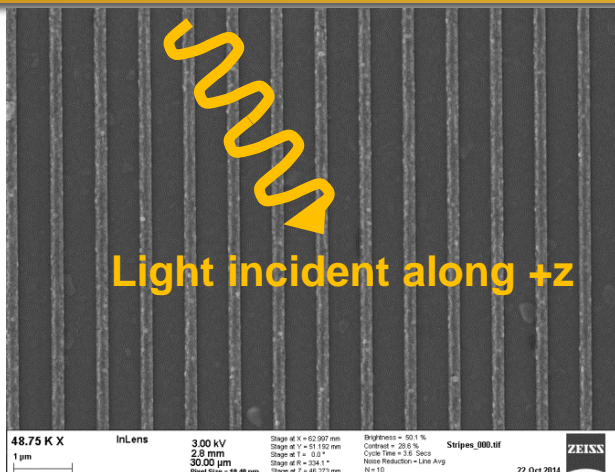
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Stripe arrays exhibit cross-stripe resonances

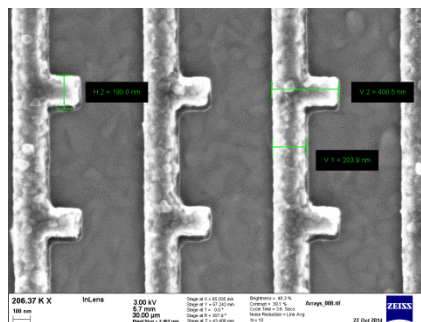
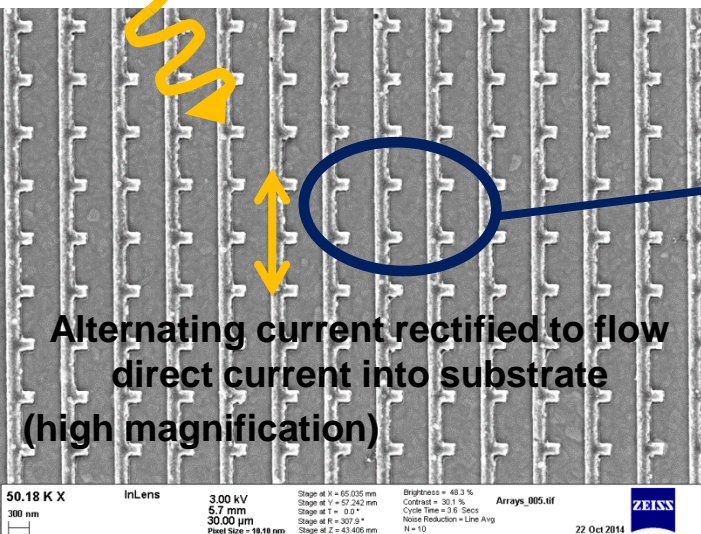


Microrectenna

Top view of stripe array



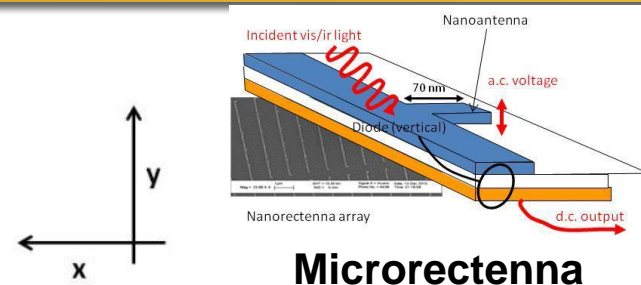
Stripe-teeth resonances (Al-Al₂O₃-Al microrectenna arrays)



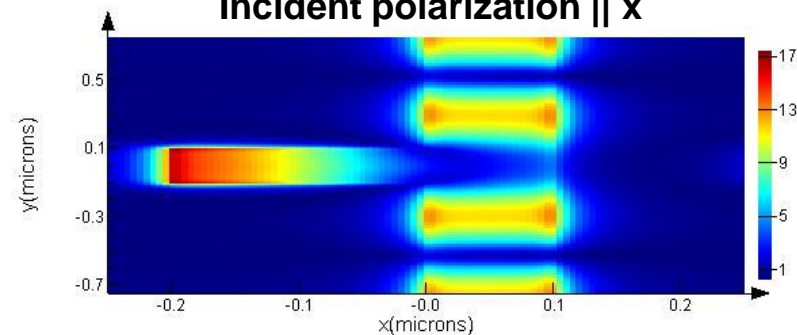
Top view


LINCOLN LABORATORY
 MASSACHUSETTS INSTITUTE OF TECHNOLOGY

US Army NSRDEC design



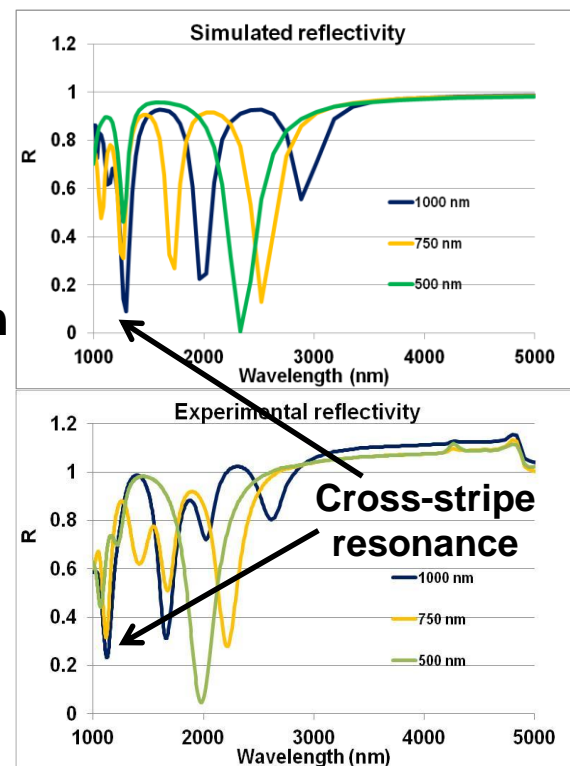
2.25 μm resonance
 Incident polarization $\parallel x$



