



University at Buffalo
The State University of New York

Bow Shock Emission and Near-Surface Nitric Oxide Absorption Measurement Techniques for Gas/Surface Interaction Interrogation

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AFOSR Review Meeting

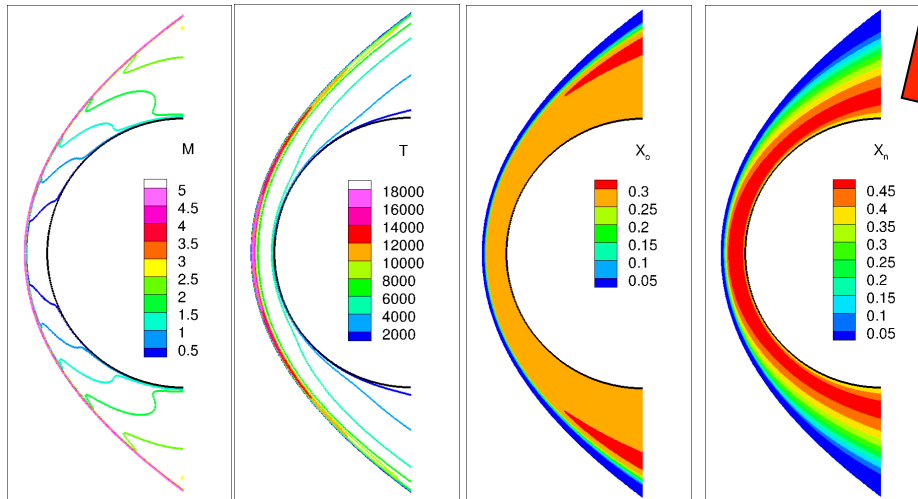
15 July 2013



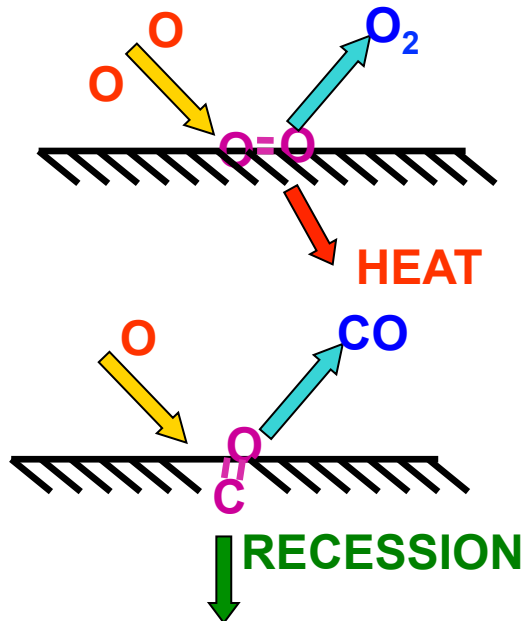
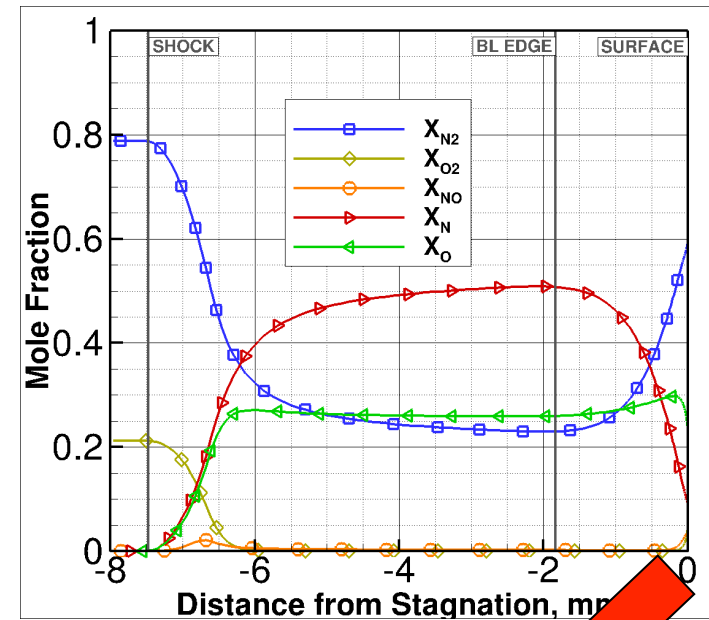
Outline



- Motivation
- CUBRC LENS-XX Facility
- Near-surface Tunable Diode Laser Absorption Spectroscopy (TDLAS)
 - Theory
 - Experimental Setup
 - Line-of-Sight Modeling
 - Results
- Bow shock Emission Spectroscopy
- Conclusions

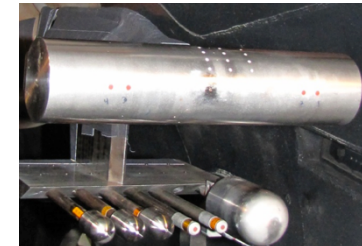
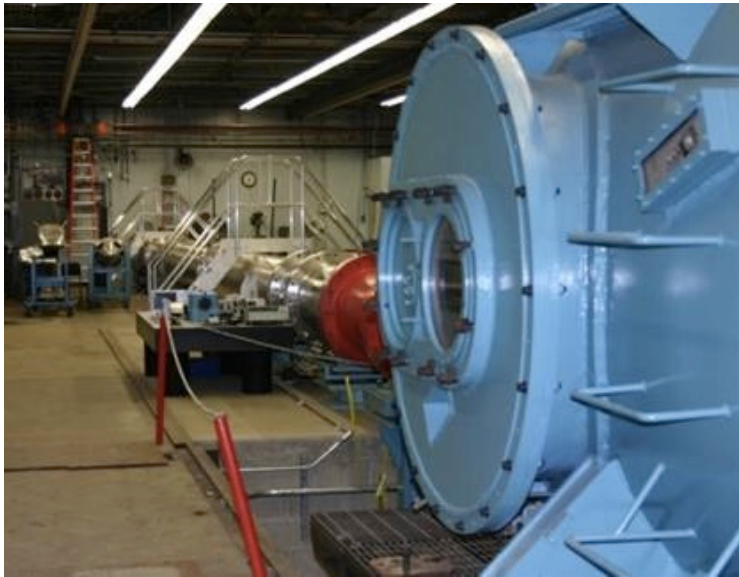


Very hot shock layer temperatures cause the gas to dissociate in a stagnation region.

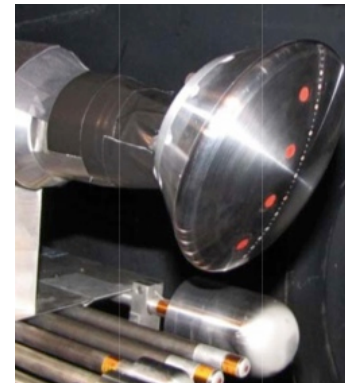


Energetic species existing in the shock layer can reach the surface and react, releasing heat and/or removing TPS.

- In high enthalpy environments, it is very difficult to “measure” catalytic and ablative processes directly.
- Traditionally, must observe the “effect” by measuring the heat flux or post-test recession and inference.



Basic shapes (hemisphere, cylinder)



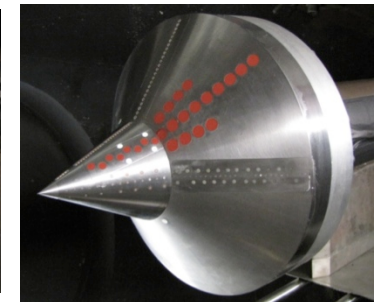
Orion



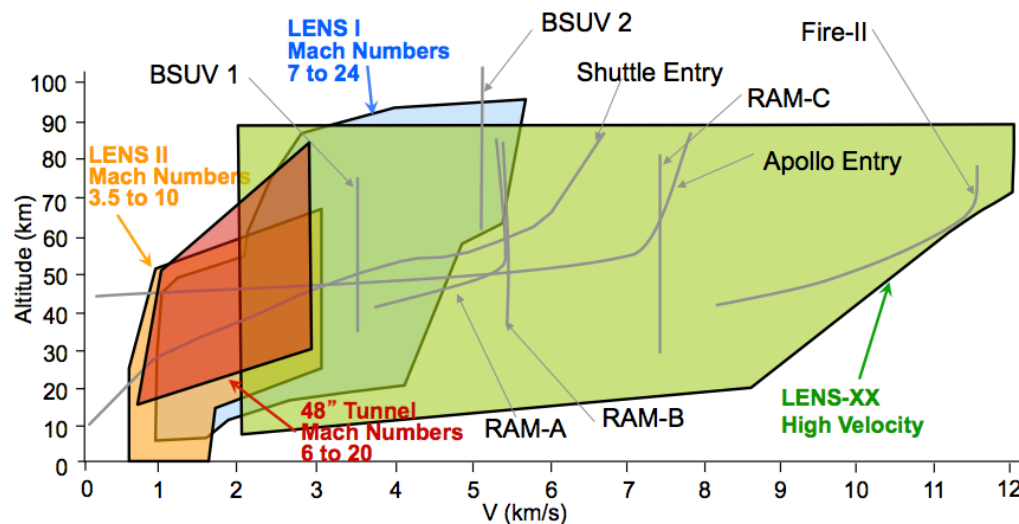
MSL



Hollow Cylinder



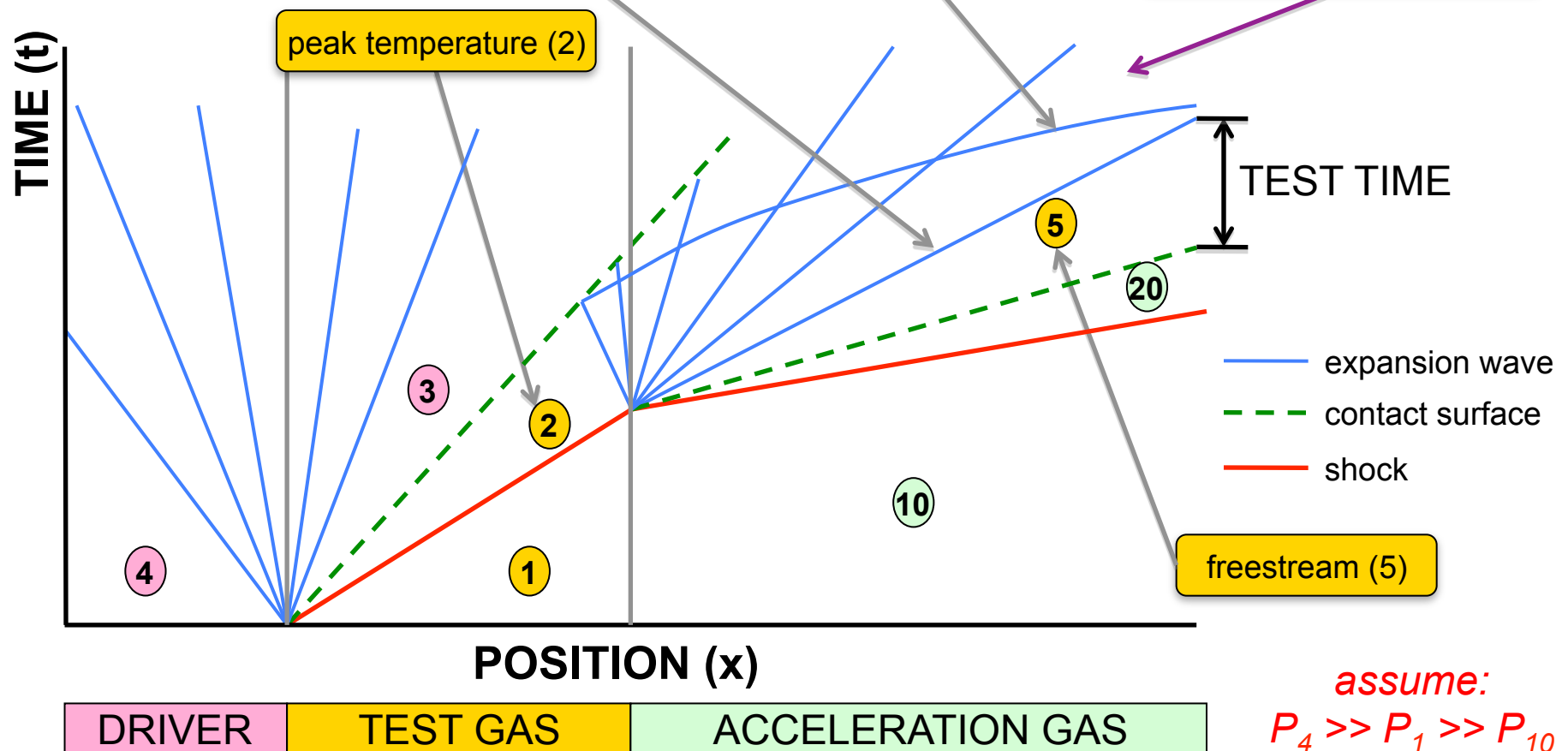
Double Cone



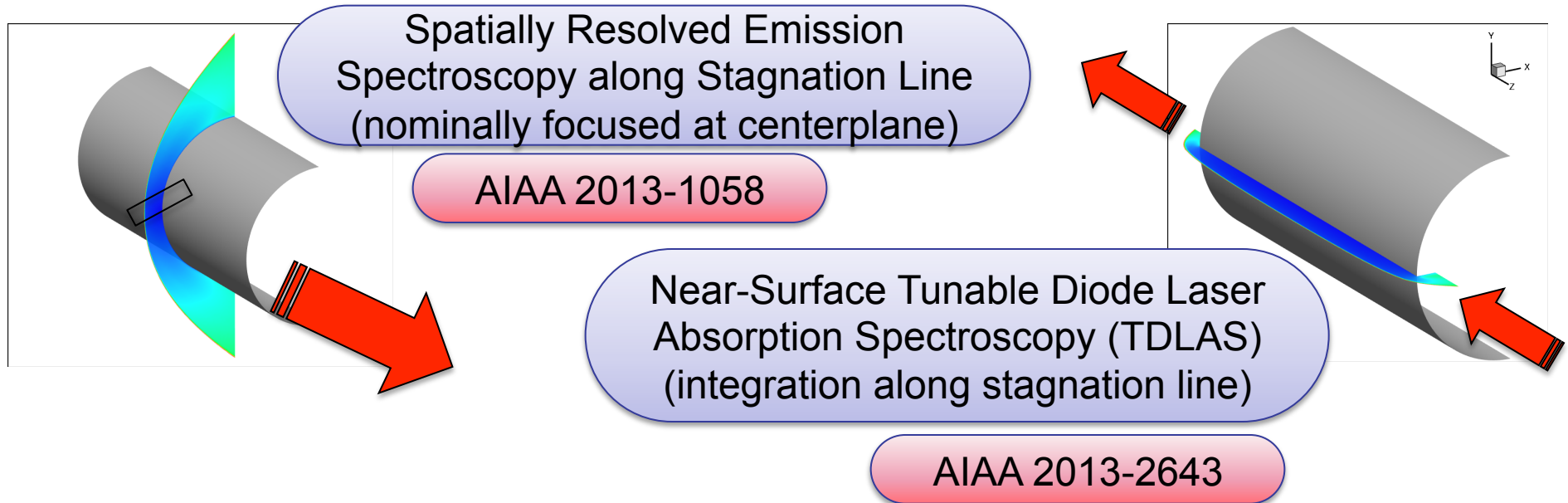
Test Time Limited by Two Factors:

- Head of unsteady expansion (reflected off primary contact)
- Tail of unsteady expansion

unsteady expansion adds kinetic energy directly ($U_5 \gg U_2$)



New Diagnostics for Catalytic and Ablating Flows Developed on a Cylinder Model



- Near-surface TDLAS with 5.44 micron QCL from Alpes Lasers targeting Nitric Oxide (NO) fundamental transition.
- Why study NO formation?
 - We already own a very expensive laser (\$\$\$\$).
 - Well-grounded cold wall (300K) surface temperature.
 - Importance of NO formation on reacting air surface catalysis demonstrated in literature.
 - Lessons learned apply directly to ablating flows later on...



Tunable Diode Laser Absorption Spectroscopy (TDLAS)



Beer-Lambert Law

$$\frac{I}{I_0} = \exp(-k_v L)$$

(monochromatic absorption through a uniform gas)

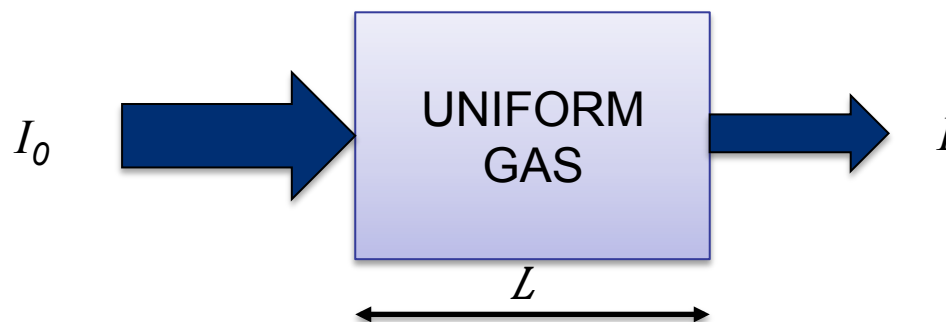
Spectral absorption coefficient

$$k_v = S_i(T) P X_j \phi_v$$

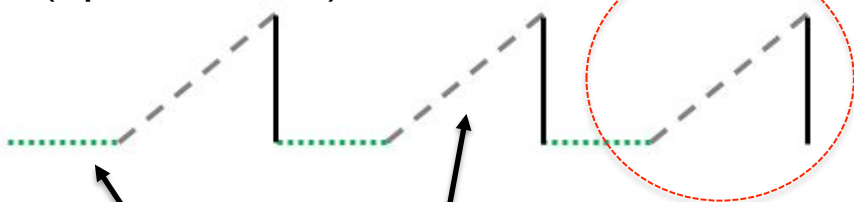
Doppler broadening
(Temperature)

Collisional broadening
(Pressure)

Gaussian + Lorentzian = Voigt convolution



Function Generator
(up to 10 kHz)



Single Data Ramp

Laser below
threshold

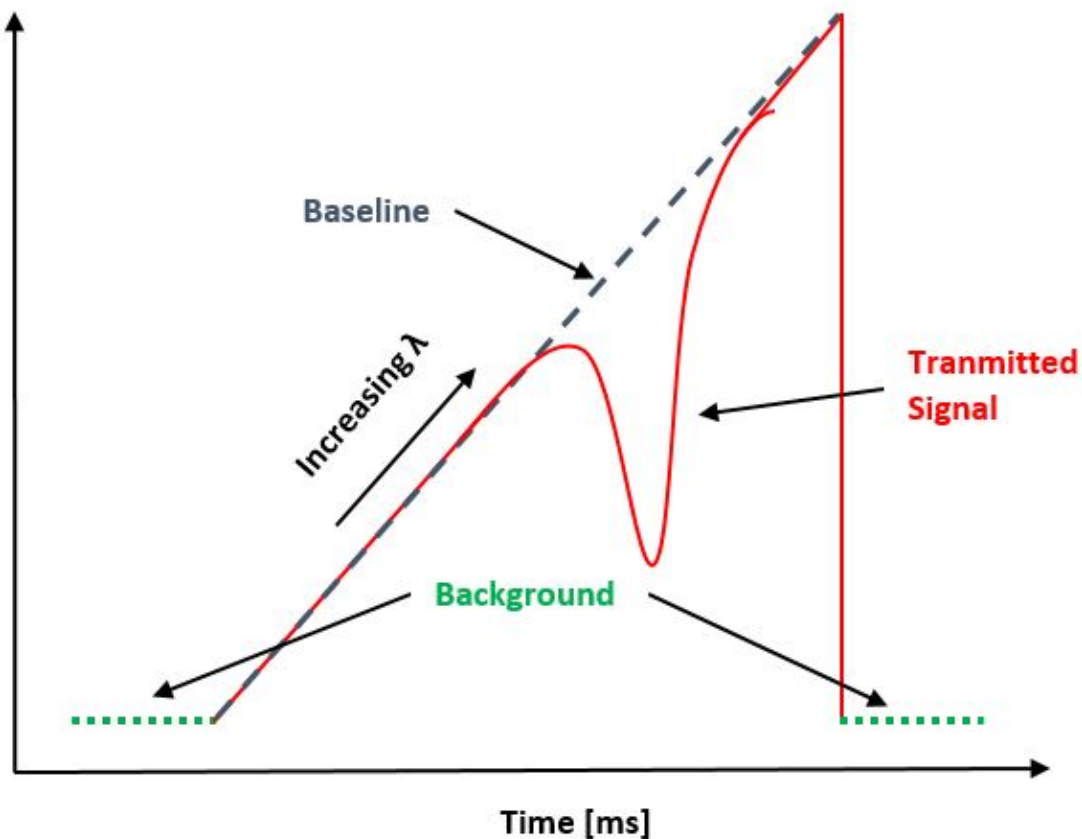
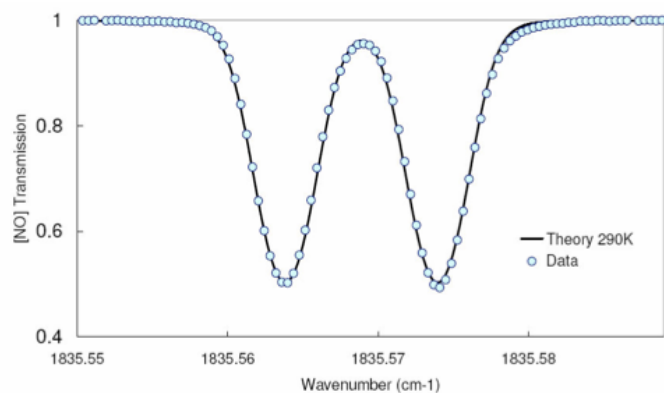