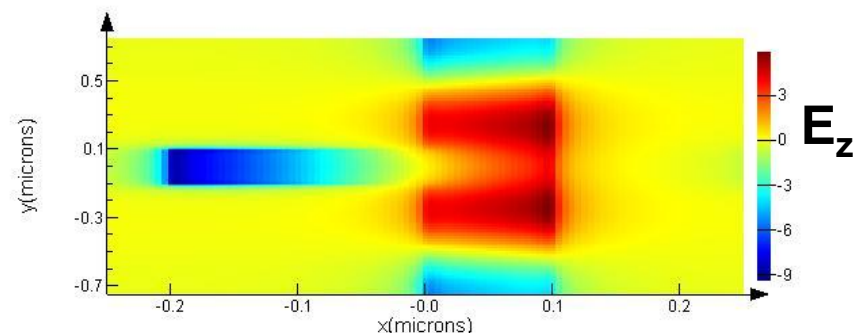
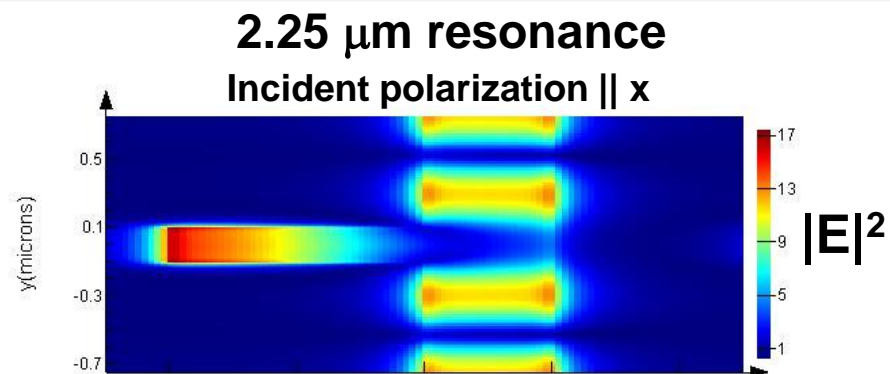
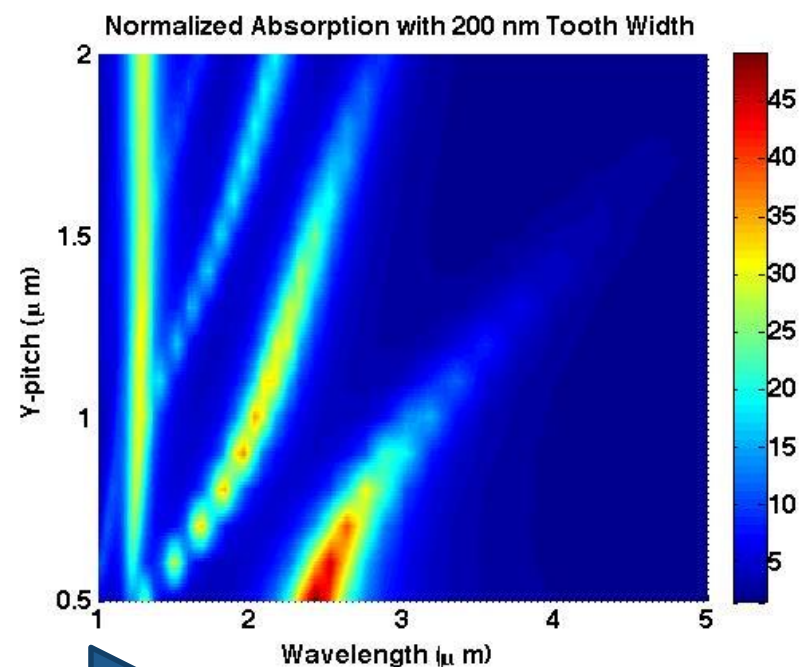
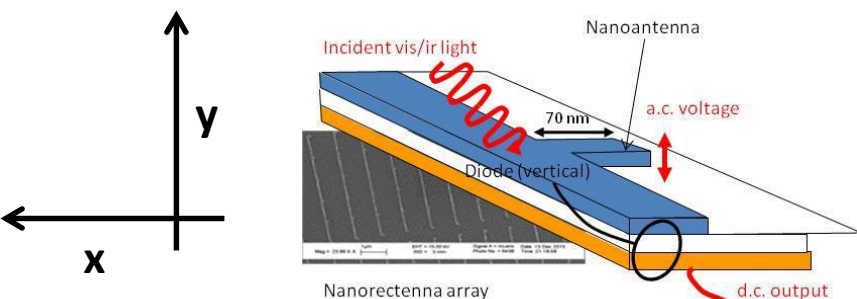
200 nm long Al teeth
 and stripes
 $E \parallel x$



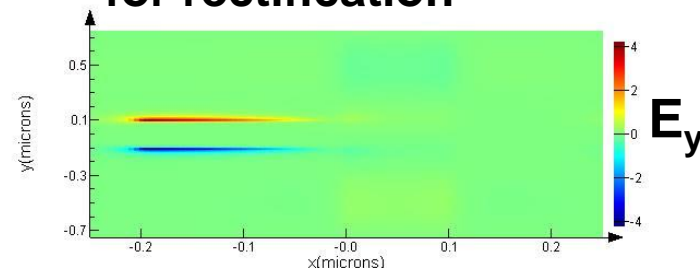
“Teeth” add additional cross-stripe resonances!
 (dependent on teeth separation)



Stripe-teeth resonances (Al-Al₂O₃-Al microrectenna arrays)