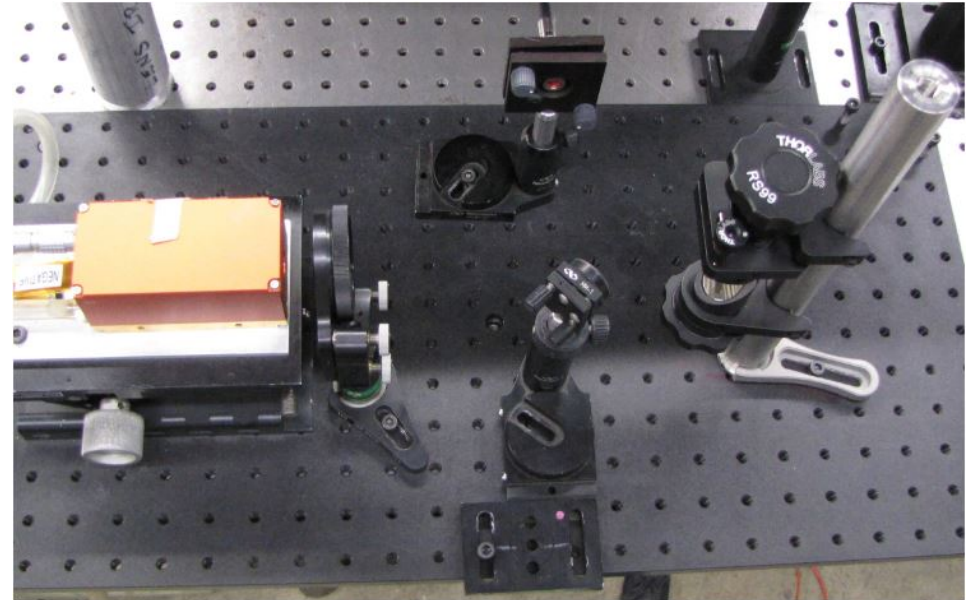
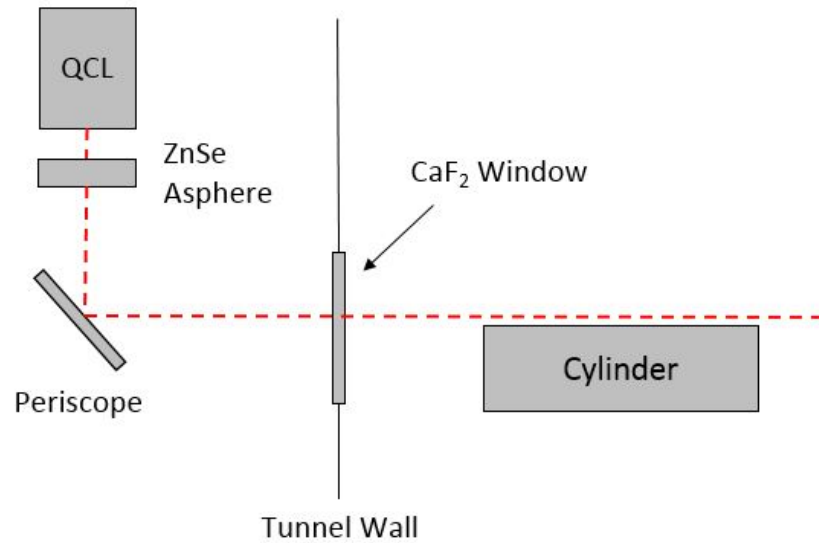
Current



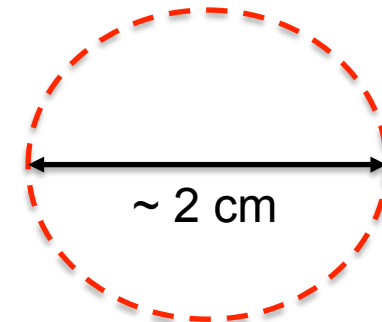
Wavelength

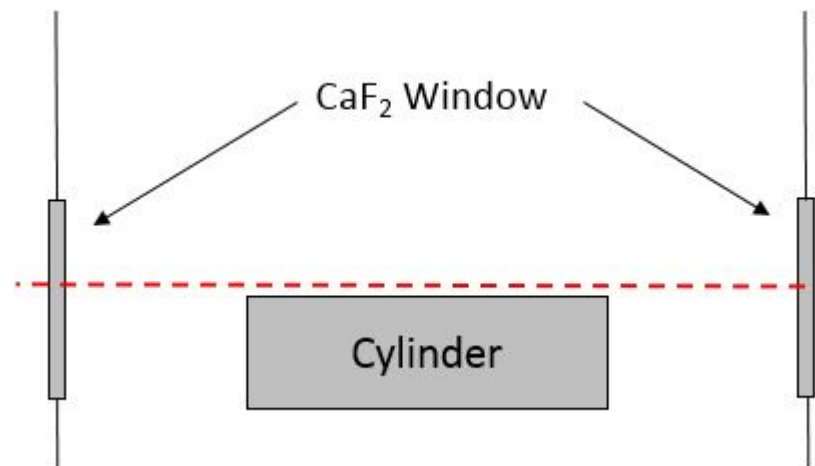
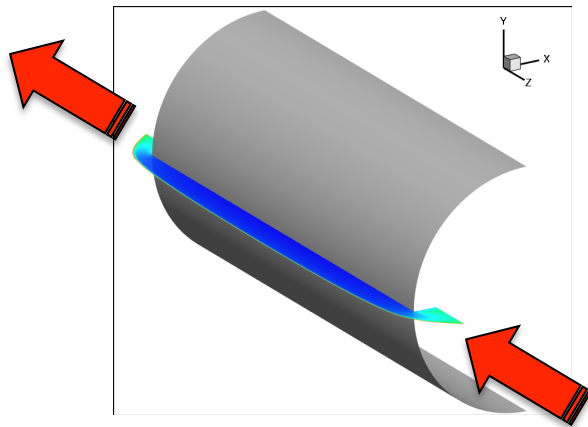
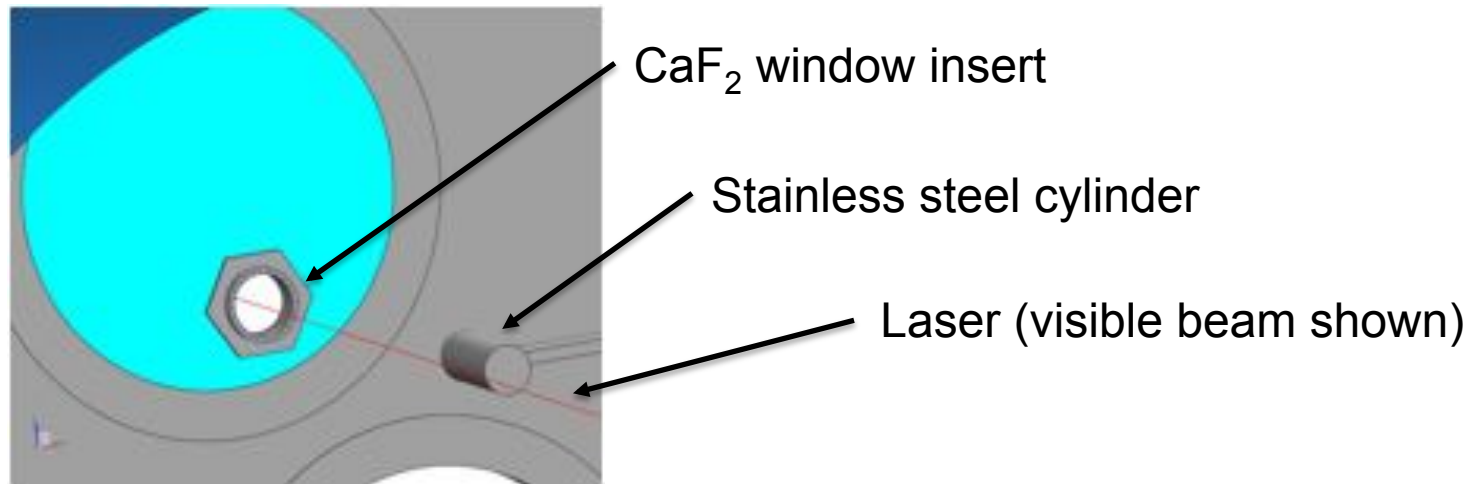
Voltage
[V]





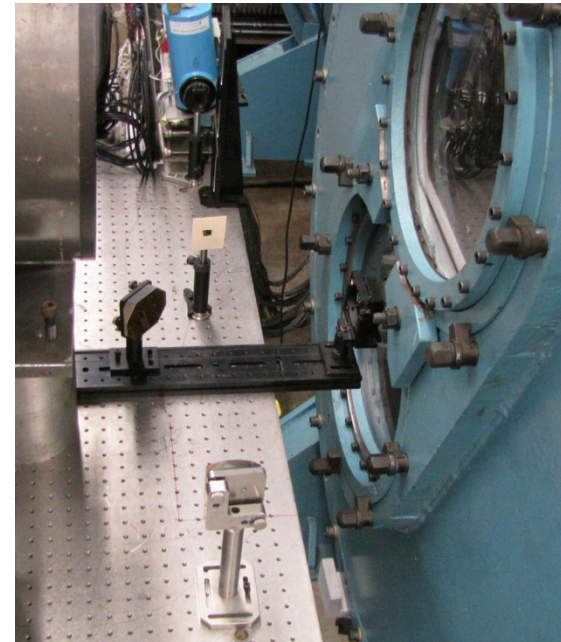
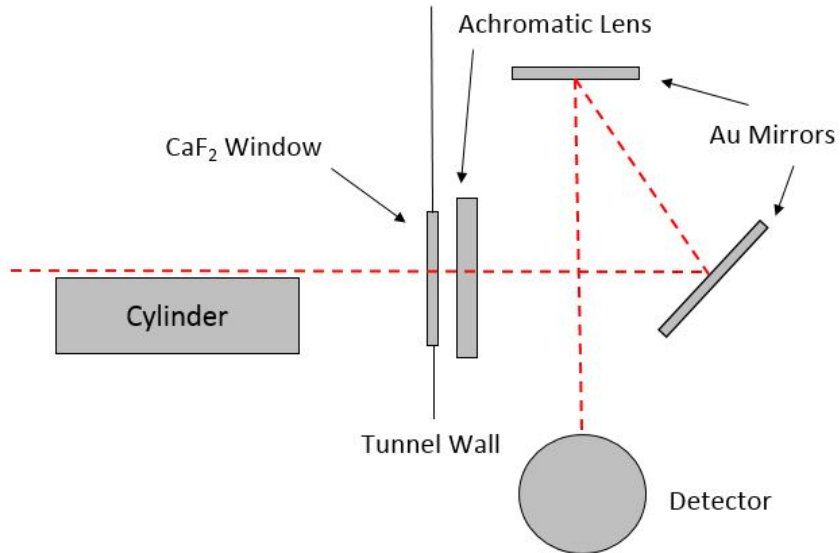
Asphere