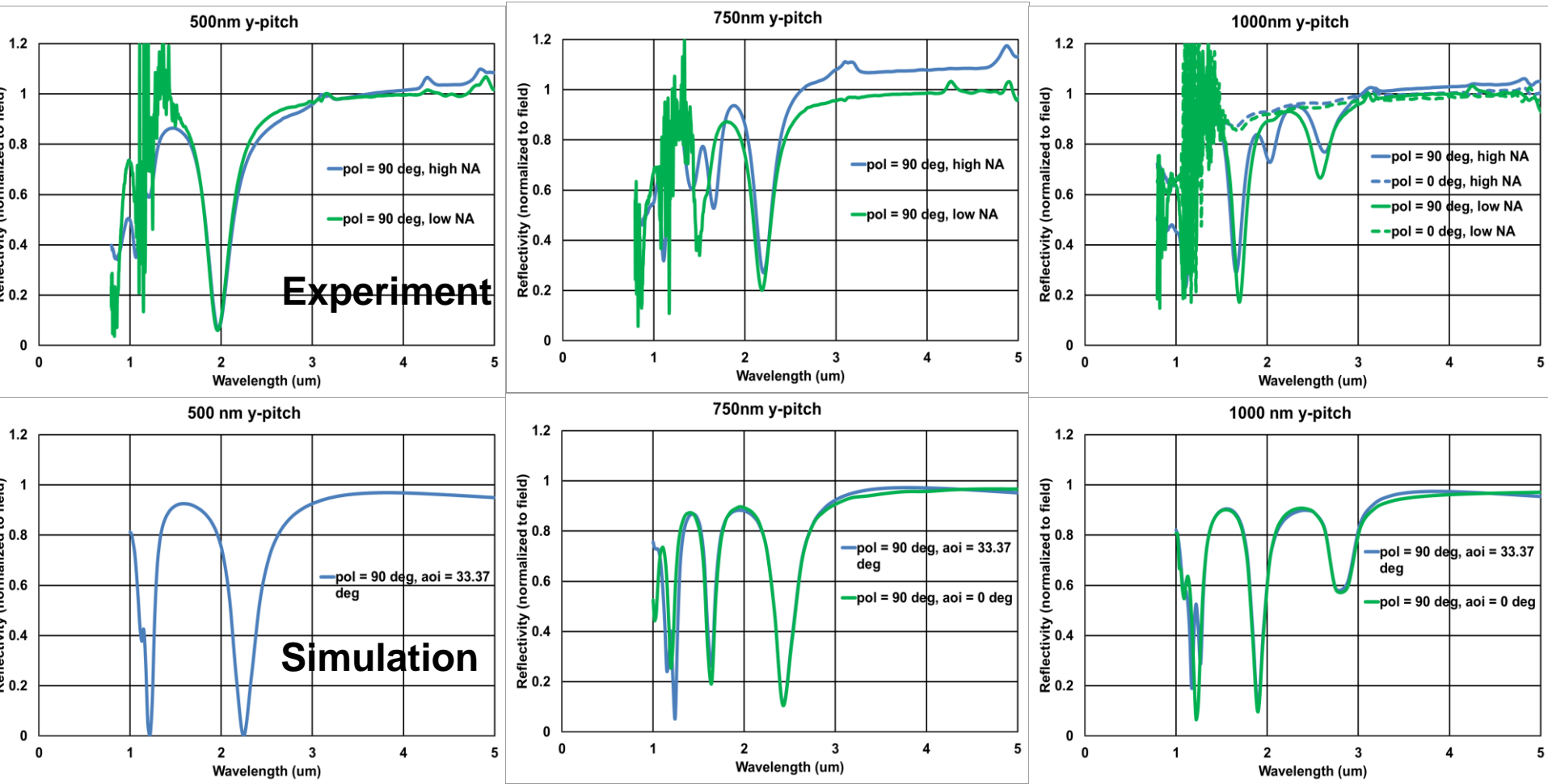


Large asymmetry in E_z needed
for rectification



Has very asymmetric E_z , but need stripes to extract current at resonance

Stripe-teeth resonances (Al-Al₂O₃-Al microrectenna arrays)



- **Good (not perfect) agreement between FTIR-measured spectra and simulated reflectivity. Insensitive to angle-of-incidence (to > 33°).**



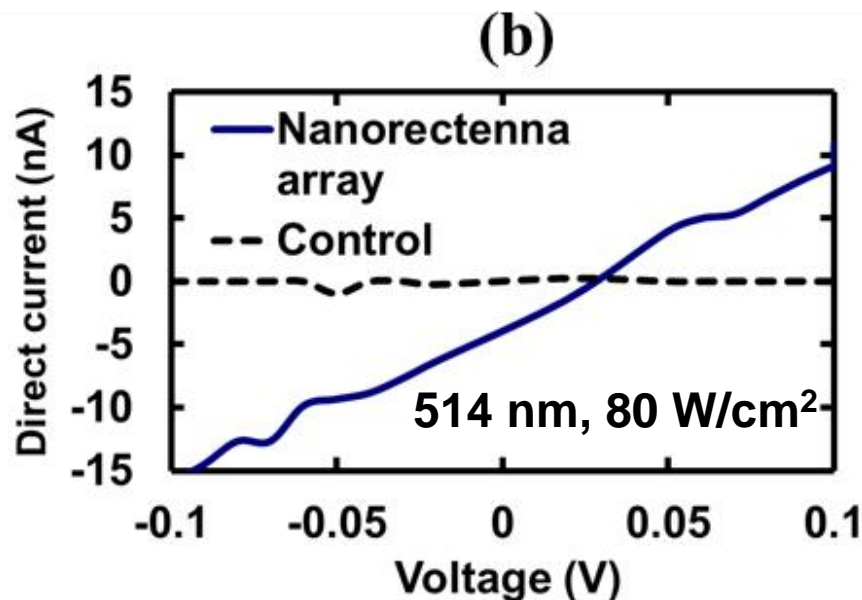
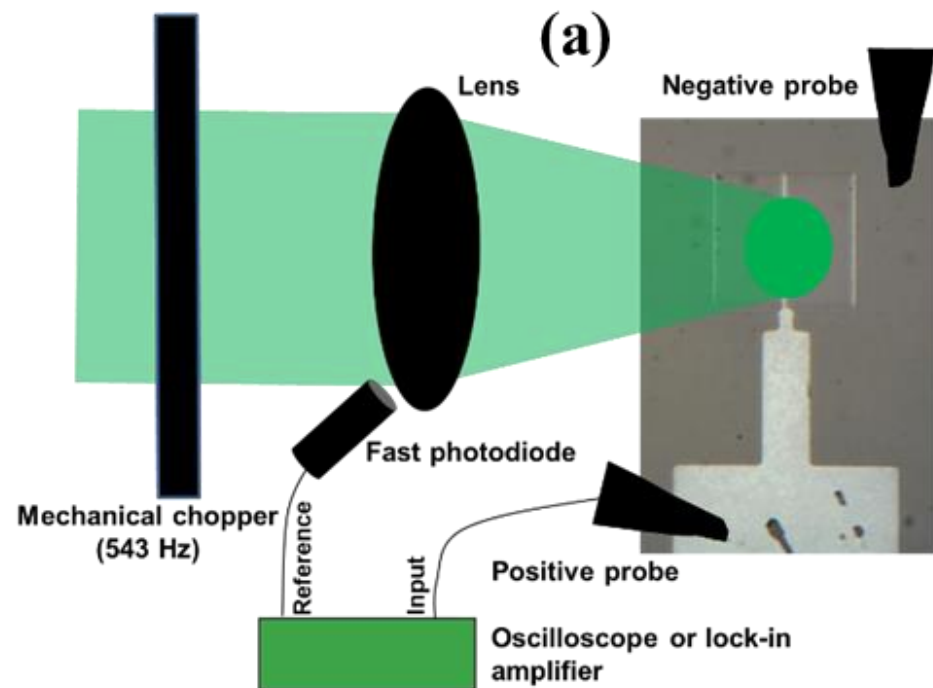
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Analysis of horizontal stripe-teeth arrays



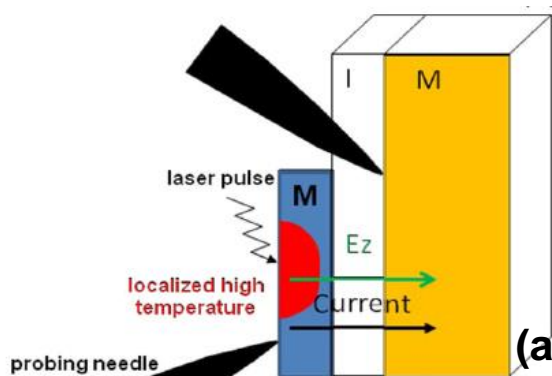
- **Designed for maximum asymmetry/non-linearity consistent with stripes to extract current**
- **Al-Al₂O₃-Al arrays have excellent quality and controlled resonances**
 - **Make broadband with chirped arrays**
 - **With “Au wire” responds to cw visible lasers**
- **Au/Ti-Nb₂O₅-NbO_x-Nb has a lossier ground plane (Nb) and, while an excellent electronic-quality oxide, antenna resonances much broader and weaker**
 - **However there is an interesting response to cw lasers with small dimensions (“nanorectenna array”)**

Nanorectenna array output power from cw laser illumination!



- 5 nA at zero volts - much higher than predicted from rectification responsivity (0.45 A/W maximum)!

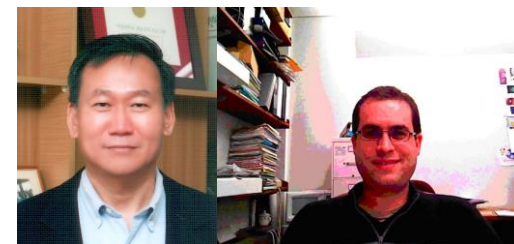
NSRDEC
measurement,
analysis, modeling



Photothermoelectric effect
(antenna heated more than the ground plane)?



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Nanowire-based nanorectenna clusters

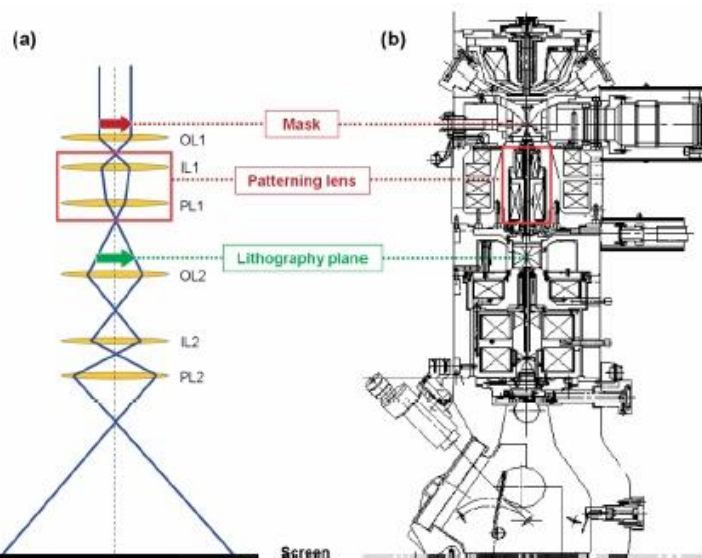
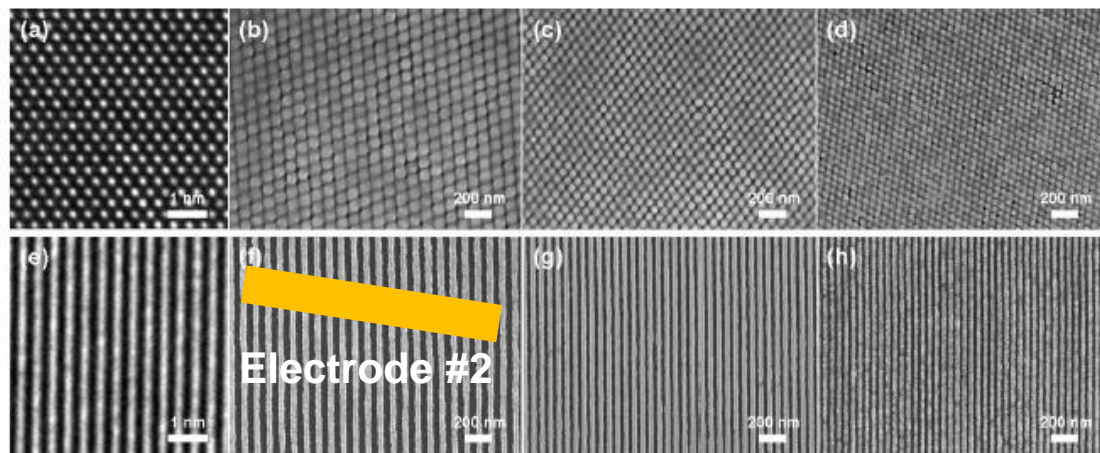


Figure 1. Schematic ray diagram and cross-sectional view of the present lithography system. a) Ray diagram of the basic lens system of image formation, which is composed of two different sets of OL, IL, and PL. The first set magnifies the sample image to the lithography plane with a magnification ranging from 50 to 300 times, while the second set further magnifies this image to the viewing screen. b) The specially designed hardware which was developed based on the modification of a 200 kV TEM equipped with a field emission gun (JEM-2010F, JEOL Ltd.).

- Inverted Au/ Al_2O_3 (ALD)/Al stack
- Au wire antennas underneath Al electrode
- Regular, high-resolution arrays of lines and dots
- Unique nanopatterning approach

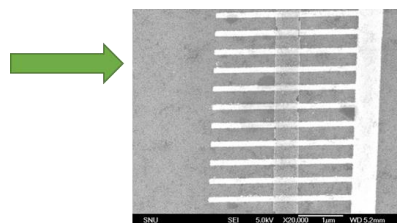
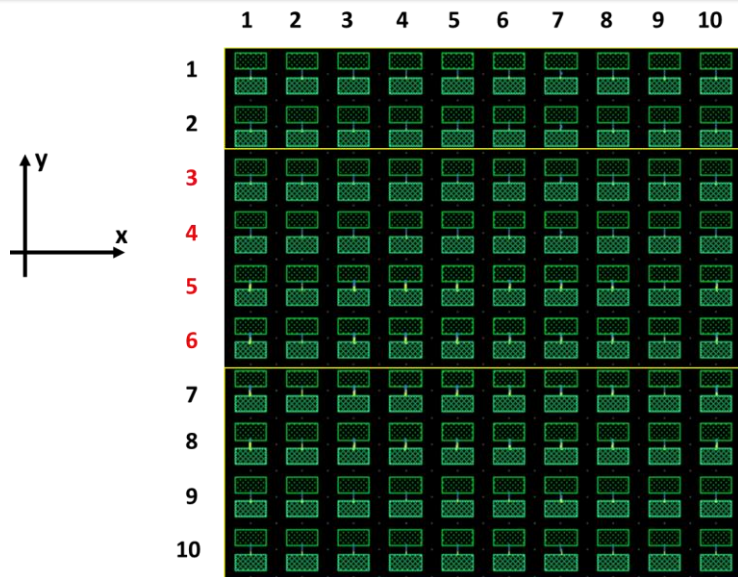