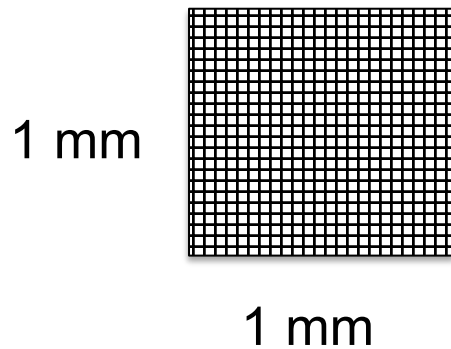


Top View

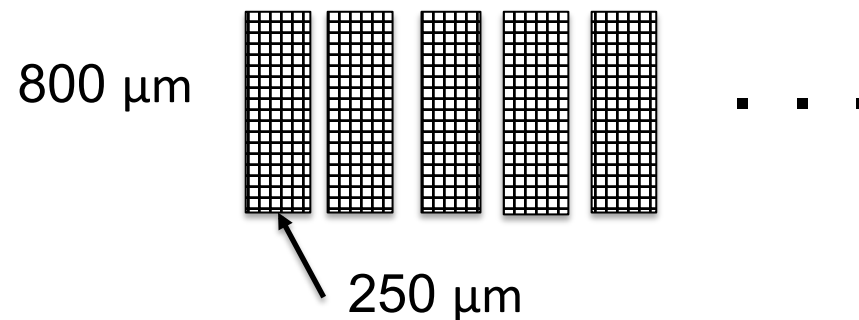
Catch Side (Detector)



Single-Element Detector



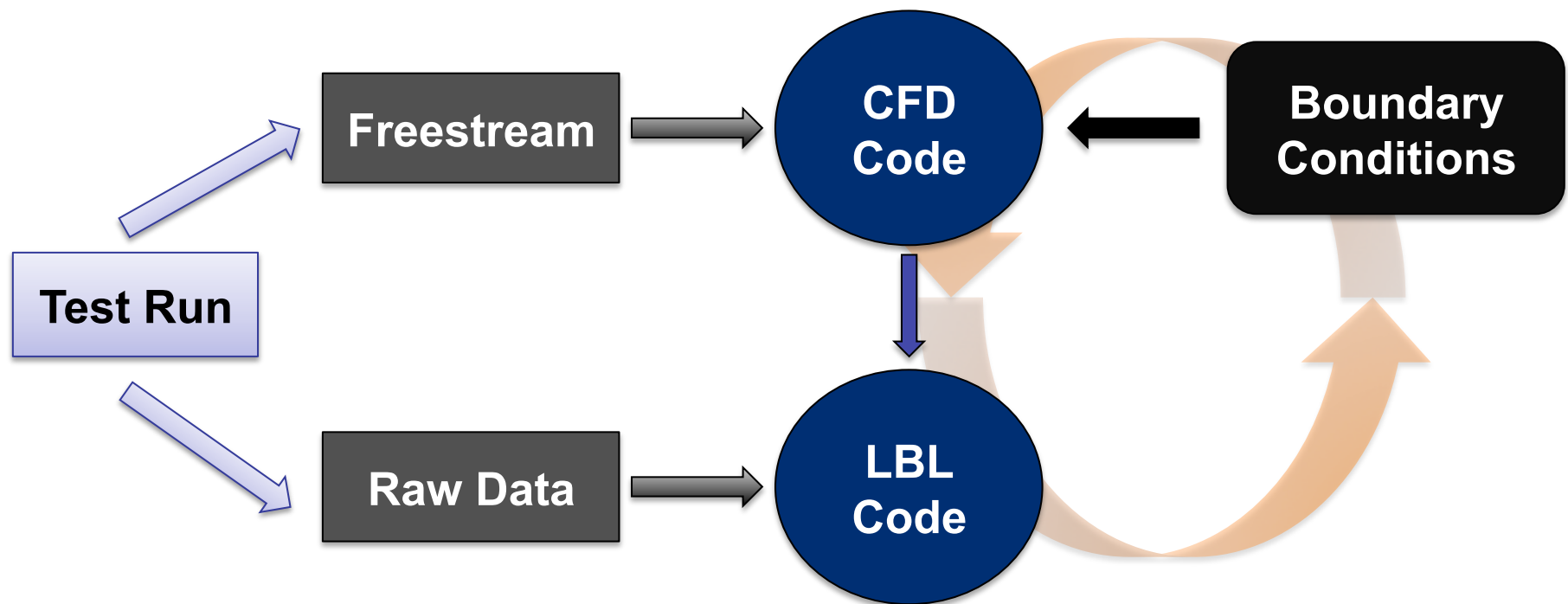
Linear Array Detector (32 elements)



4:1 magnification or greater possible with different optics

CFD : Computational Fluid Dynamics

LBL : Line-by-Line





CFD Boundary Condition Models of Surface Catalysis



- Non-catalytic wall: no recombination occurs on the surface, which implies zero diffusion flux to surface.

$$-J_k = 0$$

- Super-catalytic wall: Explicitly specified composition corresponding to complete recombination of energetic species into lowest energy state (N_2/O_2 for air).
- Specified reaction efficiency (SRE) catalytic wall: A percentage of reactants reaching the surface for which a reaction occurs. Controlled with a single efficiency parameter, γ , but γ has no connection to a physical process.

$$-\rho_w D_k \nabla y_k \Big|_w + \rho_w v_w y_{k,w} = \sum_r \alpha_r M_k \left(\frac{\gamma_r \rho_w c_{j(r)}}{M_{j(r)}} \sqrt{\frac{\Re T_w}{2\pi M_{j(r)}}} \right)$$

- Generalized finite rate surface chemistry (FRSC) wall: Reactions are modeled via one or more physical kinetic processes to generate production rates for each species at the surface, balanced by diffusion into the gas interior. Most physical BC, but requires a large number of parameters not easily obtainable.

$$-\rho_w D_k \nabla y_k \Big|_w + \rho_w v_w y_{k,w} = M_k \sum_{i=1}^{Nr} \left\{ \left(v_{ki}'' - v_{ki}' \right) \left(k_{fi} \prod_{m=1}^{Ns} [X_m]^{v_{mi}'} - k_{bi} \prod_{m=1}^{Ns} [X_m]^{v_{mi}''} \right) \right\}$$