Electrode #2

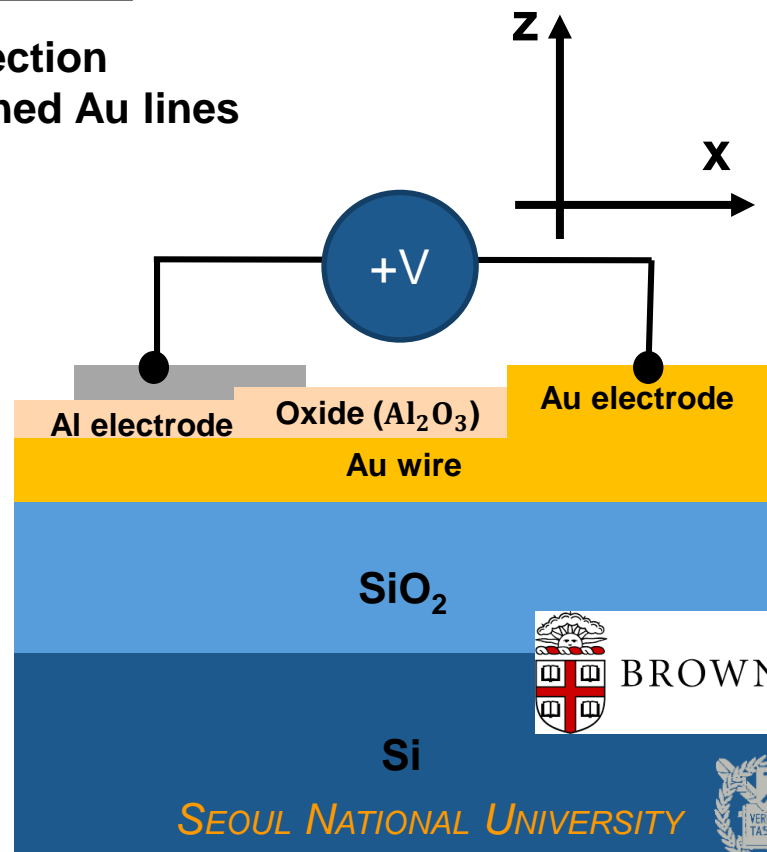
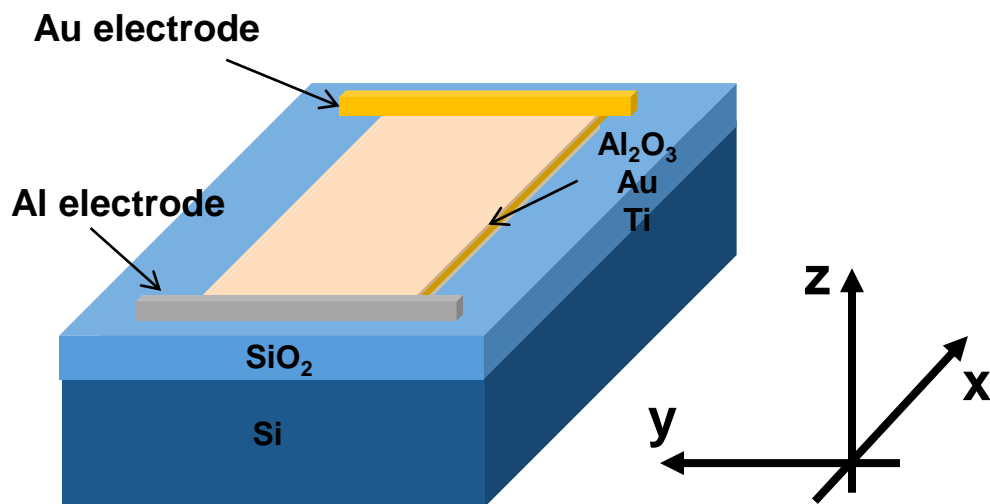
Electrode #1

Vertical diode, horizontal antennas

Nanowire-based nanorectenna clusters



Projection
nanopatterned Au lines

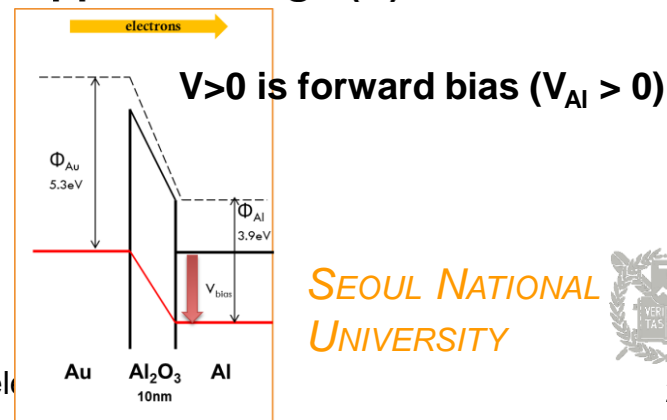
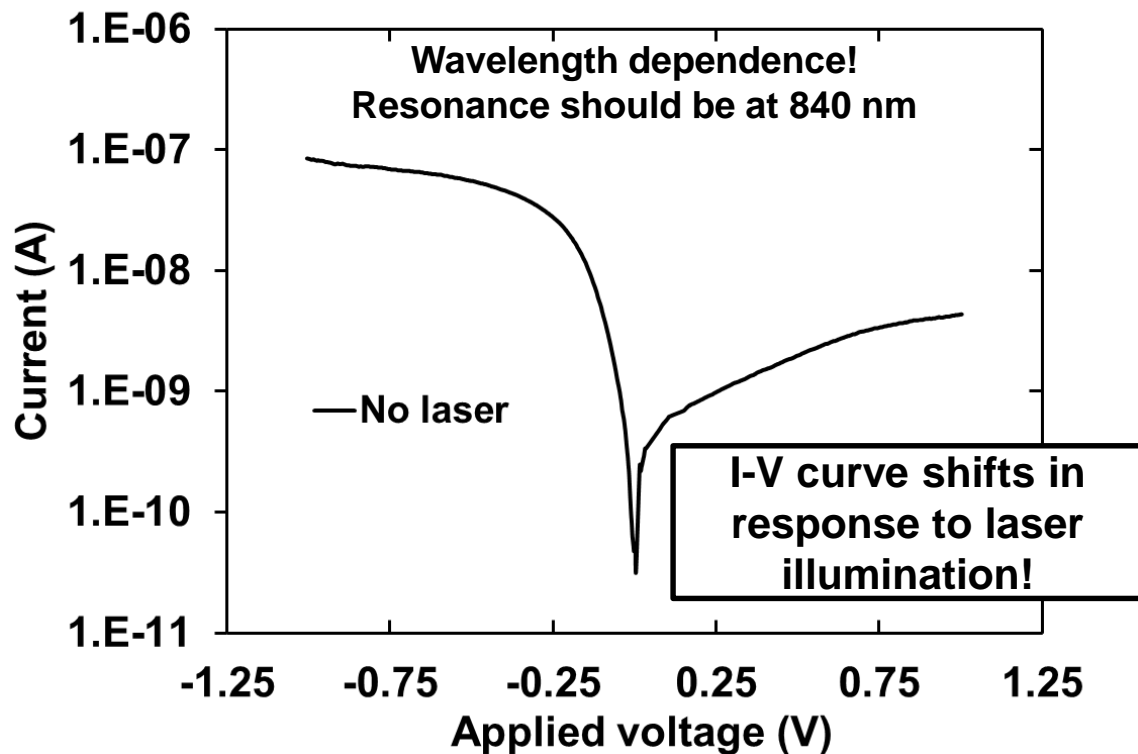
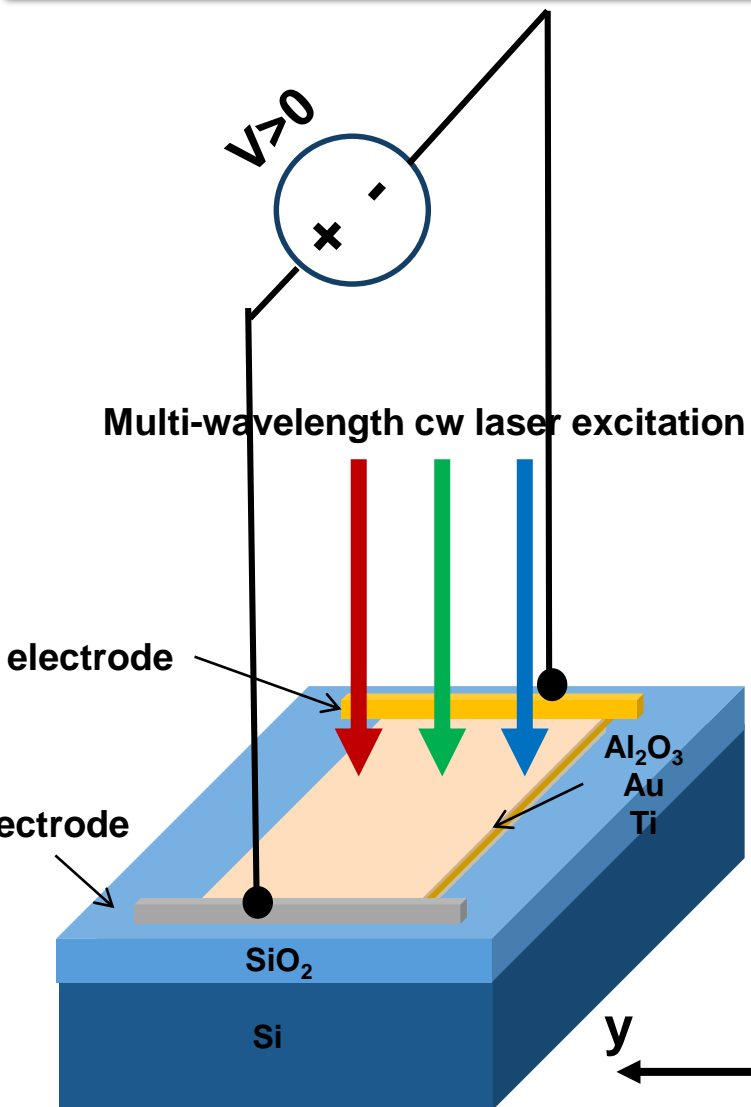


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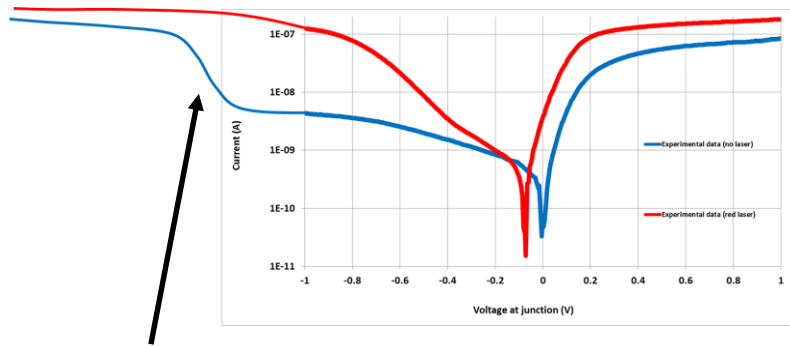


Nanowire-based nanorectenna clusters



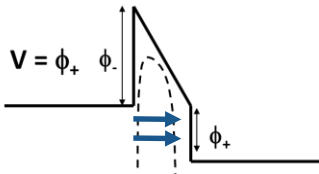
Modeling Al-Al₂O₃-Au nanorectennas to explain data

Hypothesis I: steps in I-V curve are due to oscillations in transmission function through barrier layer in MIM diode, which are due to interferences in the transmission through the trapezoidal (image-modified) potential

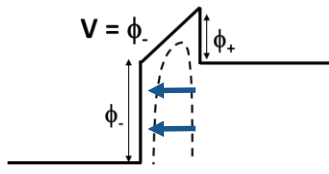


Hypothesized “step” in I-V curve

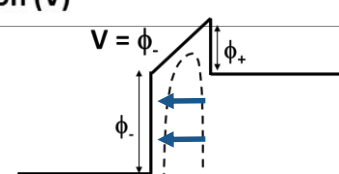
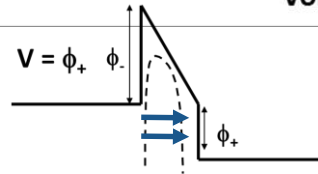
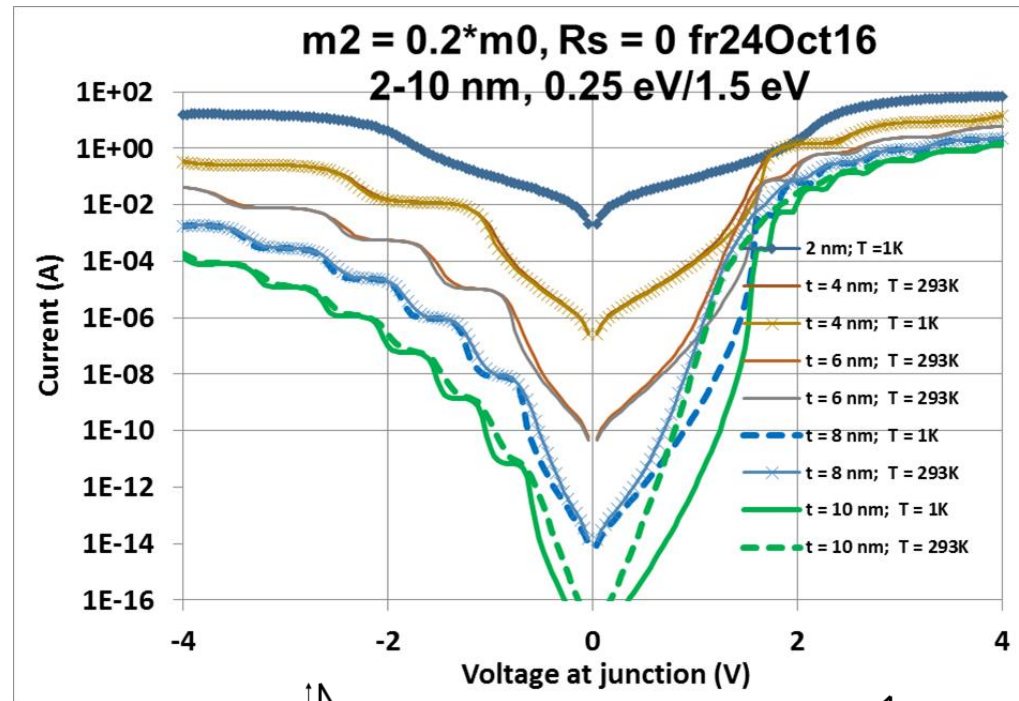
Forward bias