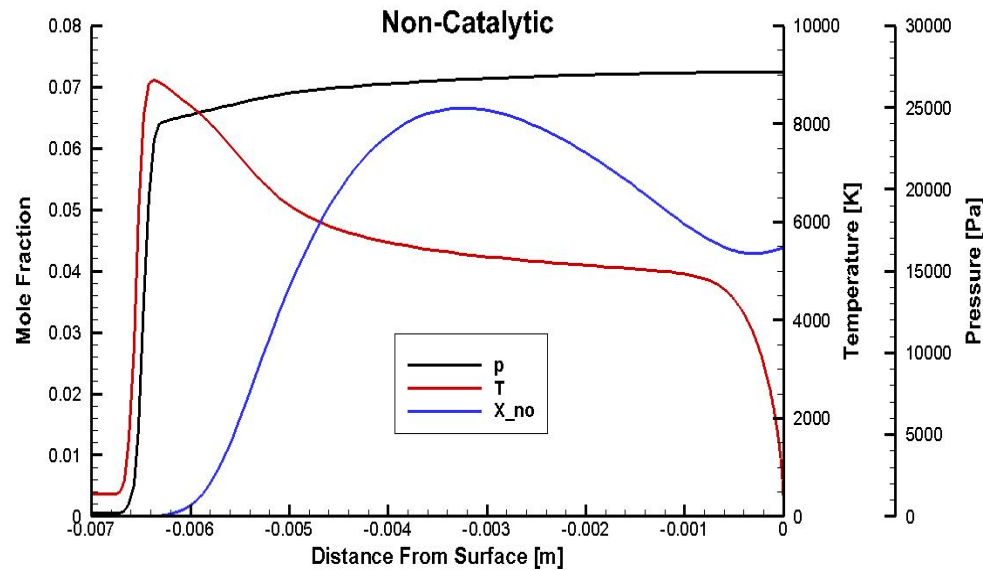
Computational Fluid Dynamics

Freestream Conditions

$$v = 4,249 \text{ m/s}$$

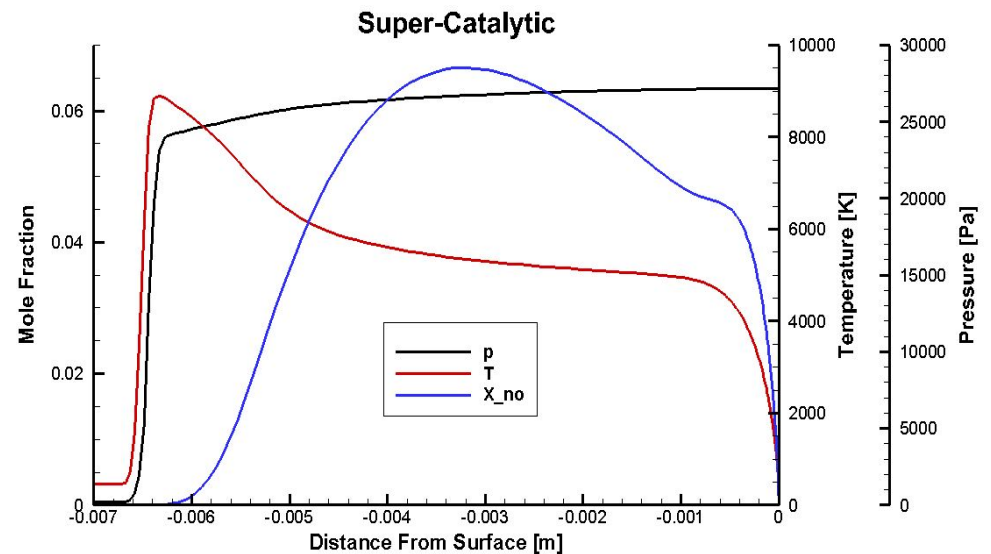
$$\rho = 0.00159 \text{ kg/m}^3$$

$$T = 457 \text{ K}$$

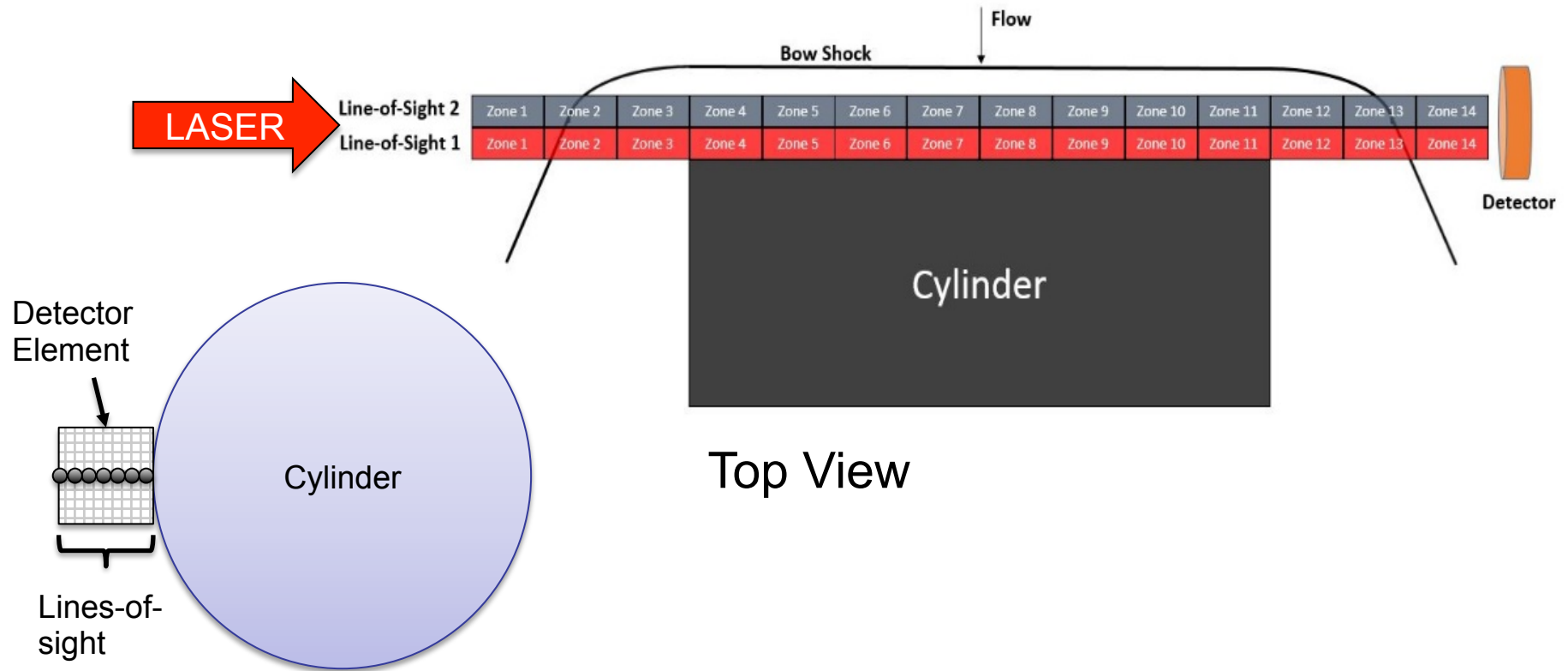


Key Difference

Concentration of
NO in shock layer



Line-by-Line Spectra Calculation



Side View
Finite detector area

Varying flow field

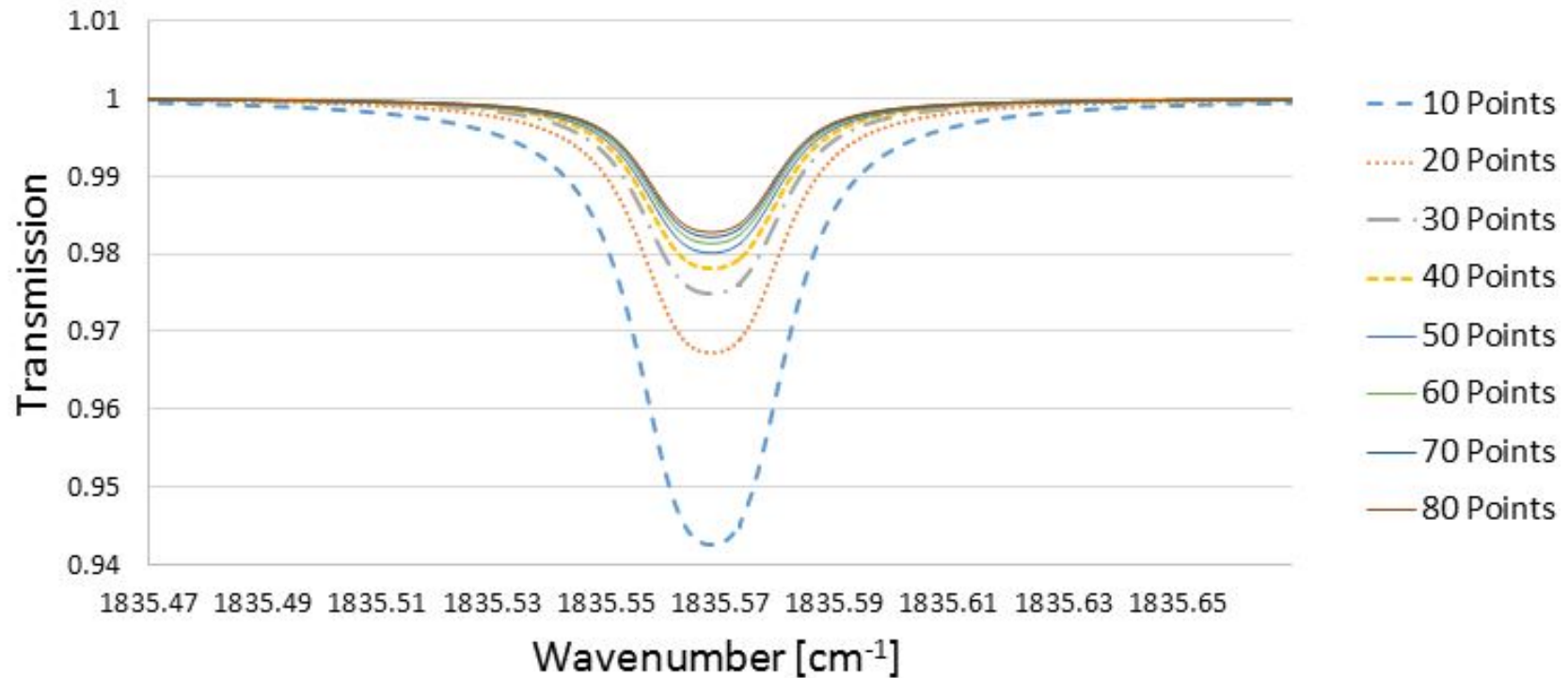


Multiple lines-of-sight

Multiple homogeneous zones

Line-of-Sight Number Independence

Grid Independence of LOS Calculation



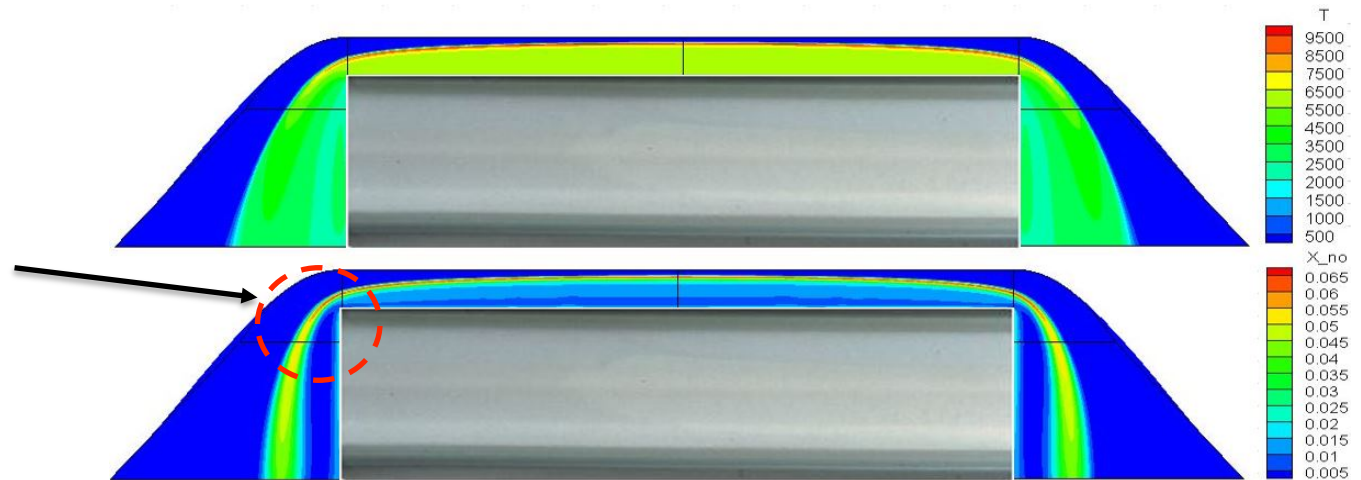
Number
independence



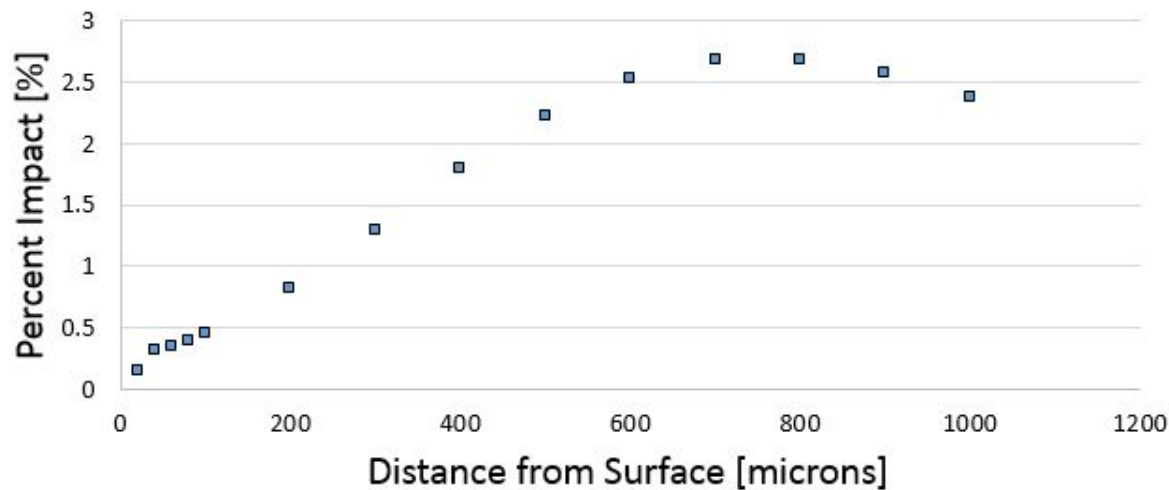
Number of LOS > 80-100

Expanding Flow Around Edge of Cylinder

NO expanding
around cylinder
edge



Percentage Edge Contribution for Fundamental
Absorption Feature



Result

Absorption confined to
width of the cylinder

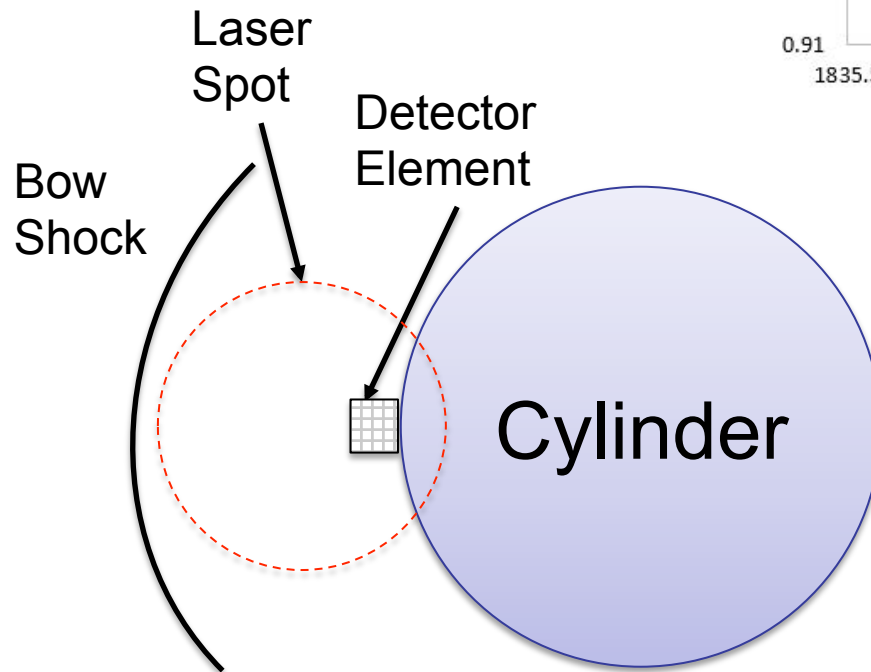
Single-Element Detector

Freestream Conditions

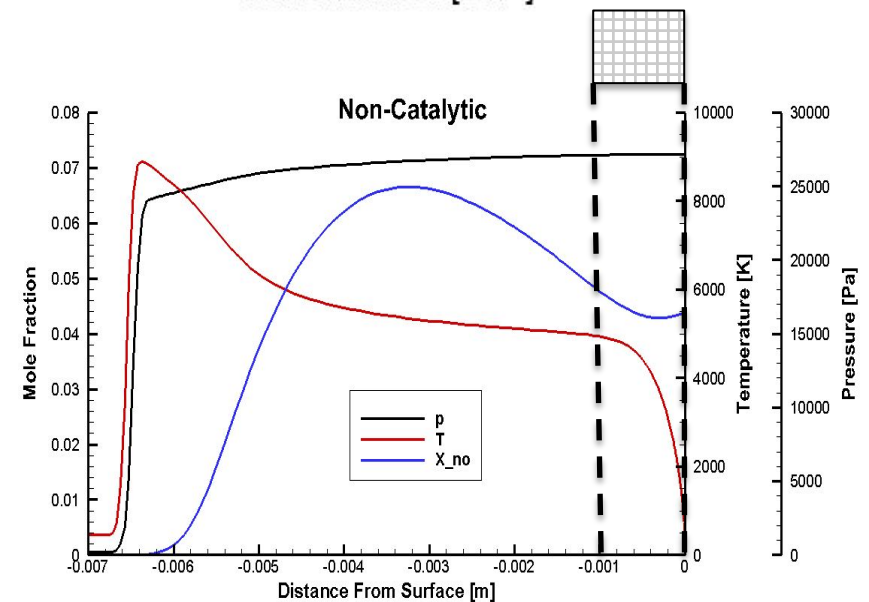
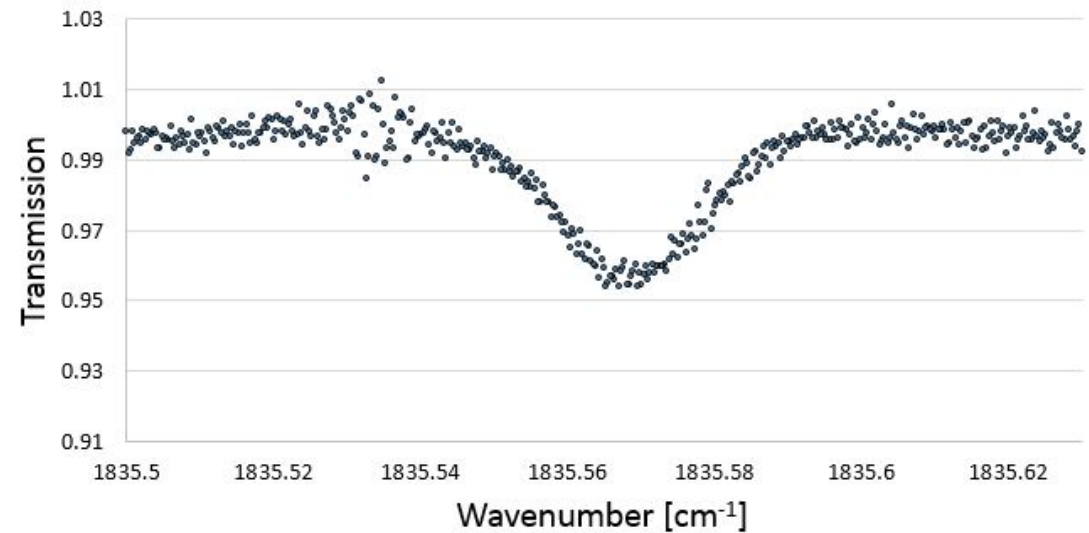
$$v = 4,249 \text{ m/s}$$