Reverse bias



A few states below the Fermi level have tunneling transmission resonances across barrier into empty states (producing steps in the I-V curve at low temperatures), but V must be at least $> \phi_+$ (for forward bias) and at least $> \phi_-$ (for reverse bias)

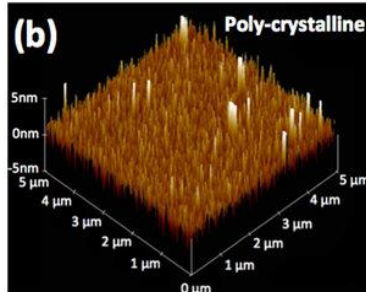
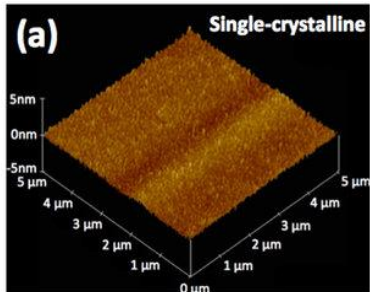
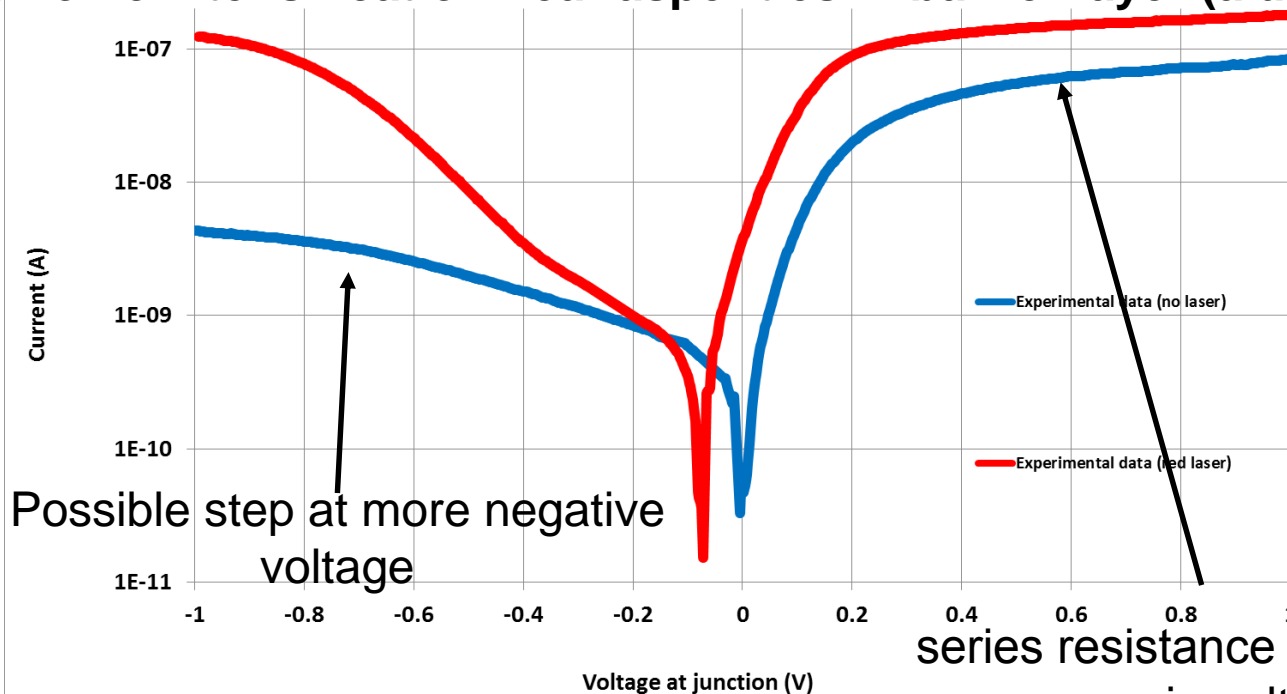