$$\rho = 0.00159 \text{ kg/m}^3$$

$$T = 457 \text{ K}$$

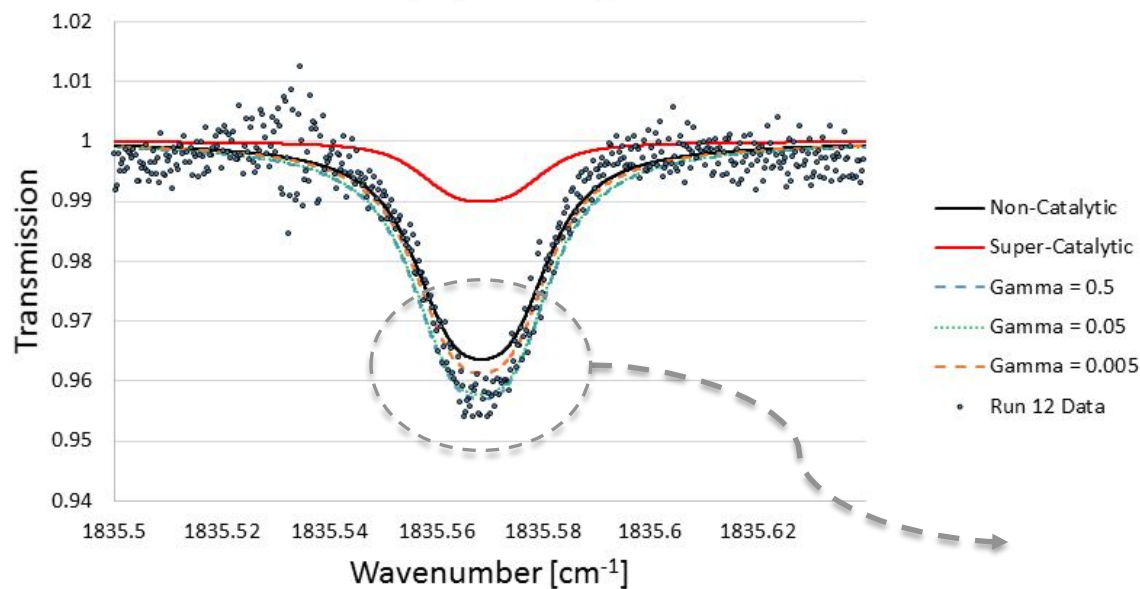


Raw Transmission Data: 3 Pt. Average



Single-Element Detector

Varying Boundary Conditions



2D CFD Solution

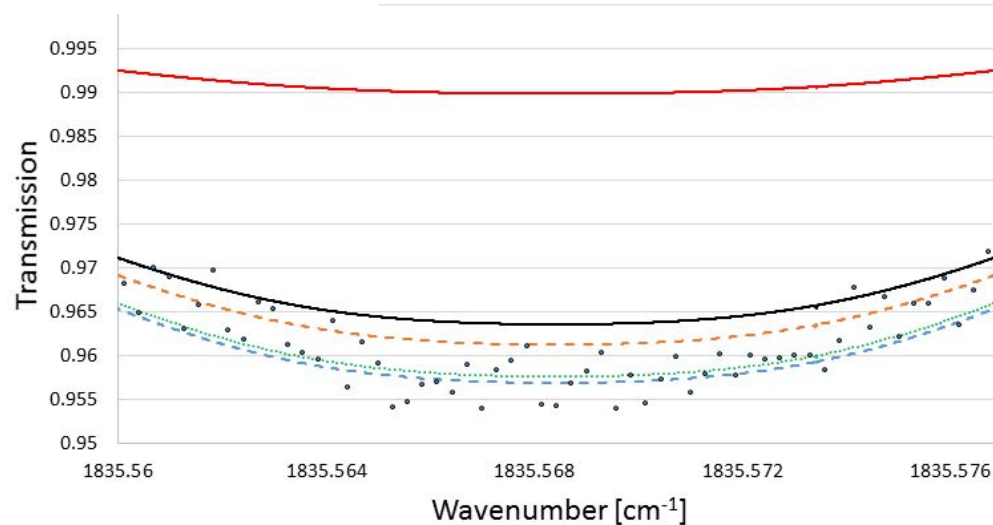


Line-by-Line Code



Simulated Transmission

Zoom-In View of Peak

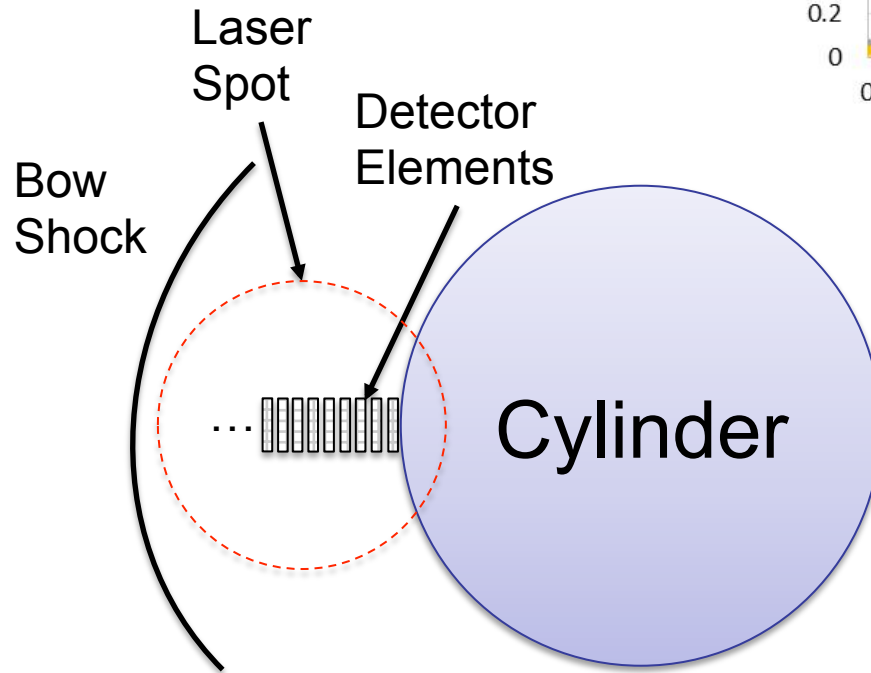


Freestream Conditions

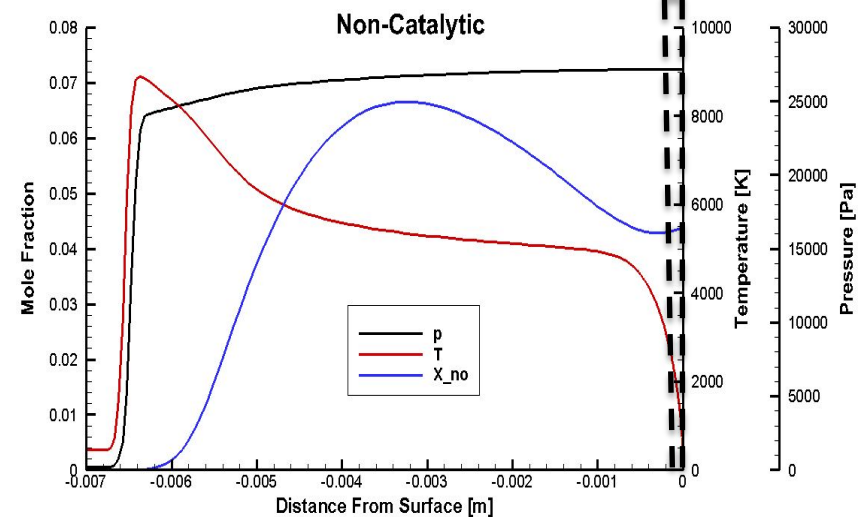
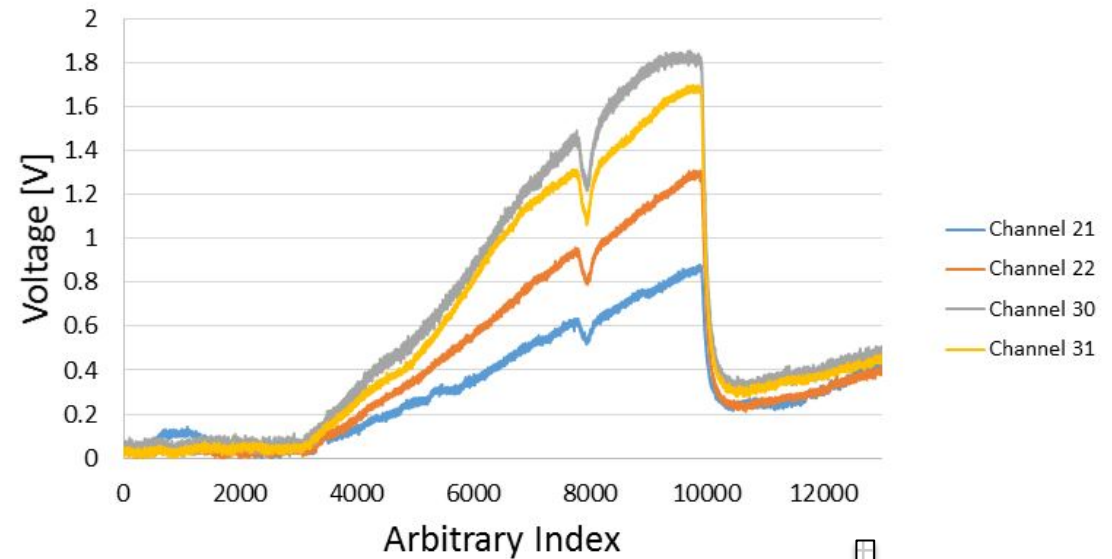
$$v = 5,166 \text{ m/s}$$

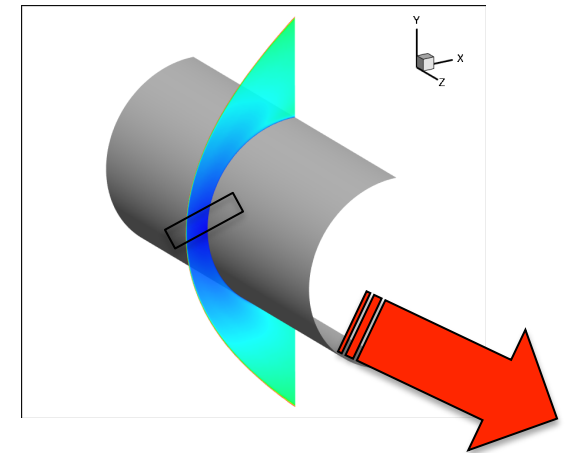
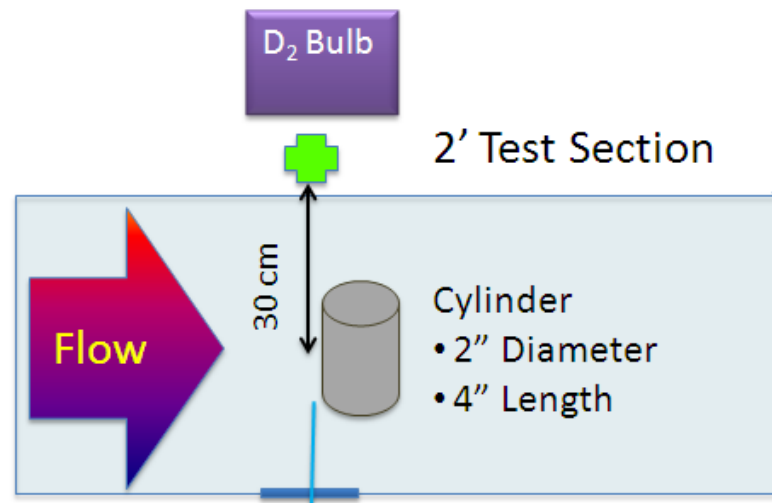
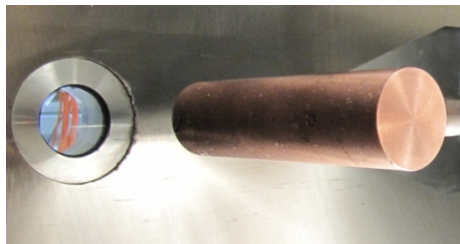
$$\rho = 0.00317 \text{ kg/m}^3$$

$$T = 215 \text{ K}$$

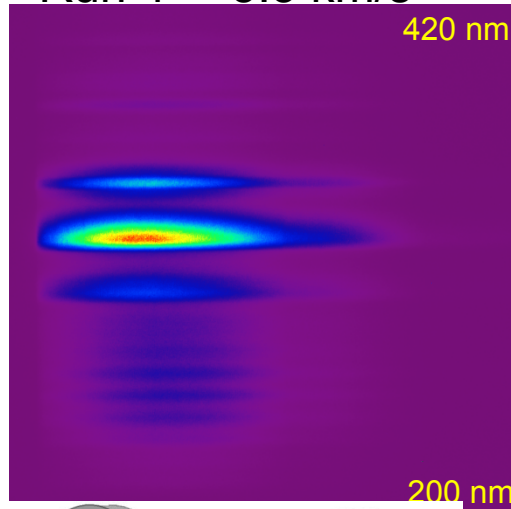


Linear Array Detector

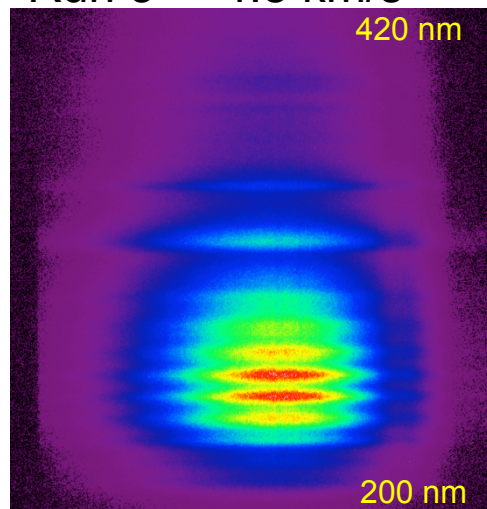




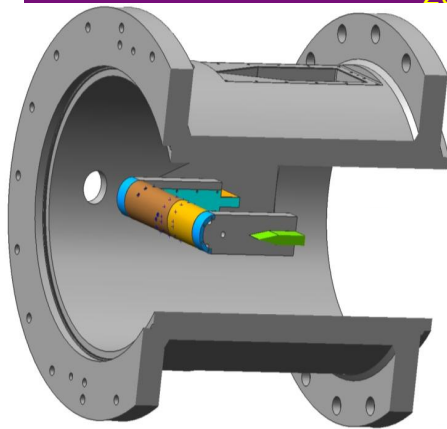
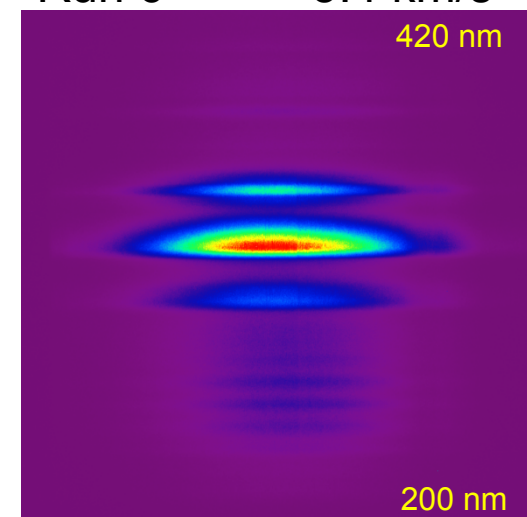
Run 4 5.3 km/s