2-10 nm thick barrier layer, $K = 6$, Temp = 293 K or 1 K

Note: $V > 0$ is *reverse bias*

Modeling Al-Al₂O₃-Au nanorectennas to explain data

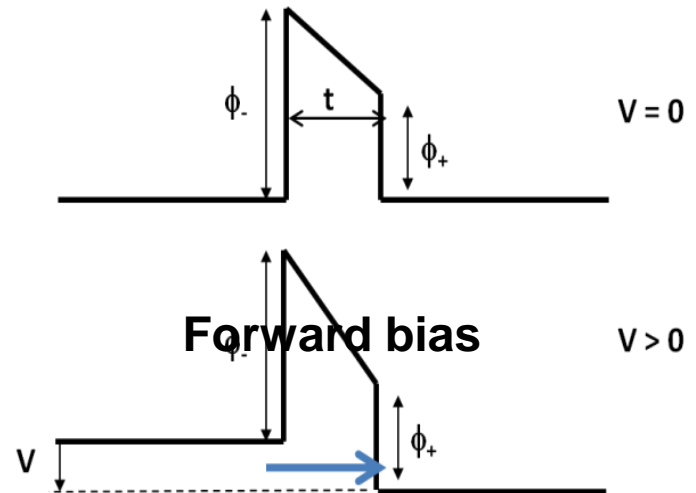
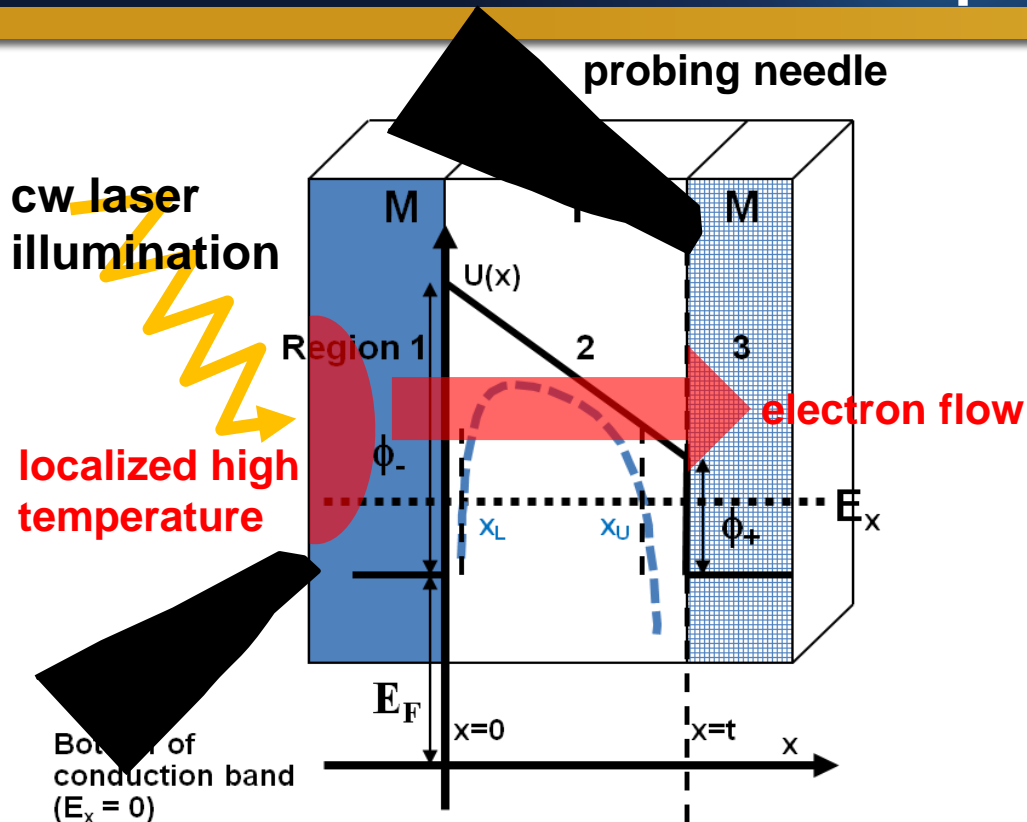
Hypothesis II: Shift in J-V curve due to laser illumination may be due to field and plasmonic intensification near asperities in barrier layer (aluminum oxide)



Other possibilities for large response to cw visible laser: rectification, charging

Note: $V > 0$ is *reverse bias*; opposite from previous notation.

MIM diode model improved to include temperature gradients

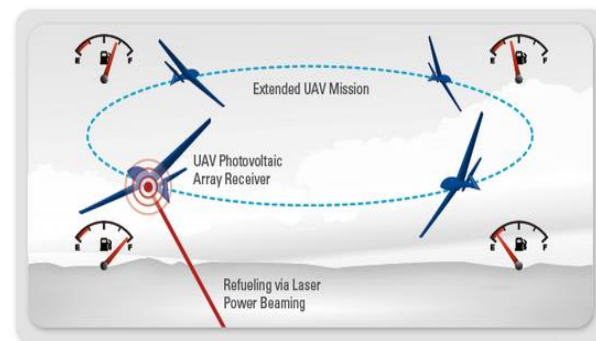
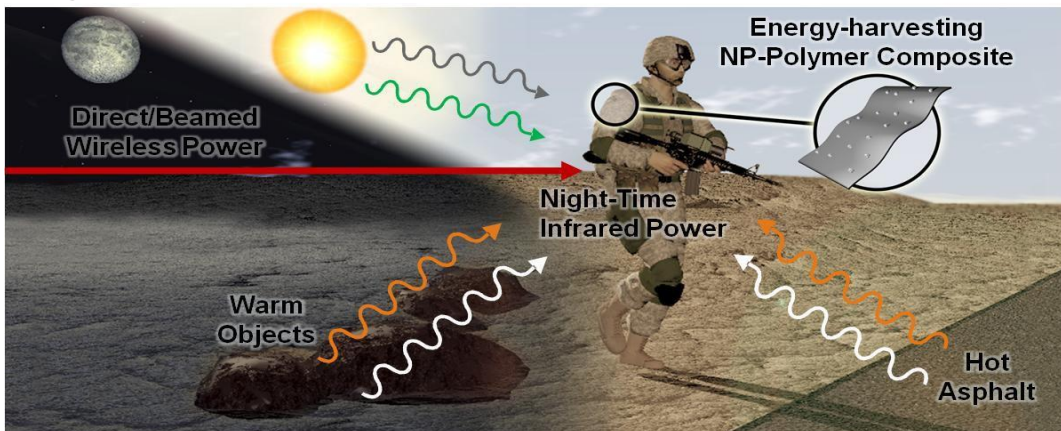


New temperature gradient in NSRDEC MIM diode model; regions 1 and 3 are at different temperatures. Barrier heights: ϕ_- and ϕ_+ , where $\phi_- > \phi_+$.

- **Nonlinear rectifying metadevices create new opportunities (quantum and nonlinear plasmonics)**
- **Nb- and Al-based stripe-teeth metamaterial arrays designed and analyzed**
 - Both have cross-stripe resonances
 - Au/NbOx/Nb: broad, weak resonances
 - Al/Al₂O₃/Al: well-controlled absorption spectrum
 - Standing wave resonances dependent on y-pitch
 - Angle of incidence has little effect to at least 33 deg.
 - J-V curves for Ag(Ti)/NbOx/Nb show $\phi/\phi_+ = 0.41/0.77$ eV
 - J-V curves for Al/Al₂O₃/Au show ϕ/ϕ_+ reduced
 - Curves shift with focused laser – due to field enhancement from AlOx roughness, photoemission/charging, and heating effects
 - “Steps” in I-V?
 - Rectification responsivity predicts shift due to laser illumination?
- **Large direct current at $V = 0$ from Ag(Ti)/NbOx/Nb and Al/Al₂O₃/Au microrectenna arrays much larger than predicted by classical and quantum rectification formulas**
 - Rectification or photothermoelectric effect?
 - Are steps in MIM diode I-V curves possible?

Potential future concepts

- A new early applied program on narrowband infrared rectenna arrays starting in FY17.
- Proof-of-concept experiments (labscale demonstrations) will be carried out for power and data beaming.



Potential application: Wireless power/data transfer/communications (Warfighter/Soldier/Squad and/or UAS sustainment)

Enhanced thin-film photovoltaics

Potential future application:
Solar blankets and/or
military shelters