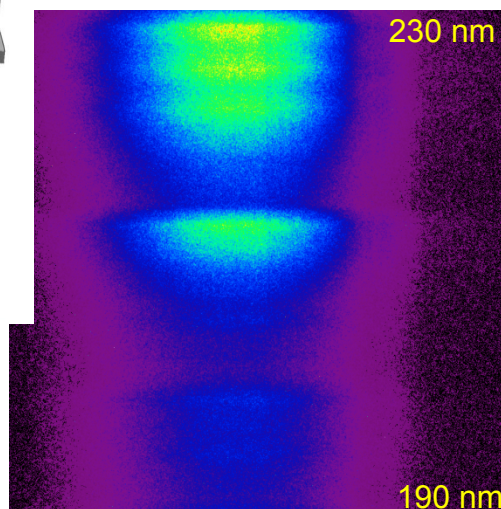
Run 5 4.8 km/s



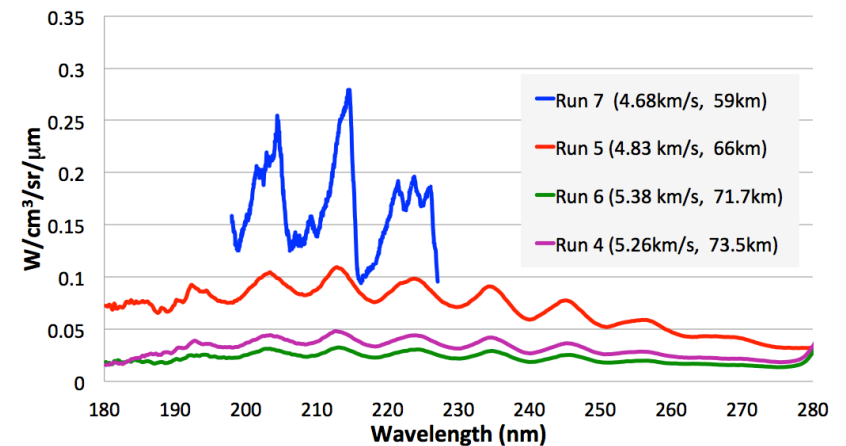
Run 6 5.4 km/s



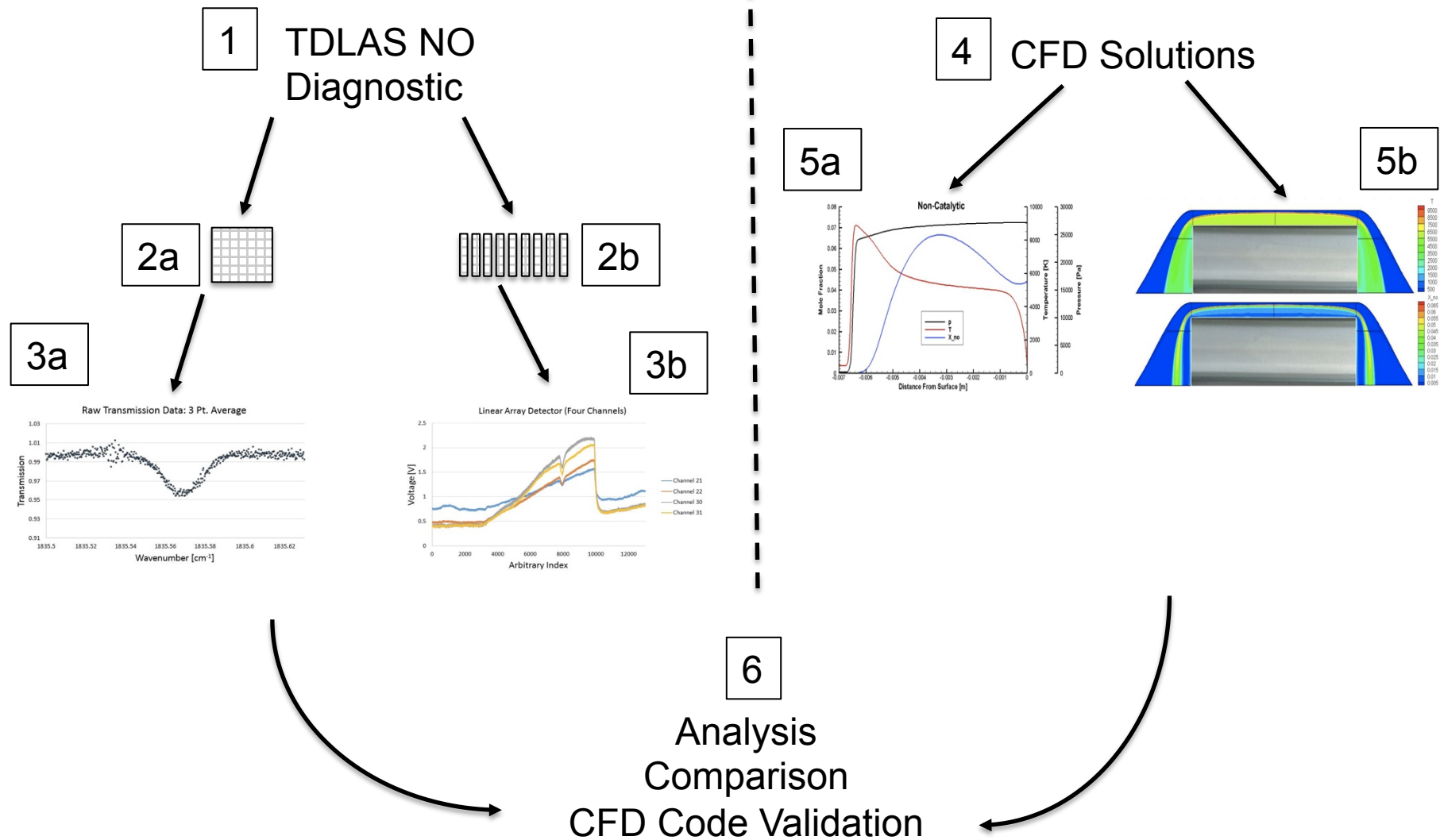
Run 7 4.7 km/s

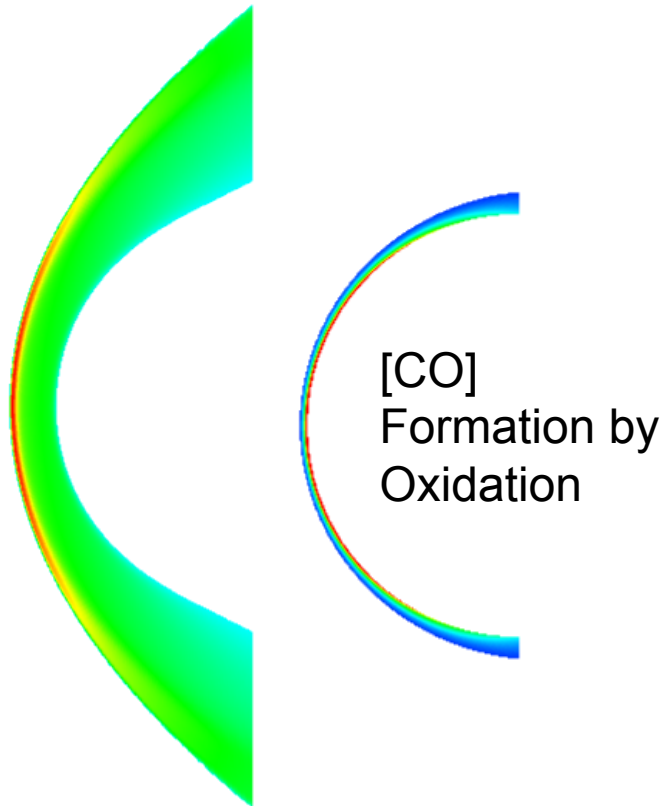


High resolution
Measurement
 $\Delta\lambda = 0.17\text{nm}$

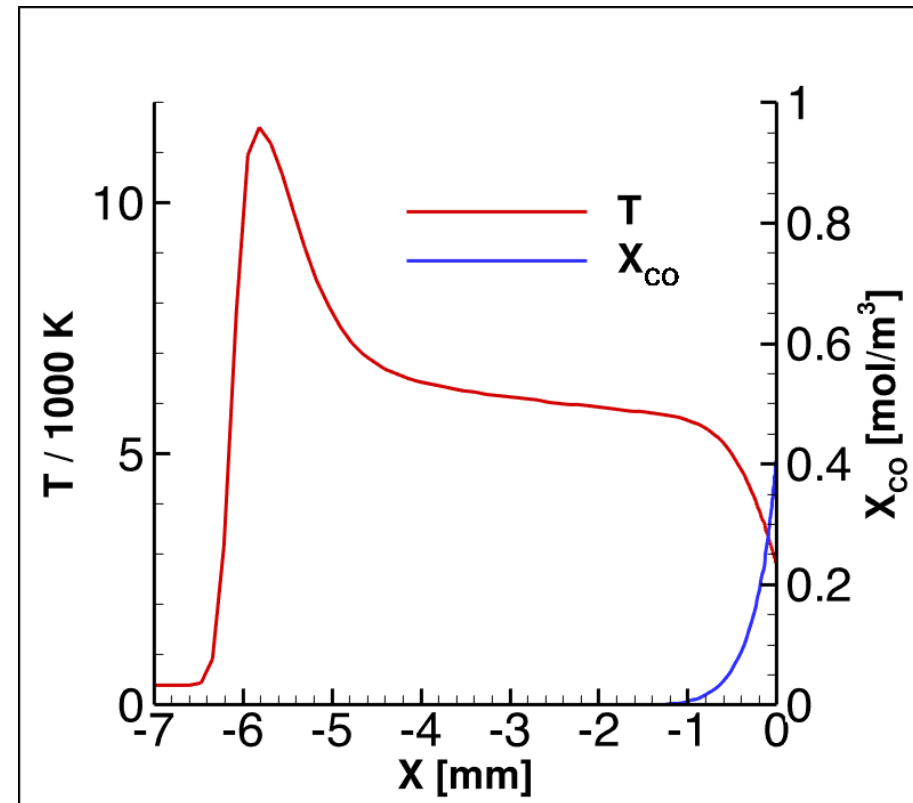


Summary and Conclusions





Temperature
Field in Shock
Layer



- In principle, direct substitution of TDLAS targeting CO transition possible.
- More challenging environment because of variable wall temperature
- Potentially use linear array detector to track surface recession in real-time?